1.2MHz, Low-Power 36V Op Amps

Order Information

Model Name	Order Number	Package	Transport Media, Quantity	Marking Information
LM321	LM321-TR	5-Pin SOT23	Tape and Reel, 3,000	H21
LM358	LM358-SR	8-Pin SOP	Tape and Reel, 4,000	LM358
LIVISSO	LM358-VR	8-Pin MSOP	Tape and Reel, 3,000	LM358
LM324	LM324-SR	14-Pin SOP	Tape and Reel, 2,500	LM324
	LM324-TR	14-Pin TSSOP	Tape and Reel, 3,000	LM324

Absolute Maximum Ratings Note 1

Supply Voltage: $V^+ - V^-$ Note 2	42V
Input Voltage $V^ 0.3$ to	V ⁺ + 0.3
Input Current: +IN, –IN Note 3	±20mA
Differential Input Voltage	±42V
Output Short-Circuit Duration Note 4	Infinite

Current at Supply Pins	±60mA
Operating Temperature Range40°C	to 125°C
Maximum Junction Temperature	150°C
Storage Temperature Range –65°C	to 150°C
Lead Temperature (Soldering, 10 sec)	260°C

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

Note 2: The op amp supplies must be established simultaneously, with, or before, the application of any input signals.

Note 3: The inputs are protected by ESD protection diodes to each power supply. If the input extends more than 500mV beyond the power supply, the input current should be limited to less than 10mA.

Note 4: A heat sink may be required to keep the junction temperature below the absolute maximum. This depends on the power supply voltage and how many amplifiers are shorted. Thermal resistance varies with the amount of PC board metal connected to the package. The specified values are for short traces connected to the leads.

ESD, Electrostatic Discharge Protection

Symbol	Parameter	Condition	Minimum Level	Unit
HBM	Human Body Model ESD	MIL-STD-883H Method 3015.8	2	kV
CDM	Charged Device Model ESD	JEDEC-EIA/JESD22-C101E	2	kV

Thermal Resistance

Package Type	θ _{JA}	θ _{JC}	Unit
5-Pin SOT23	250	81	°C/W
8-Pin SOP	158	43	°C/W
8-Pin MSOP	210	45	°C/W
14-Pin SOP	120	36	°C/W
14-Pin TSSOP	180	35	°C/W

Electrical Characteristics

The specifications are at $T_A = 27^{\circ}$ C. $V_S = 5$ V, $V_{CM} = V_{OUT} = 2.5$ V, $R_L = 2k\Omega$, $C_L = 100$ pF, unless otherwise noted.

SYMBOL	PARAMETER	CONDITIONS	MIN	ТҮР	MAX	UNITS
		$V_{\rm S}$ = 5 V, $V_{\rm CM}$ = 2.5V and $V_{\rm CM}$ = 0V	-3	±1	3	mV
Vos	Input Offset Voltage	V_{S} = 30 V, V_{CM} = 15V and V_{CM} = 0V	-3	±1	3	mV
Vos TC	Input Offset Voltage Drift	-40°C to 125°C		1		µV/°C
		T _A = 27 °C		60		pА
IB	Input Bias Current	T _A = 85 °C		200		pА
los	Input Offset Current			0.001		pА
Vn	Input Voltage Noise	f = 0.1Hz to 10Hz		10		μVpp
en	Input Voltage Noise Density	f = 1kHz		48		nV/√Hz
in	Input Current Noise	f = 1kHz		2		fA/√Hz
C _{IN}	Input Capacitance	Differential Common Mode		2.5 5		pF
CMRR	Common Mode Rejection Ratio	DC, V _{CM} =0V to 28V	80	120		dB
V _{CM}	Common-mode Input Voltage Range	V _S = 5 V to 30V	V-		V+-2	V
PSRR	Power Supply Rejection Ratio	$V_S = 5 V \text{ to } 30V$	90	120		dB
A _{VOL}	Open-Loop Large Signal Gain	V_{S} = 15 V, V_{O} = 1 V to 11 V, R_{L} = 2 k Ω	98	110		dB
M	Output Output from Output Dail	$R_{LOAD} = 10k\Omega$, $V_S = \pm 15 V$	14.70	14.75		V
V _{OH}	Output Swing from Supply Rail	$R_{LOAD} = 2k\Omega$, $V_S = \pm 15 V$	13.70	13.90		V
		R_{LOAD} = 10k Ω , V_S = ±15 V		-14.85	-14.70	V
Vol	Output Swing from Supply Rail	$R_{LOAD} = 2k\Omega, V_S = \pm 15 V$		-14.25	-14.10	V
		$R_{LOAD} \ge 10 \text{ k}\Omega, \text{ V}_{S} = 15 \text{ V}$		5		mV
Rout	Closed-Loop Output Impedance	$A_V = 1$, f =1kHz, $I_{OUT} = 0$		0.002		Ω
Ro	Open-Loop Output Impedance	f = 1kHz, I _{OUT} = 0		120		Ω
Isc	Output Short-Circuit Current	Sink or source current, V _S = 30V	20	35		mA
Vs	Supply Voltage		3		36	V
		V _S = 5V, No load		100	150	μA
lq	Quiescent Current per Amplifier	V _S = 30V, No load		110	200	μA
PM	Phase Margin	$R_{LOAD} = 1k\Omega, C_{LOAD} = 100pF$		62		0
GM	Gain Margin	$R_{LOAD} = 1k\Omega, C_{LOAD} = 60pF$		18		dB
GBWP	Gain-Bandwidth Product	f = 1kHz		1.2		MHz
SR	Slew Rate at unity gain	A_V = 1, V _S = ±15V, V _{OUT} = -10V to 10V, C _{LOAD} =60pF, R _{LOAD} = 10kΩ		0.55		V/µs
FPBW	Full Power Bandwidth Note 1			17.5		kHz
ts	Settling Time, 0.1% Settling Time, 0.01%	A _V = -1, V _{OUT} = 1V Step		2.8 3.1		μs
THD+N	Total Harmonic Distortion and Noise	f = 1kHz, A _V =1, R _L = 2kΩ, V _{OUT} = 1Vp-p		0.001		%
Xtalk	Channel Separation	f = 1 kHz to 20 kHz		80		dB

Note 1: Full power bandwidth is calculated from the slew rate FPBW = SR/ $\pi \cdot V_{P-P}$

1.2MHz, Low-Power 36V Op Amps Typical Performance Characteristics

 $V_S = \pm 15V$, $V_{CM} = 0V$, $R_L = Open$, unless otherwise specified.



Open-Loop Gain and Phase



Input Bias Current vs. Temperature



Unity Gain Bandwidth vs. Temperature



Input Voltage Noise Spectral Density



Input Bias Current vs. Input Common Mode Voltage



Typical Performance Characteristics

 $V_{S} = \pm 15V$, $V_{CM} = 0V$, $R_{L} = Open$, unless otherwise specified. (Continued)



Quiescent Current vs. Temperature



Power-Supply Rejection Ratio





CMRR vs. Frequency

Short Circuit Current vs. Temperature



Quiescent Current vs. Supply Voltage



1.2MHz, Low-Power 36V Op Amps Typical Performance Characteristics

 $V_{S} = \pm 15V$, $V_{CM} = 0V$, $R_{L} = Open$, unless otherwise specified. (Continued)

Power-Supply Rejection Ratio vs. Temperature

CMRR vs. Temperature



EMIRR IN+ vs. Frequency



Negative Over-Voltage Recovery



Time (50µs/div)



Small-Scale Step Response



Time (5µs/div)

Positive Over-Voltage Recovery



Time (50µs/div)

Typical Performance Characteristics

 $V_{S}=\pm15V,\,V_{CM}$ = 0V, R_{L} = Open, unless otherwise specified. (Continued)

0.1 Hz TO 10 Hz Input Voltage Noise



Time (1s/div)

Large-Scale Step Response



Time (20µs/div)

Negative Output Swing vs. Load Current



Offset Voltage vs Common-Mode Voltage



Positive Output Swing vs. Load Current



Pin Functions

-IN: Inverting Input of the Amplifier.
+IN: Non-Inverting Input of Amplifier.
OUT: Amplifier Output. The voltage range extends to within mV of each supply rail.
V+ or +V_s: Positive Power Supply. Typically the voltage is from 3V to 36V. Split supplies are possible as long as the voltage between V+ and V- is between 3V and 36V. A bypass capacitor of 0.1µF as close to the part as

possible should be used between power supply pins or between supply pins and ground.

V- or -V_s: Negative Power Supply. It is normally tied to ground. It can also be tied to a voltage other than ground as long as the voltage between V₊ and V₋ is from 3V to 36V. If it is not connected to ground, bypass it with a capacitor of 0.1μ F as close to the part as possible.

Operation

The LM321/358/324 output signal range extends beyond the negative and positive power supplies. The intput can even extend all the way to the negative supply. The Class-AB control buffer and output bias stage uses a proprietary compensation technique to take full advantage of the process technology to drive very high capacitive loads. This is evident from the transient over shoot measurement plots in the Typical Performance Characteristics.

Applications Information

High Supply Voltage and Low Power Consumption

The LM321/358/324 of operational amplifiers can operate with power supply voltages from 3V to 36V. Each amplifier draws only 100µA quiescent current. The low supply voltage capability and low supply current are ideal for portable applications demanding HIGH CAPACITIVE LOAD DRIVING CAPABILITY and WIDE BANDWIDTH. The LM321/358/324 is optimized for wide bandwidth low power applications. They have an industry leading high GBWP to power ratio and are unity gain stable for 10nf CAPACITIVE load. When the load capacitance increases, the increased capacitance at the output pushed the non-dominant pole to lower frequency in the open loop frequency response, lowering the phase and gain margin. Higher gain configurations tend to have better capacitive drive capability than lower gain configurations due to lower closed loop bandwidth and hence higher phase margin.

Low Input Referred Noise

The LM321/358/324 provides a low input referred noise density of $48nV/\sqrt{Hz}$ at 1kHz. The voltage noise will grow slowly with the frequency in wideband range, and the input voltage noise is typically $10\mu V_{P-P}$ at the frequency of 0.1Hz to 10Hz.

Low Input Offset Voltage

The LM321/358/324 has a low offset voltage tolerance of 3mV maximum which is essential for precision applications. The offset voltage is trimmed with a proprietary trim algorithm to ensure low offset voltage for precision signal processing requirement.

Low Input Bias Current

The LM321/358/324 is a CMOS OPA family and features very low input bias current in pA range. The low input bias current allows the amplifiers to be used in applications with high resistance sources. Care must be taken to minimize PCB Surface Leakage. See below section on "PCB Surface Leakage" for more details.

PCB Surface Leakage

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LM321/LM358/LM324

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In applications where low input bias current is critical, Printed Circuit Board (PCB) surface leakage effects need to be considered. Surface leakage is caused by humidity, dust or other contamination on the board. Under low humidity conditions, a typical resistance between nearby traces is $10^{12}\Omega$. A 5V difference would cause 5pA of current to flow, which is greater than the LM321/358/324 OPA's input bias current at +27°C (±1pA, typical). It is recommended to use multi-layer PCB layout and route the OPA's -IN and +IN signal under the PCB surface.

The effective way to reduce surface leakage is to use a guard ring around sensitive pins (or traces). The guard ring is biased at the same voltage as the sensitive pin. An example of this type of layout is shown in Figure 1 for Inverting Gain application.

- 1. For Non-Inverting Gain and Unity-Gain Buffer:
 - a) Connect the non-inverting pin (V_{IN} +) to the input with a wire that does not touch the PCB surface.
 - b) Connect the guard ring to the inverting input pin (V_{IN}–). This biases the guard ring to the Common Mode input voltage.
- 2. For Inverting Gain and Trans-impedance Gain Amplifiers (convert current to voltage, such as photo detectors):
 - a) Connect the guard ring to the non-inverting input pin (V_{IN} +). This biases the guard ring to the same reference voltage as the op-amp (e.g., $V_S/2$ or ground).
 - b) Connect the inverting pin (V_{IN} -) to the input with a wire that does not touch the PCB surface.





Ground Sensing and Rail to Rail Output

The LM321/358/324 has excellent output drive capability, delivering over 35mA of output drive current. The output stage is a rail-to-rail topology that is capable of swinging to within 5mV of either rail. Since the inputs can go 100mV beyond either rail, the op-amp can easily perform 'True Ground Sensing'.

The maximum output current is a function of total supply voltage. As the supply voltage to the amplifier increases, the output current capability also increases. Attention must be paid to keep the junction temperature of the IC below 150°C when the output is in continuous short-circuit. The output of the amplifier has reverse-biased ESD diodes connected to each supply. The output should not be forced more than 0.5V beyond either supply, otherwise current will flow through these diodes.

ESD

The LM321/358/324 has reverse-biased ESD protection diodes on all inputs and output. Input and out pins cannot be biased more than 200mV beyond either supply rail.

Feedback Components and Suppression of Ringing

Care should be taken to ensure that the pole formed by the feedback resistors and the parasitic capacitance at the inverting input does not degrade stability. For example, in a gain of +2 configuration with gain and feedback resistors of 10k, a poorly designed circuit board layout with parasitic capacitance of 5pF (part +PC board) at the amplifier's inverting input will cause the amplifier to ring due to a pole formed at 1.2MHz. An additional capacitor of 5pF across the feedback resistor as shown in Figure 2 will eliminate any ringing.

Careful layout is extremely important because low power signal conditioning applications demand high-impedance circuits. The layout should also minimize stray capacitance at the OPA's inputs. However some stray capacitance may be unavoidable and it may be necessary to add a 2pF to 10pF capacitor across the feedback resistor. Select the smallest capacitor value that ensures stability.





Driving Large Capacitive Load

The LM321/358/324 of OPA is designed to drive large capacitive loads. Refer to Typical Performance Characteristics for "Phase Margin vs. Load Capacitance". As always, larger load capacitance decreases overall phase margin in a feedback system where internal frequency compensation is utilized. As the load capacitance increases, the feedback loop's phase margin decreases, and the closed-loop bandwidth is reduced. This produces gain peaking in the frequency response, with overshoot and ringing in output step response. The unity-gain buffer (G = +1V/V) is the most sensitive to large capacitive loads.

When driving large capacitive loads with the LM321/358/324 (e.g., > 200 pF when G = +1V/V), a small series resistor at the output (R_{ISO} in Figure 3) improves the feedback loop's phase margin and stability by making the output load resistive at higher frequencies.



Power Supply Layout and Bypass

The LM321/358/324 OPA's power supply pin should have a local bypass capacitor (i.e., 0.01μ F to 0.1μ F) within 2mm for good high frequency performance. It can also use a bulk capacitor (i.e., 1μ F or larger) within 100mm to provide large, slow currents. This bulk capacitor can be shared with other analog parts.

Ground layout improves performance by decreasing the amount of stray capacitance and noise at the OPA's inputs and outputs. To decrease stray capacitance, minimize PC board lengths and resistor leads, and place external components as close to the op amps' pins as possible.

Proper Board Layout

To ensure optimum performance at the PCB level, care must be taken in the design of the board layout. To avoid leakage currents, the surface of the board should be kept clean and free of moisture. Coating the surface creates a barrier to moisture accumulation and helps reduce parasitic resistance on the board.

Keeping supply traces short and properly bypassing the power supplies minimizes power supply disturbances due to output current variation, such as when driving an ac signal into a heavy load. Bypass capacitors should be connected as closely as possible to the device supply pins. Stray capacitances are a concern at the outputs and the inputs of the amplifier. It is recommended that signal traces be kept at least 5mm from supply lines to minimize coupling.

A variation in temperature across the PCB can cause a mismatch in the Seebeck voltages at solder joints and other points where dissimilar metals are in contact, resulting in thermal voltage errors. To minimize these thermocouple effects, orient resistors so heat sources warm both ends equally. Input signal paths should contain matching numbers

and types of components, where possible to match the number and type of thermocouple junctions. For example, dummy components such as zero value resistors can be used to match real resistors in the opposite input path. Matching components should be located in close proximity and should be oriented in the same manner. Ensure leads are of equal length so that thermal conduction is in equilibrium. Keep heat sources on the PCB as far away from amplifier input circuitry as is practical.

The use of a ground plane is highly recommended. A ground plane reduces EMI noise and also helps to maintain a constant temperature across the circuit board.

Instrumentation Amplifier

The LM321/358/324 OPA is well suited for conditioning sensor signals in battery-powered applications. Figure 4 shows a two op-amp instrumentation amplifier, using the LM321/358/324 OPA.

The circuit works well for applications requiring rejection of Common Mode noise at higher gains. The reference voltage (V_{REF}) is supplied by a low-impedance source. In single voltage supply applications, V_{REF} is typically $V_S/2$.



Two-Pole Micro-power Sallen-Key Low-Pass Filter

Figure 5 shows a micro-power two-pole Sallen-Key Low-Pass Filter with 400Hz cut-off frequency. For best results, the filter's cut-off frequency should be 8 to 10 times lower than the OPA's crossover frequency. Additional OPA's phase margin shift can be avoided if the OPA's bandwidth-to-signal ratio is greater than 8. The design equations for the 2-pole Sallen-Key low-pass filter are given below with component values selected to set a 400Hz low-pass filter cutoff frequency:





Package Outline Dimensions

SC70-5 /SOT-353



	Dimens	sions	Dimens	sions
Symbol	In Millimeters		In Inch	es
	Min	Max	Min	Max
А	0.900	1.100	0.035	0.043
A1	0.000	0.100	0.000	0.004
A2	0.900	1.000	0.035	0.039
b	0.150	0.350	0.006	0.014
С	0.080	0.150	0.003	0.006
D	2.000	2.200	0.079	0.087
E	1.150	1.350	0.045	0.053
E1	2.150	2.450	0.085	0.096
е	0.650T	ΥP	0.026T	ΥP
e1	1.200	1.400	0.047	0.055
L	0.525R	EF	0.021R	EF
L1	0.260	0.460	0.010	0.018
θ	0°	8°	0°	8°

SOT23-5



Package Outline Dimensions

SOP-8



1.2MHz, Low-Power 36V Op Amps Package Outline Dimensions

MSOP-8



	Dimensior	IS	Dimensions	In
Symbol	In Millimet	ers	Inches	
	Min	Max	Min	Max
А	0.800	1.200	0.031	0.047
A1	0.000	0.200	0.000	0.008
A2	0.760	0.970	0.030	0.038
b	0.30 TYP		0.012 TYP	
С	0.15 TYP		0.006 TYP	
D	2.900	3.100	0.114	0.122
е	0.65 TYP		0.026	
E	2.900	3.100	0.114	0.122
E1	4.700	5.100	0.185	0.201
L1	0.410	0.650	0.016	0.026
θ	0°	6°	0°	6°

Package Outline Dimensions

TSSOP-14



	Dimensions			
Symbol		In Millimeters		
Symbol	MIN	ТҮР	MAX	
А	-	-	1.20	
A1	0.05	-	0.15	
A2	0.90	1.00	1.05	
b	0.20	-	0.28	
С	0.10	-	0.19	
D	4.86	4.96	5.06	
E	6.20	6.40	6.60	
E1	4.30	4.40	4.50	
е		0.65 BSC		
L	0.45	0.60	0.75	
L1		1.00 REF		
L2		0.25 BSC		
R	0.09	-	-	
θ	0°	-	8°	

1.2MHz, Low-Power 36V Op Amps Package Outline Dimensions

SOP-14

