Contents

1   Maximum ratings

Table 1. Absolute maximum ratings

Symbol	Parameter	Value	Unit
IS	Supply current at V_{cl}[1]	25	mA
VLVG	Low side output	14.6	V
VOUT	High side reference	-1 to VBOOT -18	V
VHVG	High side output	-1 to VBOOT	V
VBOOT	Floating supply voltage	618	V
dVBOOT/dt	VBOOT pin slew rate (repetitive)	±50	V/ns
dVOUT/dt	OUT pin slew rate (repetitive)	±50	V/ns
Vir	Forced input voltage (pins Rfmin, Rfstart)	-0.3 to 5	V
Vic	Forced input voltage (pins Css, Cf)	-0.3 to 5	V
VEN1, VEN2	Enable input voltage	-0.3 to 5	V
IEN1, IEN2	Enable input current	±3	mA
Vopc	Sense op amp common mode range	-0.3 to 5	V
Vopd	Sense op amp differential mode range	-5 to 5	V
Vopo	Sense op amp output voltage (forced)	4.6	V
Tstg	Storage temperature	-40 to +150	°C
Tj	Junction temperature	-40 to +150	°C
Tamb	Ambient temperature	-40 to +125	°C

1. The device is provided of an internal clamping Zener between GND and the Vs pin, It must not be supplied by a low impedance voltage source.

Note: *ESD immunity for pins 14, 15 and 16 is guaranteed up to 900 (human body model).*

Table 2. Thermal data

Symbol	Parameter	SO16N	DIP16	Unit
R_{thJA}	Thermal resistance junction to ambient	120	80	°C/W

Table 3. Recommended operating conditions

Symbol	Parameter	Value	Unit
V_S	Supply voltage	10 to Vcl	V
V_{out}[1]	High side reference	-1 to Vboot - Vcl	V
V_{boot}[1]	Floating supply rail	500	V
fmax	Maximum switching frequency	400	kHz

1. If the condition V_{boot} - V_{out} < 18 is guaranteed, V_{out} can range from -3 to 580 V.

2 Electrical characteristics

V_S = 12 V; V_{BOOT} - V_{OUT} = 12 V; T_A = 25 °C

Table 4. Electrical characteristics

Symbol	Pin	Parameter	Test condition	Min.	Typ.	Max.	Unit
Supply voltage							
V_{suvp}	12	V_S turn on threshold		10	10.7	11.4	V
V_{suvn}		V_S turn off threshold		7.3	8	8.7	V
V_{suvh}		Supply voltage under voltage hysteresis			2.7		V
V_{cl}		Supply voltage clamping		14.6	15.6	16.6	V
I_{su}		Start up current	$V_S < V_{suvn}$			250	µA
I_q		Quiescent current, fout = 60 kHz, no load	$V_S > V_{suvp}$		2	3	mA
High voltage section							
$I_{bootleak}$	16	BOOT pin leakage current	V_{BOOT} = 580 V			5	µA
$I_{outleak}$	14	OUT pin leakage current	V_{OUT} = 562 V			5	µA
R_{DSon}	16	Bootstrap driver on-resistance		100	150	300	Ω
High/low side drivers							
I_{hvgso}	15	High side driver source current	V_{HVG} - V_{OUT} = 0	170	250		mA
I_{hvgsi}		High side driver sink current	V_{HVG} - V_{BOOT} = 0	300	450		mA
I_{lvgso}	11	Low side driver source current	V_{LVG} - GND = 0	170	250		mA
I_{lvgsi}		Low side driver sink current	V_{LVG} - V_S = 0	300	450		mA
t_{rise}	15,11	Low/high side output rise time	C_{load} = 1 nF		80	120	ns
t_{fall}			C_{load} = 1 nF		40	80	ns
Oscillator							
DC	14	Output duty cycle		48	50	52	%
f_{min}		Minimum output oscillation frequency	C_f = 470 pF; R_{fmin} = 50 kΩ	58.2	60	61.8	kHz
f_{start}		Soft-start output oscillation frequency	C_f = 470 pF; R_{fmin} = 50 kΩ; R_{fstart} = 47kΩ	114	120	126	kHz

Table 4. Electrical characteristics (continued)

Symbol	Pin	Parameter	Test condition	Min.	Typ.	Max.	Unit
V_{ref}	2, 4	Voltage to current converters threshold		1.9	2	2.1	V
t_d	14	Deadtime between low and high side conduction		0.2	0.27	0.35	µs
IVref	2, 4	Reference current		120			µA
Timing section							
k_{ss}	1	Soft-start timing constant	$C_{ss} = 330$ nF	0.115	0.15	0.185	s/µF
Sense op amp							
I_{IB}	6, 7	Input bias current				0.1	µA
V_{io}		Input offset voltage		-10		10	mV
R_{out}		Output resistance		200		300	?
I_{out-}	5	Source output current	$V_{out} = 4.5$ V	1			mA
I_{out+}		Sink output current	$V_{out} = 0.2$ V	1			mA
V_{ic}	6,7	Op amp input common mode range		-0.2		3	V
GBW		Sense op amp gain band width product[1]		0.5	1		MHz
Gdc		DC open loop gain		60	80		dB
Comparators							
Vthe1	8	Enabling comparator threshold		0.56	0.6	0.64	V
Vthe2	9	Enabling comparator threshold		1.05	1.2	1.35	V
tpulse	8,9	Minimum pulse length				200	ns

1. Guaranteed by design.

3 Pin connections

Figure 2. Pin connections
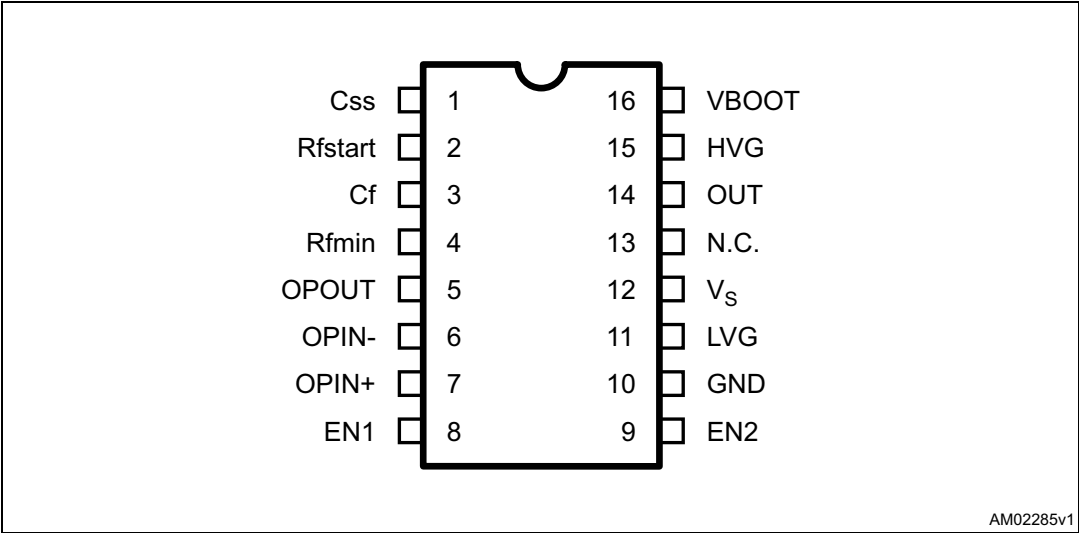
Pin no.	Name	Function
1	CSS	Soft-start timing capacitor
2	R_{fstart}	Soft-start frequency setting - low impedance voltage source -see also C_f
3	C_f	Oscillator frequency setting - see also R_{fmin}, R_{fstart}
4	R_{fmin}	Minimum oscillation frequency setting - low impedance voltage source - see also C_f
5	O_{Pout}	Sense op amp output - low impedance
6	O_{Pon-}	Sense op amp inverting input -high impedance
7	O_{Pon+}	Sense op amp non inverting input - high impedance
8	EN1	Half bridge latched enable
9	EN2	Half bridge unlatched enable
10	GND	Ground
11	LVG	Low side driver output
12	V_s	Supply voltage with internal Zener clamp
13	N.C.	Not connected
14	OUT	High side driver reference
15	HVG	High side driver output
16	V_{boot}	Bootstrapped supply voltage

Table 5. Pin description

4   Timing diagrams

Figure 3. EN2 timing diagram
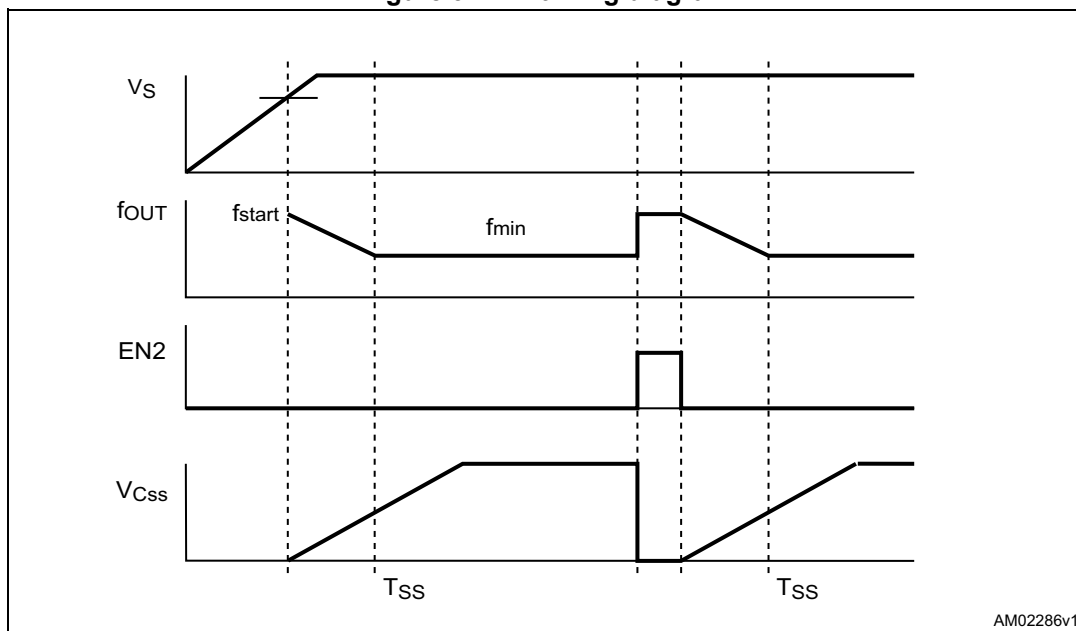
Figure 4. EN1 timing diagram
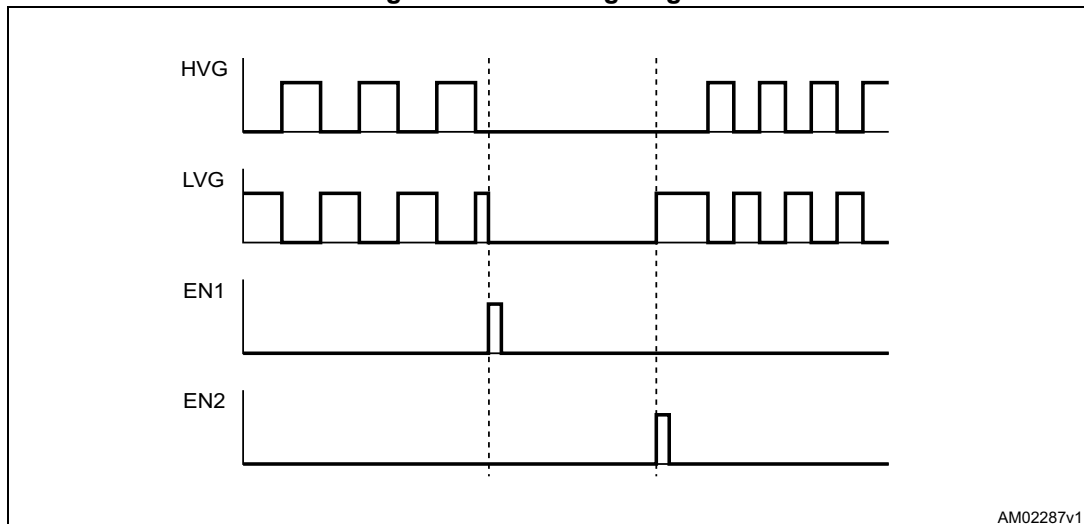
Figure 5. Oscillator/output timing diagram
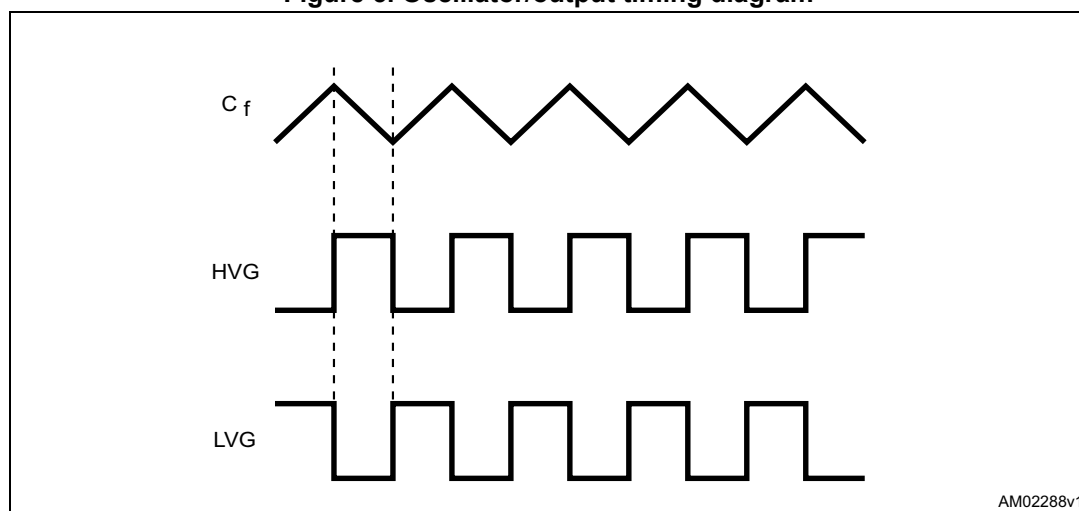
# 5 Block diagram description

5.1 High/low side driving section

A high and low side driving section provide the proper driving to the external power MOS or IGBT. A high sink/source driving current (450/250 mA typ.) ensure fast switching times also when size for power MOS are used. The internal logic ensures a minimum deadtime to avoid cross conduction of the power devices.

5.2 Timing and oscillator section

The device is provided of a soft-start function. It consists in a period of time, T_{SS}, in which the switching frequency shifts from fstart to fmin. This feature is explained in the following description (refer to *Figure 6* and *Figure 7*).

Figure 6. Soft-start and frequency shifting block
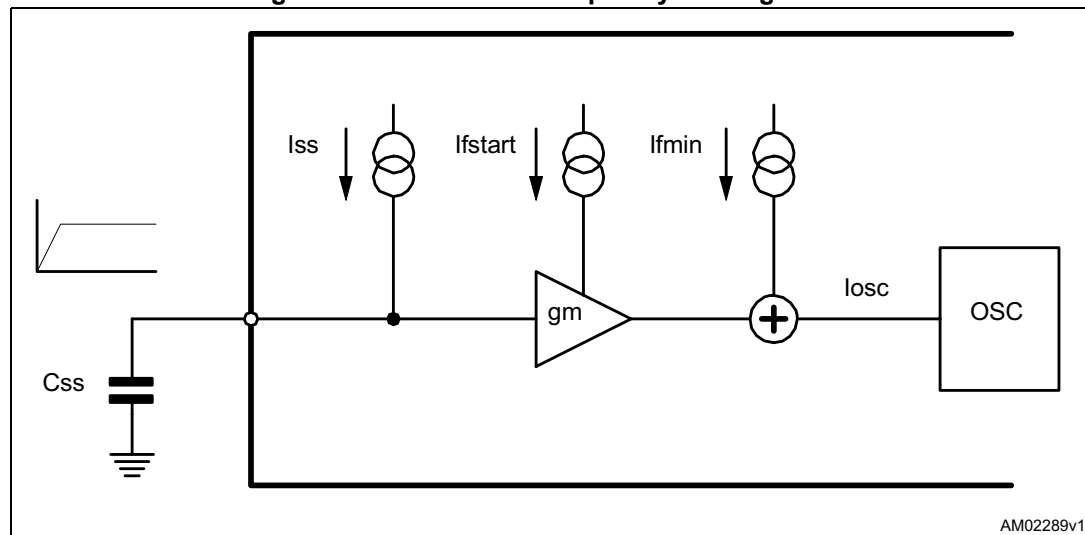
During the soft-start time the current I_{SS} charges the capacitor $C_{SS,}$ generating a voltage ramp which is delivered to a transconductance amplifier, as shown in *Figure 6*. Thus this voltage signal is converted in a growing current which is subtracted to Ifstart. Therefore the current which drives the oscillator to set the frequency during the soft-start is equal to:

Equation 1

$$I_{osc} = I_{fmin} + (I_{fstart} - g_m V_{Css}(t)) = I_{fmin} + \left(I_{fstart} - \frac{g_m I_{ss}}{C_{ss}}\right)$$

Equation 2

$$\text{where} \quad I_{fmin} = \frac{V_{REF}}{R_{fmin}}, I_{fstart} = \frac{V_{REF}}{R_{fstart}}, V_{REF} = 2V$$

At the startup (t = 0) the oscillator frequency is set by:

Equation 3

$$I_{OSC}(0) = I_{fmin} + I_{fstart} = V_{REF}\left(\frac{1}{R_{fmin}} + \frac{1}{R_{fstart}}\right)$$

At the end of the soft-start (t = T_{SS}) the second term of eq.1 decreases to zero and the switching frequency is set only by Imin (i.e. R_{fmin}):

Equation 4

$$I_{OSC}(T_{SS}) = I_{fmin} = \frac{V_{REF}}{R_{fmin}}$$

Since the second term of *Equation 1* is equal to zero, we have:

Equation 5

$$I_{fstart} - \frac{g_m I_{ss}}{C_{ss}} T_{SS} = 0 \rightarrow T_{SS} = \frac{C_{ss} I_{fstart}}{g_m I_{ss}}$$

Note that there is not a fixed threshold of the voltage across C_{SS} in which the soft-start finishes (i.e. the end of the frequency shifting), and Tss depends on C_{SS}, Ifstart, g_m, and I_{SS} (*Equation 5*). Making T_{SS} independent of Ifstart, the Iss current has been designed to be a fraction of I_{fstart}, so:

Equation 6

$$I_{SS} = \frac{I_{fstart}}{K} \rightarrow T_{SS} = \frac{C_{ss} I_{fstart}}{g_m I_{fstart} K} \rightarrow T_{SS} = \frac{C_{ss}}{g_m K} \rightarrow T_{SS} - k_{SS} C_{SS}$$

In this way the soft-start time depends only on the capacitor C_{SS}. The typical value of the k_{SS} constant (Soft-start timing constant) is 0.15 s/μF.

The current I_{osc} is fed to the oscillator as shown in *Figure 7*. It is twice mirrored (x4 and x8) generating the triangular wave on the oscillator capacitor C_f. Referring to the internal structure of the oscillator (*Figure 7*), a good relationship to compute an approximate value of the oscillator frequency in normal operation is:

Equation 7

$$f_{min} = \frac{1.41}{R_{fmin} C_f}$$

The degree of approximation depends on the frequency value, but it remains very good in the range from 30 kHz to 100 kHz (*Figure 8* to *Figure 12*).
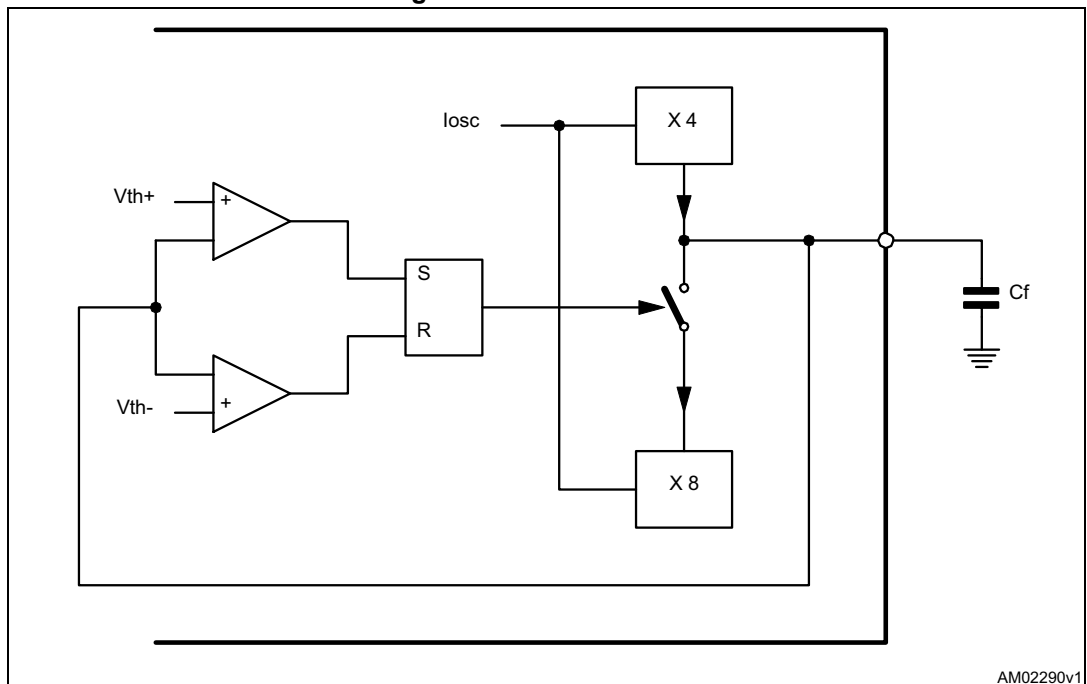
Figure 7. Oscillator block
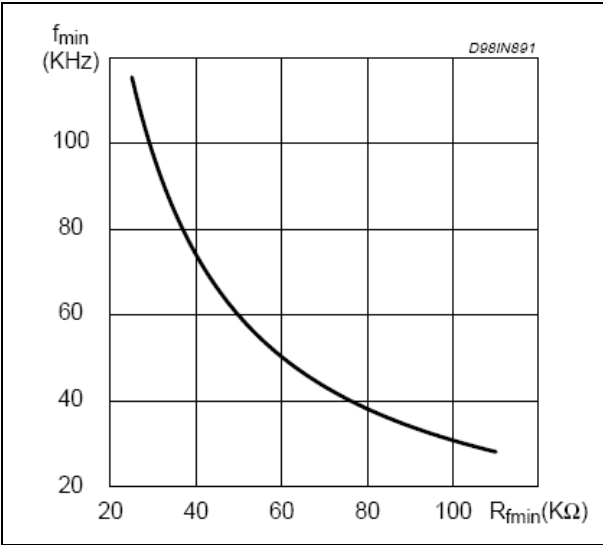
Figure 8. Typ. f$_{min}$ vs. R$_{fmin}$ at Cf = 470 pF

Figure 9. Typ. (f$_{start}$-f$_{min}$) vs. R$_{fstar}$ at C$_f$ = 470 pF
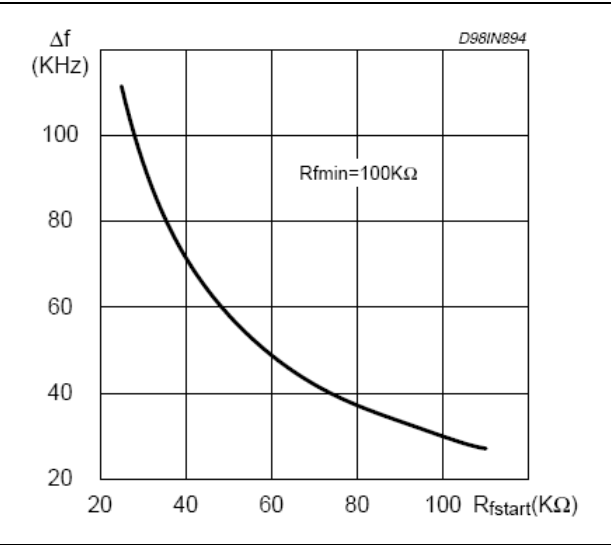
Figure 10. Typ. (f$_{start}$-f$_{min}$) vs. R$_{fstar}$ at C$_f$ = 470 pF
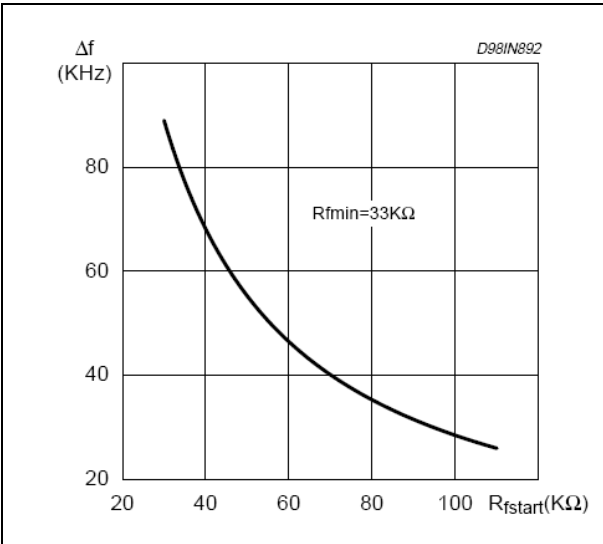
**Figure 11. f$_{min}$ at different R$_f$ vs C$_f$**
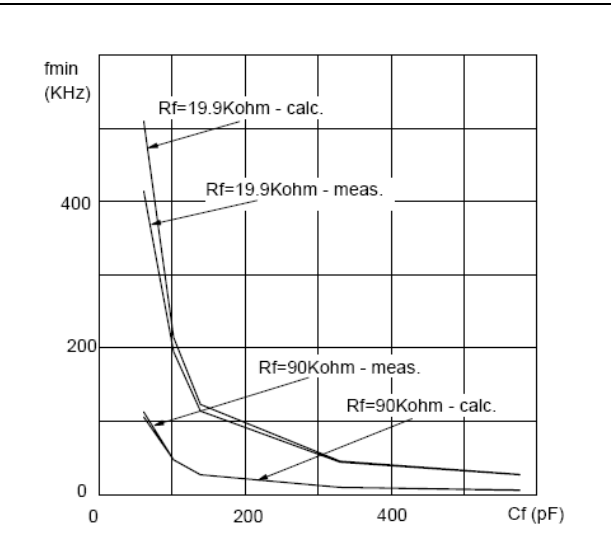
Figure 12. Typ. (f_{start}-f_{min}) vs. R_{fstar} at C_f = 470 pF
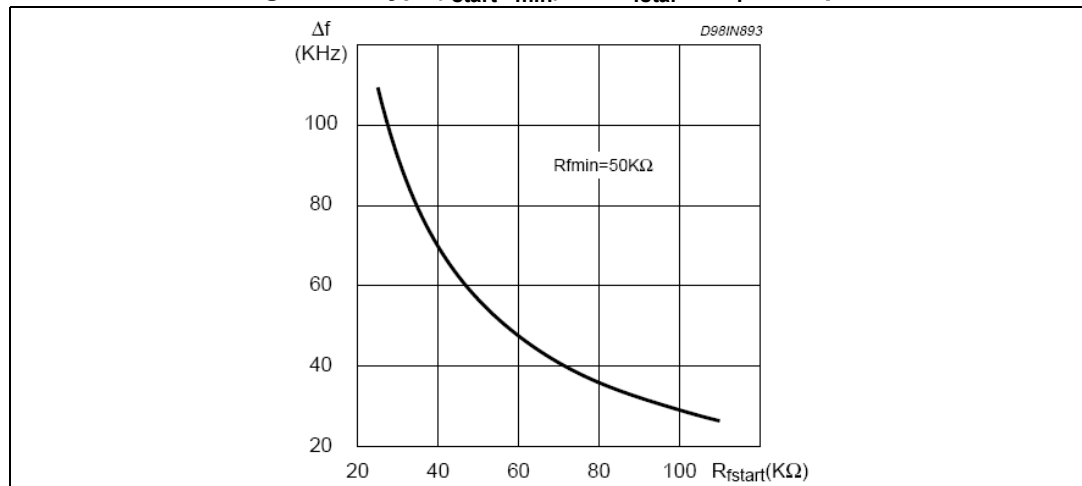
5.3 Bootstrap section

The supply of the high voltage section is obtained by means of a bootstrap circuitry. This solution normally requires a high voltage fast recovery diode for charging the bootstrap capacitor (*Figure 13* - part a). In the device a patented integrated structure replaces this external diode. It is released by means of a high voltage DMOS, driven synchronously with the low side driver (LVG), with in series a diode, as shown in *Figure 13* - part b.

Figure 13. Bootstrap driver
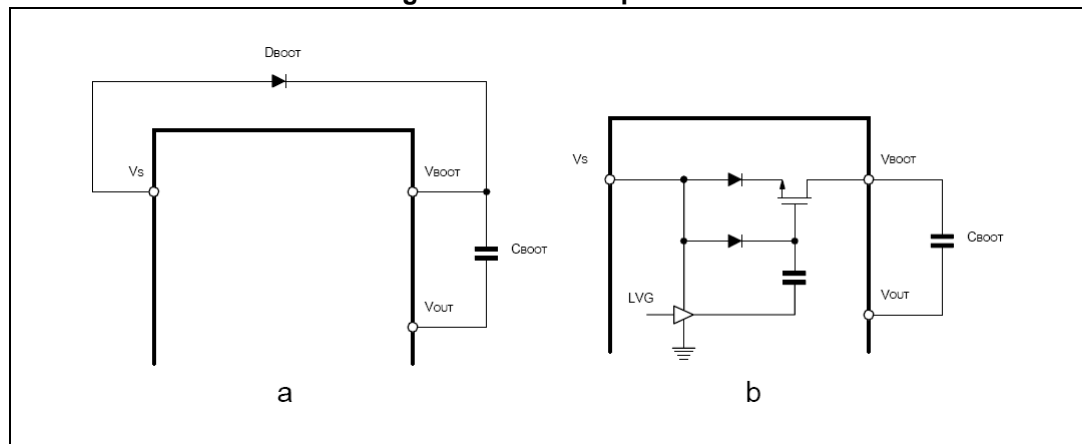
To drive the synchronized DMOS it is necessary a voltage higher than the supply voltage Vs. This voltage is obtained by means of an internal charge pump (*Figure 13* - part b).

The diode connected in series to the DMOS has been added to avoid undesirable turn on of it. The introduction of the diode prevents any current can flow from the Vboot pin to the VS one in case that the supply is quickly turned off when the internal capacitor of the pump is not fully discharged.

The bootstrap driver introduces a voltage drop during the recharging of the capacitor Cboot (i.e. when the low side driver is on), which increases with the frequency and with the size of the external power MOS. It is the sum of the drop across the R_{DSON} and of the diode

threshold voltage. At low frequency this drop is very small and can be neglected. Anyway increasing the frequency it must be taken in to account. In fact the drop, reducing the amplitude of the driving signal, can significantly increase the R_{DSON} of the external power MOS (and so the dissipation).

To be considered that in resonant power supplies the current which flows in the power MOS decreases increasing the switching frequency and generally the increases of R_{DSON} is not a problem because power dissipation is negligible. *Equation 8* is useful to compute the drop on the bootstrap driver:

Equation 8

$$V_{drop} = I_{charge}R_{dson} + V_{diode} \rightarrow V_{drop} = \frac{Q_g}{T_{charge}}R_{dson} + V_{diode}$$

where Q_g is the gate charge of the external power MOS, R_{dson} is the on-resistance of the bootstrap DMOS, and T_{charge} is the time in which the bootstrap driver remains on (about the semi-period of the switching frequency minus the deadtime). The typical resistance value of the bootstrap DMOS is 150 Ω. For example using a power MOS with a total gate charge of 30 nC the drop on the bootstrap driver is about 3 V, at a switching frequency of 200 kHz. In fact:

Equation 9

$$V_{drop} = \frac{30nC}{2.23\mu s}150\Omega + 0.6V \sim 2.6V$$

To summaries, if a significant drop on the bootstrap driver (at high switching frequency when large power MOS are used) represents a problem, an external diode can be used, avoiding the drop on the R_{DSON} of the DMOS.

5.4 Op amp section

The integrated op amp is designed to offer low output impedance, wide band, high input impedance and wide common mode range. It can be readily used to implement protection features or a closed loop control. For this purpose the op amp output can be properly connected to R_{fmin} pin to adjust the oscillation frequency.

5.5 Comparators

Two CMOS comparators are available to perform protection schemes.

Short pulses ($\geq$ 200 ns) on comparators input are recognized. The EN1 input (active high), has a threshold of 0.6 V (typical value) forces the device in a latched shut down state (e.g. LVG low, HVG low, oscillator stopped), as in the under voltage conditions. Normal operating conditions are resumed after a power-off power-on sequence. The EN2 input (active high), with a threshold of 1.2 V (typical value) restarts a soft-start sequence (see timing diagrams in *Figure 3*, *Figure 4*, and *Figure 5*). In addition the EN2 comparator, when activated, removes a latched shutdown caused by EN1.
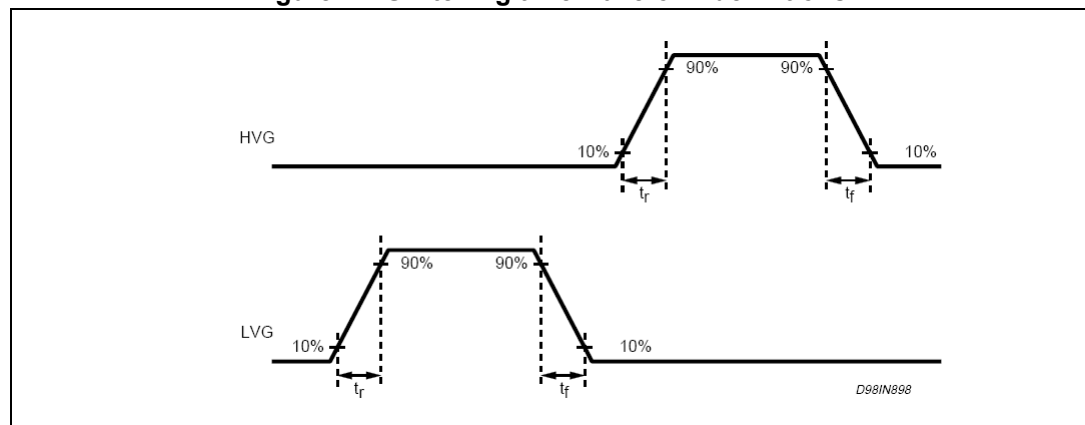
Figure 14. Switching time waveform definitions

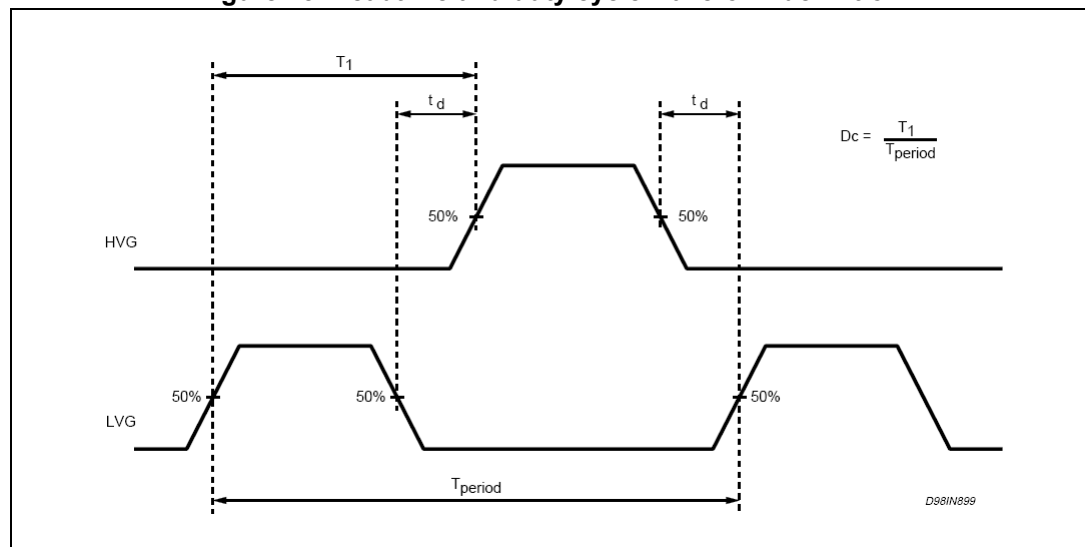**Figure 15. Deadtime and duty cycle waveform definition**

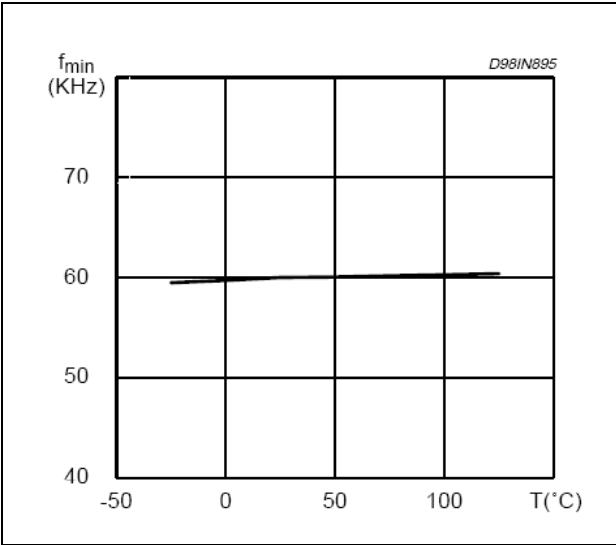### Figure 16. Typ. fmin vs. temperature

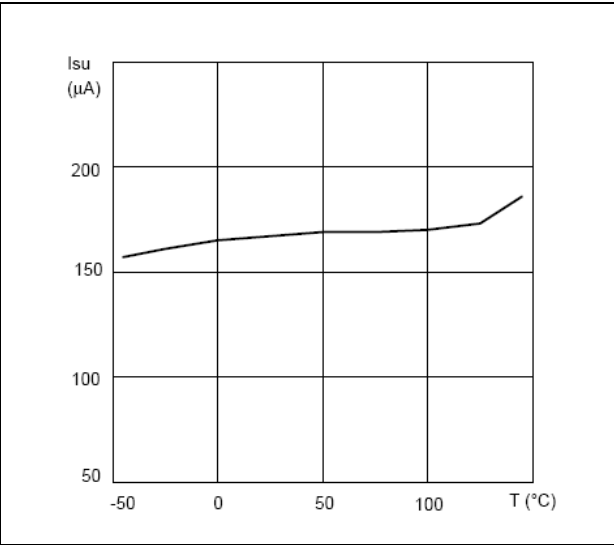### Figure 17. Startup current vs. temperature

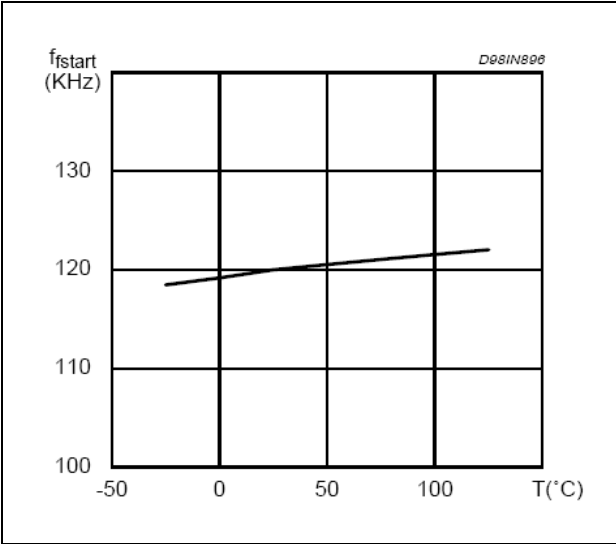### Figure 18. Typ. fstart vs. temperature

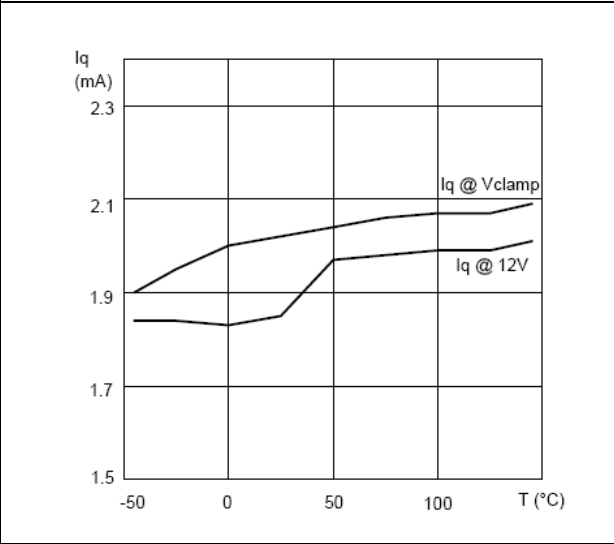### Figure 19. Quiescent current vs. temperature

Figure 20. Vs thresholds and clamp vs. temp.
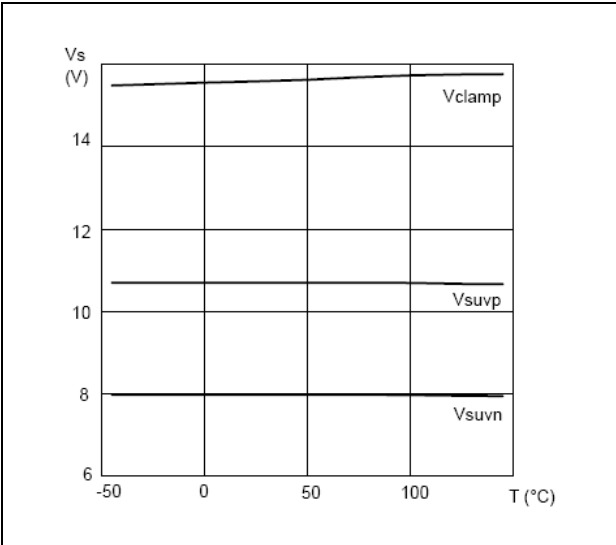

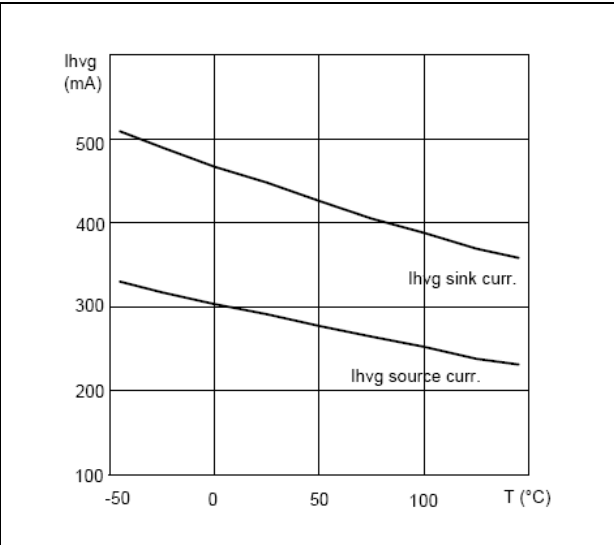**Figure 21. HVG source and sink current vs. temperature**

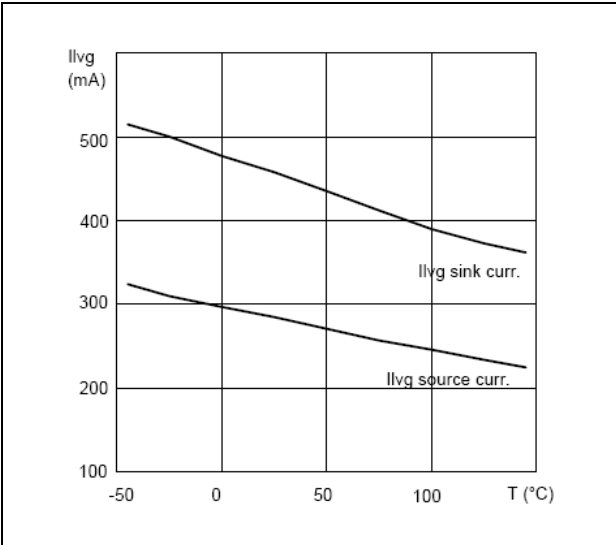**Figure 22. LVG source and sink current vs. temperature**

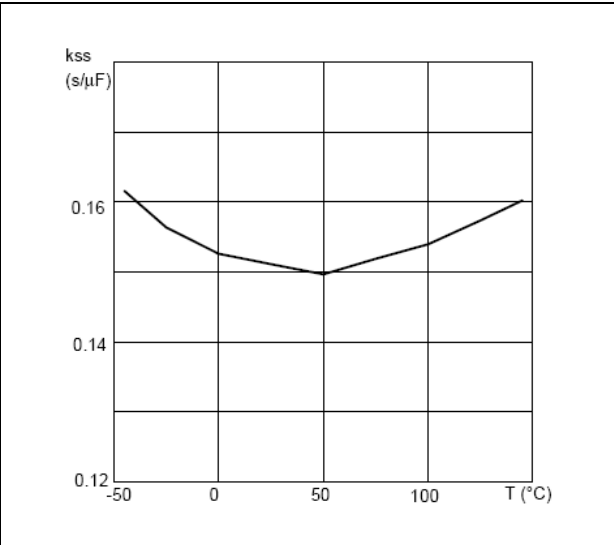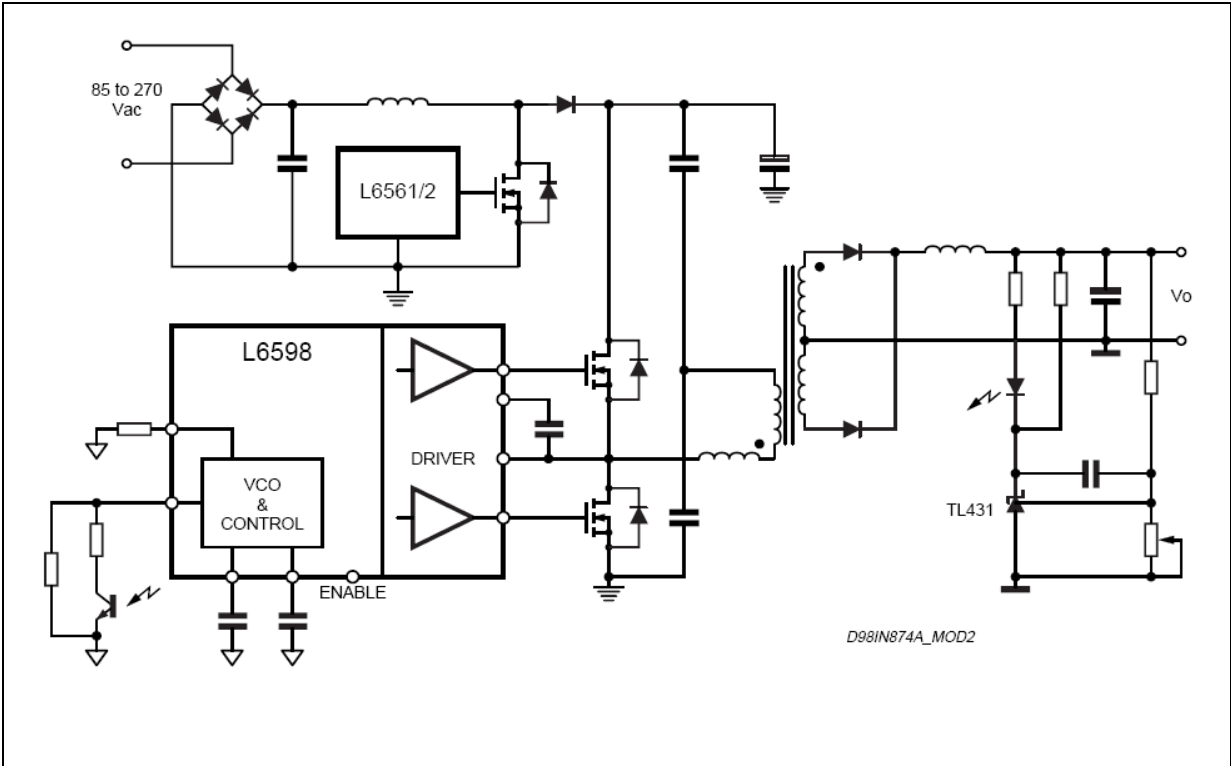**Figure 23. Soft-start timing constant vs. temperature**

Figure 24. Wide range AC/DC adapter application

D98IN874A_MOD2

6   Package information

In order to meet environmental requirements, ST offers these devices in different grades of ECOPACK® packages, depending on their level of environmental compliance. ECOPACK specifications, grade definitions and product status are available at: www.st.com. ECOPACK is an ST trademark.

Figure 25. Plastic DIP16 (0.25) package outline
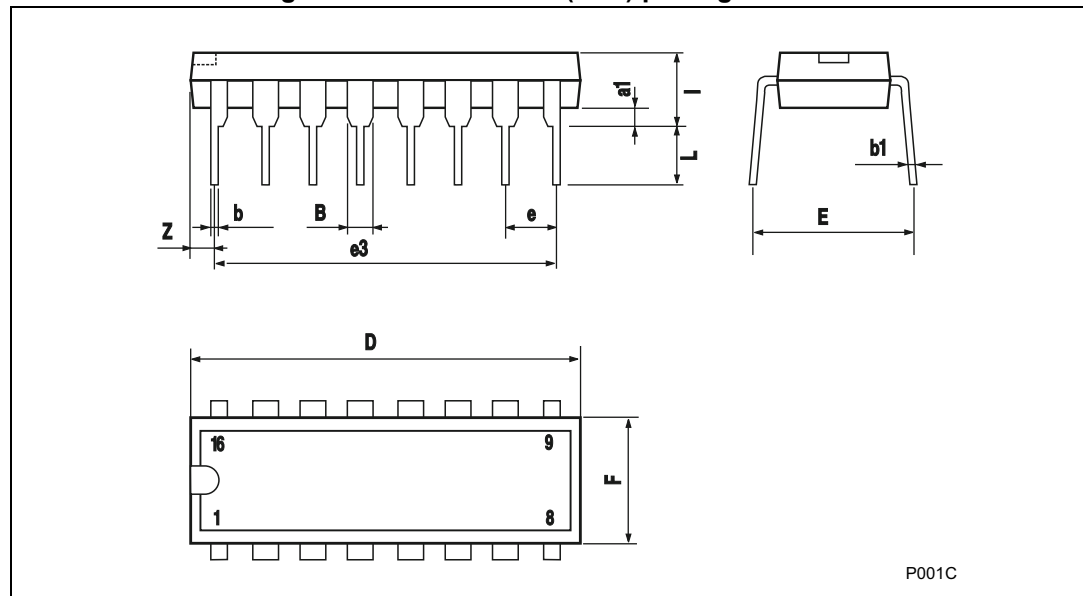
Table 6. Plastic DIP16 (0.25) package mechanical data

Symbol	Dimensions					
	mm			inch		
	Min.	Typ	Max.	Min.	Typ.	Max.
a1	0.51			0.020		
B	0.77		1.65	0.030		0.065
b		0.5			0.020	
b1		0.25			0.010	
D			20			0.787
E		8.5			0.335	
e		2.54			0.100	
e3		17.78			0.700	
F			7.1			0.280
I			5.1			0.201
L		3.3			0.130	
Z			1.27			0.050

Figure 26. SO16 package outline

0016020D
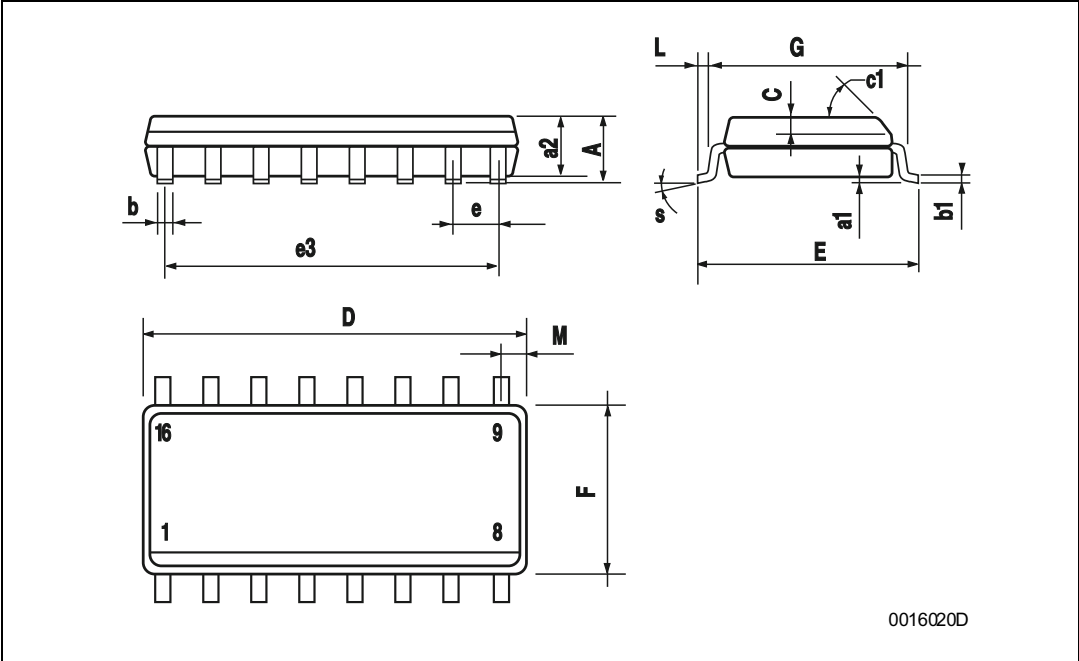
Table 7. SO16 package mechanical data

Symbol	Dimensions					
	mm			inch		
	Min.	Typ	Max.	Min.	Typ.	Max.
A			1.75			0.068
a	1 0.1		0.25	0.004		0.010
a2			1.64			0.063
b	0.35		0.46	0.013		0.018
b1	0.19		0.25	0.007		0.010
C		0.5			0.019	
c1	45° (typ.)					
D	9.8		10	0.385		0.393
E	5.8		6.2	0.228		0.244
e		1.27			0.050	
e3		8.89			0.350	
F	3.8		4.0	0.149		0.157
G	4.6		5.3	0.181		0.208
L	0.5		1.27	0.019		0.050
M			0.62			0.024
S	8° (max.)					

7 Ordering codes

Table 8. Ordering information

Order codes	Package	Packing
L6598	DIP16	Tube
L6598D	SO16N	Tube
L6598D013TR		Tape and reel

8 Revision history

Table 9. Document revision history

Date	Revision	Changes
21-Jun-2004	5	Changed the impagination following the new release of "corporate technical publication design guide". Done a few of corrections in the text.
09-Sep-2004	6	Added ordering number for the tape and reel version, updated *Table 4 on page 4*
02-Oct-2009	7	Updated *Table 4 on page 4*
18-Nov-2013	8	Added cross-reference in *Section 5*. Updated *Section 6: Package information* (reformatted - added title of *Figure 25* and *Table 6*, *Figure 26* and *Table 7* and reversed order of *figures* and *tables*, minor modifications). Updated *Table 8* (replaced L6598D016TR device by L6598D013TR device). Minor corrections throughout document.

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