

LT3463/LT3463A

ABSOLUTE MAXIMUM RATINGS

(Note 1)

| | |
|--|----------------|
| V_{IN} , $\overline{SHDN1}$, $\overline{SHDN2}$ Voltage | 15V |
| SW1, SW2, V_{OUT1} Voltage | 42V |
| D2 Voltage | -42V |
| FB1, FB2 Voltage Range | -0.3V to 2V |
| Junction Temperature | 125°C |
| Operating Ambient Temperature Range | |
| (Note 2) | -40°C to 85°C |
| Storage Temperature Range | -65°C to 125°C |

PACKAGE/ORDER INFORMATION

| | |
|--|-------------------------|
| <p>TOP VIEW</p> <p>DD PACKAGE 10-LEAD (3mm × 3mm) PLASTIC DFN $T_{JMAX} = 125^{\circ}\text{C}$, $\theta_{JA} = 43^{\circ}\text{C/W}$, $\theta_{JC} = 3^{\circ}\text{C/W}$ EXPOSED PAD (PIN 11) IS GND AND MUST BE SOLDERED TO PCB</p> | ORDER PART NUMBER |
| | LT3463EDD LT3463AEDD |
| | DD PART MARKING |
| | LAFC LBJK |

Consult LTC Marketing for parts specified with wider operating temperature ranges.

ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^{\circ}\text{C}$. $V_{IN} = 2.5\text{V}$, $V_{\overline{SHDN}} = 2.5\text{V}$ unless otherwise noted.

| PARAMETER | CONDITIONS | MIN | TYP | MAX | UNITS |
|--|--|------------|------------|------------|--------------------------------|
| Minimum Input Voltage | | | 2.2 | 2.4 | V |
| Total Quiescent Current | For Both Switchers, Not Switching | | 40 | 60 | μA |
| Shutdown Current | $V_{\overline{SHDN1}} = V_{\overline{SHDN2}} = 0\text{V}$ | | 0.1 | 1 | μA |
| V_{REF} Pin Voltage | With 124k Ω to GND | ● 1.23 | 1.25 | 1.27 | V |
| V_{REF} Pin Voltage Line Regulation | With 124k Ω to GND | | 0.05 | 0.10 | %/V |
| FB1 Comparator Trip Voltage | High to Low Transition | ● 1.225 | 1.25 | 1.275 | V |
| FB1 Comparator Hysteresis | | | 8 | | mV |
| FB1 Line Regulation | $2.5\text{V} < V_{IN} < 15\text{V}$ | | 0.05 | 0.10 | %/V |
| FB1 Pin Bias Current (Note 3) | $V_{FB1} = 1.3\text{V}$ | ● | 20 | 50 | nA |
| FB2 Comparator Trip Voltage | Low to High Transition | ● 0 | 3 | 12 | mV |
| FB2 Comparator Hysteresis | | | 8 | | mV |
| FB2 Line Regulation ($V_{REF} - V_{FB2}$) | $2.5\text{V} < V_{IN} < 15\text{V}$ | | 0.05 | 0.10 | %/V |
| FB2 Pin Bias Current (Note 4) | $V_{FB2} = -0.1\text{V}$ | ● | 20 | 50 | nA |
| SW1 Switch Off Time | $V_{OUT1} - V_{IN} = 4\text{V}$ $V_{OUT1} - V_{IN} = 0\text{V}$ | | 300 1.5 | | ns μs |
| SW2 Switch Off Time | $V_{FB2} < 0.1\text{V}$ $V_{FB2} = 1\text{V}$ | | 300 1.5 | | ns μs |
| Switch V_{CESAT} (SW1, SW2) | $I_{SW} = 150\text{mA}$ | | 180 | | mV |
| Switch Current Limit (SW1) | | 180 | 250 | 320 | mA |
| Switch Current Limit (SW2) | LT3463 LT3463A | 180 320 | 250 400 | 320 460 | mA mA |
| Switch Leakage Current (SW1, SW2) | Switch Off, $V_{SW} = 42\text{V}$ | | 0.01 | 1 | μA |
| Schottky Forward Voltage (V_{OUT1} , D2) | $I_D = 150\text{mA}$ | | 750 | | mV |
| Schottky Reverse Leakage Current | $V_{OUT1} - V_{SW} = 42\text{V}$ $V_{D2} = -42\text{V}$ | | 1 1 | 5 5 | μA μA |
| $\overline{SHDN1}$ Pin Current | $V_{\overline{SHDN1}} = 2.5\text{V}$ | | 4 | 10 | μA |
| $\overline{SHDN2}$ Pin Current | $V_{\overline{SHDN2}} = 2.5\text{V}$ | | 4 | 10 | μA |
| $\overline{SHDN1}/\overline{SHDN2}$ Start-Up Threshold | | 0.3 | 1 | 1.5 | V |

Note 1: Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.

Note 2: The LT3463/LT3463A are guaranteed to meet performance specifications from 0°C to 70°C. Specifications over the -40°C to 85°C

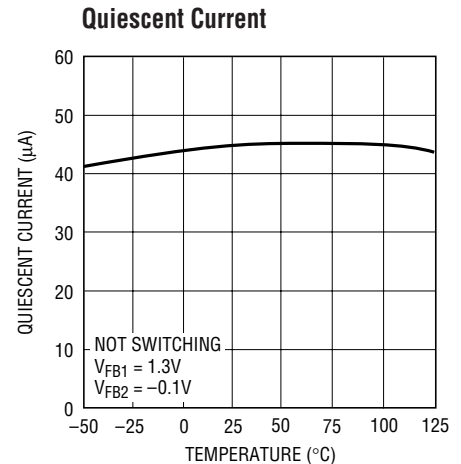
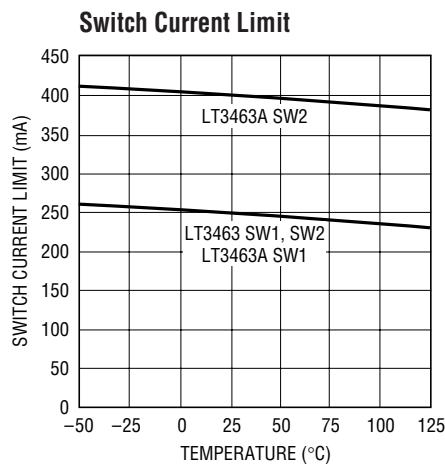
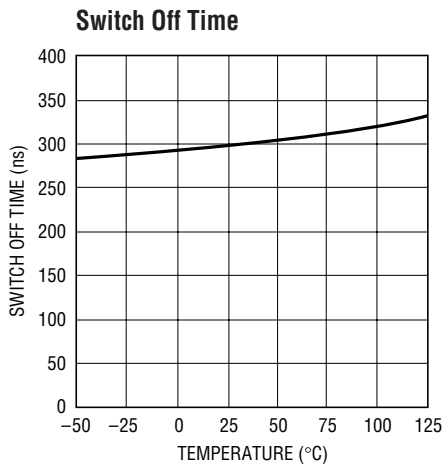
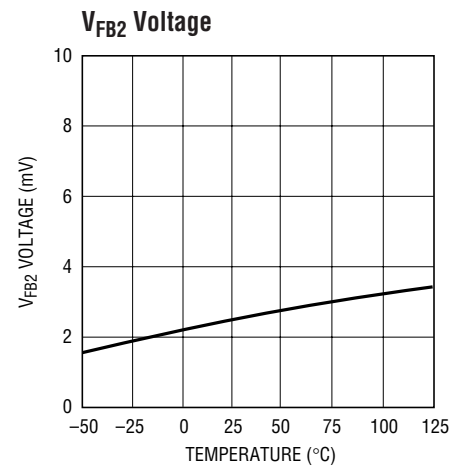
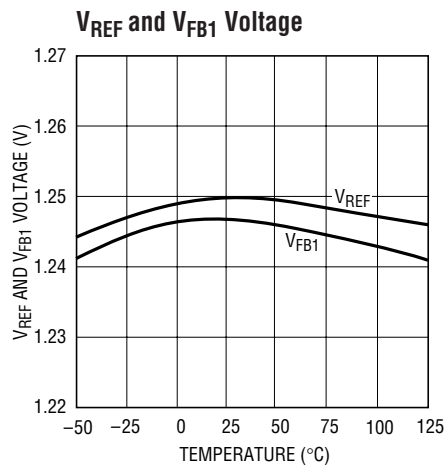
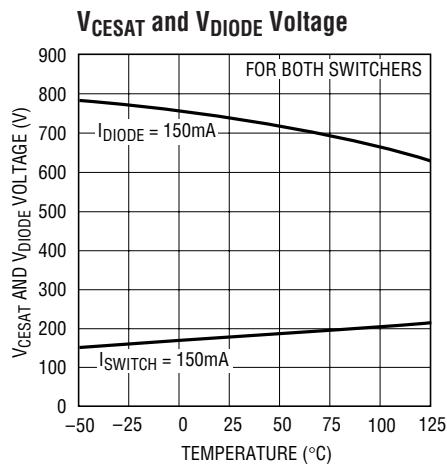
operating ambient temperature range are assured by design, characterization and correlation with statistical process controls.

Note 3: Bias current flows into the FB1 pin.

Note 4: Bias current flows out of the FB2 pin.

3463f

TYPICAL PERFORMANCE CHARACTERISTICS



PIN FUNCTIONS

V_{OUT1} (Pin 1): Output Voltage Switcher 1. This is the cathode of an internal Schottky diode whose anode is connected to the SW1 pin.

SW1 (Pin 2): Switch Pin for Switcher 1. This is the collector of the internal NPN switch. Minimize the metal trace area connected to this pin to minimize EMI.

V_{IN} (Pin 3): Input Supply Pin. Bypass this pin with a capacitor as close to the device as possible.

SW2 (Pin 4): Switch Pin for Switcher 2. This is the collector of the internal NPN switch. Minimize the metal trace area connected to this pin to minimize EMI.

D2 (Pin 5): Diode for Switcher 2. This is the anode of an internal Schottky diode whose cathode connected to the GND pin.

FB2 (Pin 6): Feedback Pin for Switcher 2. Set the output voltage by selecting values for R3 and R4.

V_{REF} (Pin 7): Voltage Reference Pin (1.25V). This pin is used along with FB2 to set the negative output voltage for Switcher 2.

SHDN2 (Pin 8): Shutdown Pin for Switcher 2. Pull this pin above 1.5V to enable Switcher 2. Pull below 0.3V to turn it off. Do not leave this pin floating.

PIN FUNCTIONS

SHDN1 (Pin 9): Shutdown Pin for Switcher 1. Pull this pin above 1.5V to enable Switcher 1. Pull below 0.3V to turn it off. Do not leave this pin floating.

FB1 (Pin 10): Feedback Pin for Switcher 1. Set the output voltage by selecting values for R1 and R2.

GND (Pin 11): Exposed Pad. Solder this exposed pad directly to the local ground plane. This pad must be electrically connected for proper operation.

BLOCK DIAGRAM

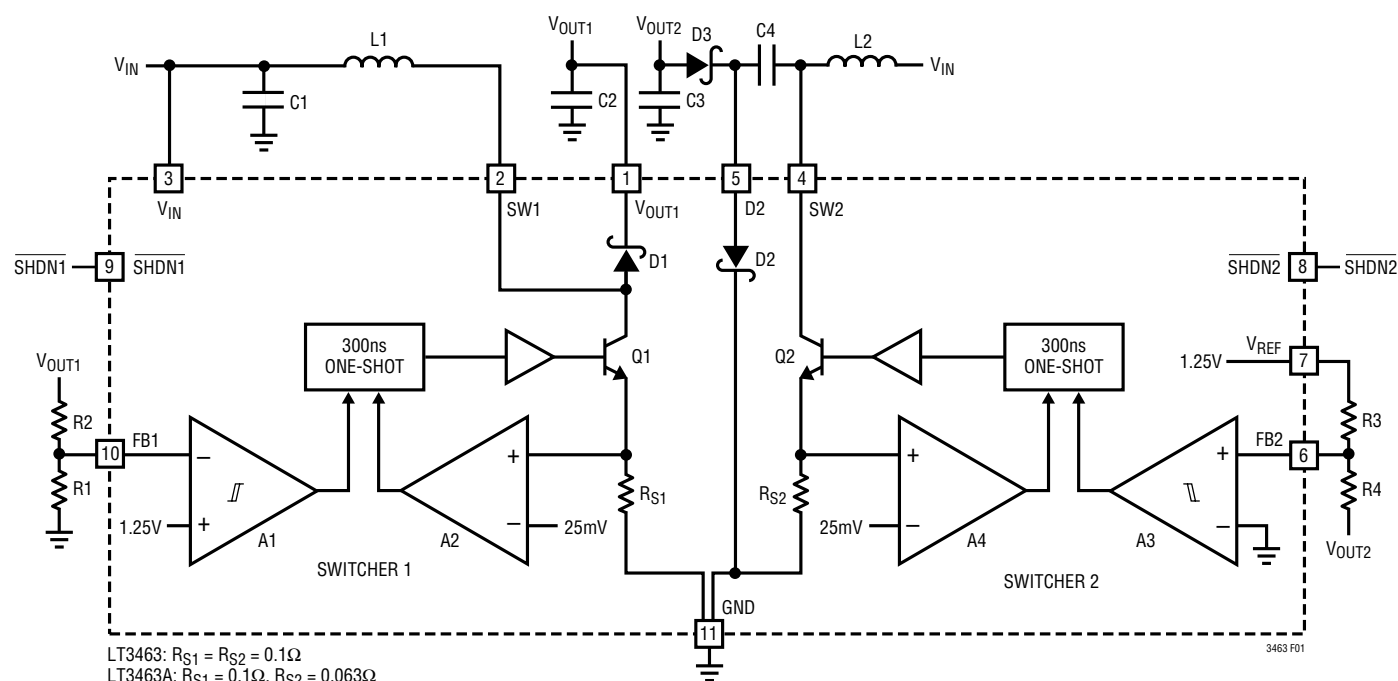


Figure 1. Block Diagram

OPERATION

The LT3463 uses a constant off-time control scheme to provide high efficiency over a wide range of output current. Operation can be best understood by referring to the block diagram in Figure 1. When the voltage at the FB1 pin is slightly above 1.25V, comparator A1 disables most of the internal circuitry. Output current is then provided by capacitor C2, which slowly discharges until the voltage at the FB1 pin goes below the hysteresis point of A1 (typical hysteresis at the FB1 pin is 8mV). A1 then enables the internal circuitry, turns on power switch Q1, and the

current in inductor L1 begins ramping up. Once the switch current reaches 250mA, comparator A2 resets the one-shot, which turns off Q1 for 300ns. Q1 turns on again and the inductor currents ramp back up to 250mA, then A2 again resets the one-shot. This switching action continues until the output voltage is charged up (until the FB1 pin reaches 1.25V), then A1 turns off the internal circuitry and the cycle repeats. The second switching regulator is an inverting converter (which generates a negative output) but the basic operation is the same.

APPLICATIONS INFORMATION

Choosing an Inductor

Several recommended inductors that work well with the LT3463 are listed in Table 1, although there are many other manufacturers and devices that can be used. Consult each manufacturer for more detailed information and for their entire selection of related parts. Many different sizes and shapes are available. Use the equations and recommendations in the next few sections to find the correct inductance value for your design.

Table 1. Recommended Inductors

| PART | L (μH) | MAX I _{DC} (mA) | MAX DCR(Ω) | HEIGHT (mm) | MANUFACTURER |
|----------|--------|-----------------------------|---------------|----------------|--|
| CMD4D06 | 4.7 | 750 | 0.22 | 0.8 | Sumida (847) 956-0666 www.sumida.com |
| | 10 | 500 | 0.46 | | |
| | 22 | 310 | 1.07 | | |
| CDRH3D16 | 10 | 500 | 0.19 | 1.8 | Sumida |
| | 22 | 310 | 0.36 | | |
| LPO4812 | 4.7 | 600 | 0.16 | 1.2 | Coilcraft (847) 639-6400 www.coilcraft.com |
| | 10 | 400 | 0.30 | | |
| | 22 | 280 | 0.64 | | |
| LQH32C | 10 | 450 | 0.39 | 1.8 | Murata (714) 852-2001 www.murata.com |
| | 15 | 300 | 0.75 | | |
| | 22 | 250 | 0.92 | | |
| LQH31C | 4.7 | 340 | 0.85 | 1.8 | Murata |

Inductor Selection—Boost Regulator

The formula below calculates the appropriate inductor value to be used for a boost regulator using the LT3463 (or at least provides a good starting point). This value provides a good tradeoff in inductor size and system performance. Pick a standard inductor close to this value. A larger value can be used to slightly increase the available output current, but limit it to around twice the value calculated below, as too large of an inductance will increase the output voltage ripple without providing much additional output current. A smaller value can be used (especially for systems with output voltages greater than 12V) to give a smaller physical size. Inductance can be calculated as:

$$L = \frac{V_{OUT} - V_{IN(MIN)} + V_D}{I_{LIM}} t_{OFF}$$

where $V_D = 0.5V$ (Schottky diode voltage), $I_{LIM} = 250mA$ (or 400mA) and $t_{OFF} = 300ns$; for designs with varying V_{IN}

such as battery powered applications, use the minimum V_{IN} value in the above equation. For most regulators with output voltages below 7V, a 4.7μH inductor is the best choice, even though the equation above might specify a smaller value.

For higher output voltages, the formula above will give large inductance values. For a 3V to 20V converter (typical LCD Bias application), a 21μH inductor is called for with the above equation, but a 10μH inductor could be used without much reduction in the maximum output current.

Inductor Selection—Inverting Regulator

The formula below calculates the appropriate inductor value to be used for an inverting regulator using the LT3463 (or at least provides a good starting point). This value provides a good tradeoff in inductor size and system performance. Pick a standard inductor close to this value (both inductors should be the same value). A larger value can be used to slightly increase the available output current, but limit it to around twice the value calculated below, as too large of an inductance will increase the output voltage ripple without providing much additional output current. A smaller value can be used (especially for systems with output voltages greater than 12V) to give a smaller physical size. Inductance can be calculated as:

$$L = 2 \left(\frac{|V_{OUT}| + V_D}{I_{LIM}} \right) t_{OFF}$$

where $V_D = 0.5V$ (Schottky diode voltage), $I_{LIM} = 250mA$ (or 400mA) and $t_{OFF} = 300ns$.

For higher output voltages, the formula above will give large inductance values. For a 3V to 20V converter (typical LCD bias application), a 49μH inductor is called for with the above equation, but a 10μH or 22μH inductor could be used without much reduction in the maximum output current.

Inductor Selection—Inverting Charge Pump Regulator

For the inverting regulator, the voltage seen by the internal power switch is equal to the sum of the absolute value of the input and output voltages, so that generating high

APPLICATIONS INFORMATION

output voltages from a high input voltage source will often exceed the 50V maximum switch rating. For instance, a 12V to –40V converter using the inverting topology would generate 52V on the SW pin, exceeding its maximum rating. For this application, an inverting charge pump is the best topology.

The formula below calculates the approximate inductor value to be used for an inverting charge pump regulator using the LT3463. As for the boost inductor selection, a larger or smaller value can be used. For designs with varying V_{IN} such as battery powered applications, use the minimum V_{IN} value in the equation below.

$$L = \frac{|V_{OUT}| - V_{IN(MIN)} + V_D}{I_{LIM}} t_{OFF}$$

Capacitor Selection

The small size and low ESR of ceramic capacitors makes them ideal for LT3463 applications. Use only X5R and X7R types because they retain their capacitance over wider voltage and temperature ranges than other ceramic types. A 1 μ F input capacitor and a 0.22 μ F or 0.47 μ F output capacitor are sufficient for most applications. Table 2 shows a list of several ceramic capacitor manufacturers. Consult the manufacturers for more detailed information on their entire selection of ceramic capacitors. For applications needing very low output voltage ripple, larger output capacitor values can be used.

Table 2. Recommended Ceramic Capacitor Manufacturers

| MANUFACTURER | PHONE | URL |
|--------------|--------------|--|
| AVX | 843-448-9411 | www.avxcorp.com |
| Kemet | 408-986-0424 | www.kemet.com |
| Murata | 814-237-1431 | www.murata.com |
| Taiyo Yuden | 408-573-4150 | www.t-yuden.com |

Inrush Current

When V_{IN} is increased from ground to operating voltage while the output capacitor is discharged, an inrush current will flow through the inductor and integrated Schottky diode into the output capacitor. Conditions that increase

inrush current include a larger more abrupt voltage step at V_{IN} , a larger output capacitor tied to the outputs, and an inductor with a low saturation current.

While the internal diode is designed to handle such events, the inrush current should not be allowed to exceed 1 amp. For circuits that use output capacitor values within the recommended range and have input voltages of less than 5V, inrush current remains low, posing no hazard to the device. In cases where there are large steps at V_{IN} and/or a large capacitor is used at the outputs, inrush current should be measured to ensure safe operation.

Setting the Output Voltages

The output voltages are programmed using two feedback resistors. As shown in Figure 1, resistors R1 and R2 program the positive output voltage (for Switcher 1), and resistors R3 and R4 program the negative output voltage (for Switcher 2) according to the following formulas:

$$V_{OUT1} = 1.25V \left(1 + \frac{R2}{R1} \right)$$

$$V_{OUT2} = -1.25V \left(\frac{R4}{R3} \right)$$

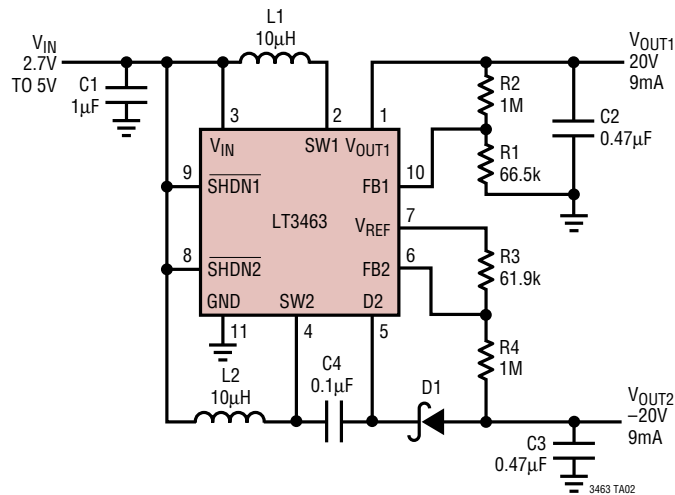
R1 and R3 are typically 1% resistors with values in the range of 50k to 250k.

Board Layout Considerations

As with all switching regulators, careful attention must be paid to the PCB board layout and component placement. To maximize efficiency, switch rise and fall times are made as short as possible. To prevent electromagnetic interference (EMI) problems, proper layout of the high frequency switching path is essential. The voltage signal of the SW pin has sharp rising and falling edges. Minimize the length and area of all traces connected to the SW pin and always use a ground plane under the switching regulator to minimize interplane coupling. In addition, the ground connection for the feedback resistor R1 should be tied directly to the GND pin and not shared with any other component, ensuring a clean, noise-free connection.

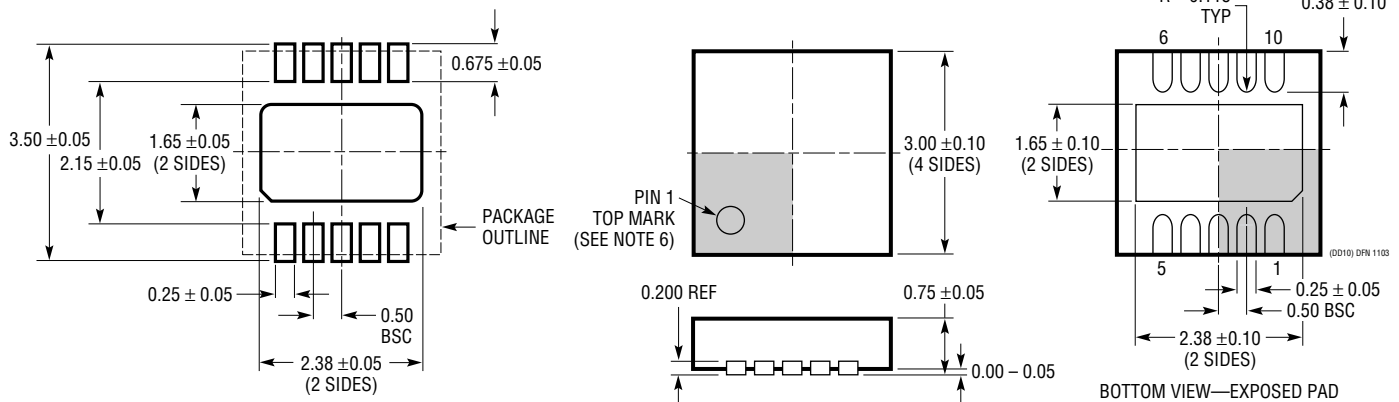
TYPICAL APPLICATION

Dual Output $\pm 20V$ Converter



PACKAGE DESCRIPTION

DD Package 10-Lead Plastic DFN (3mm × 3mm) (Reference LTC DWG # 05-08-1699)



RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS

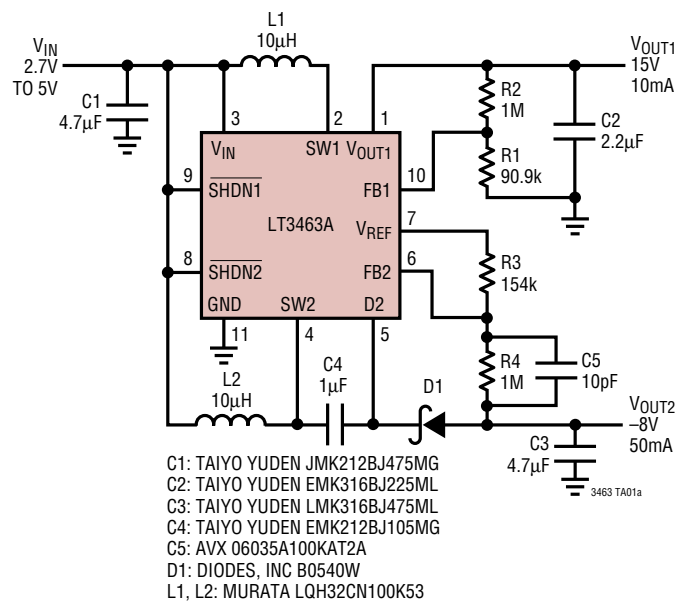
NOTE:

1. DRAWING TO BE MADE A JEDEC PACKAGE OUTLINE MO-229 VARIATION OF (WEED-2). CHECK THE LTC WEBSITE DATA SHEET FOR CURRENT STATUS OF VARIATION ASSIGNMENT
2. DRAWING NOT TO SCALE
3. ALL DIMENSIONS ARE IN MILLIMETERS
4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE

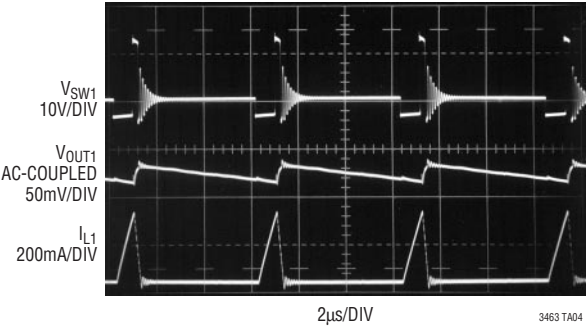
5. EXPOSED PAD SHALL BE SOLDER PLATED
6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE

TYPICAL APPLICATION

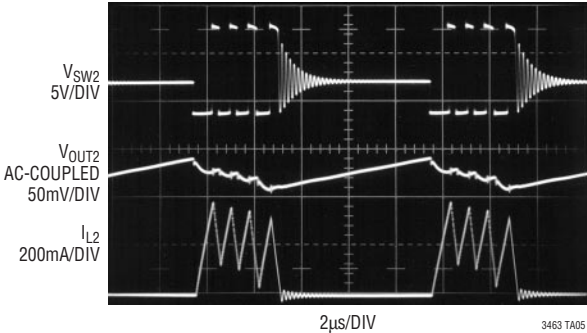
CCD Bias Supply



Typical Waveforms for 15V Output



Typical Waveforms for -8V Output



RELATED PARTS

| PART NUMBER | DESCRIPTION | COMMENTS |
|-----------------|---|--|
| LT1615/LT1615-1 | 300mA/80mA (ISW), High Efficiency Step-Up DC/DC Converters | VIN: 1V to 15V, VOUT(MAX): 34V, IQ: 20µA, ISD: <1µA, ThinSOT Package |
| LT1944 | Dual Output 350mA (ISW), Constant Off-Time, High Efficiency Step-Up DC/DC Converter | VIN: 1.2V to 15V, VOUT(MAX): 34V, IQ: 20µA, ISD: <1µA, MS Package |
| LT1944-1 | Dual Output 150mA (ISW), Constant Off-Time, High Efficiency Step-Up DC/DC Converter | VIN: 1.2V to 15V, VOUT(MAX): 34V, IQ: 20µA, ISD: <1µA, MS Package |
| LT1945 | Dual Output, Pos/Neg, 350mA (ISW), Constant Off-Time, High Efficiency Step-Up DC/DC Converter | VIN: 1.2V to 15V, VOUT(MAX): ±34V, IQ: 20µA, ISD: <1µA, MS Package |
| LT3464 | 85mA (ISW), High Efficiency Step-Up DC/DC Converter with Integrated Schottky and PNP Disconnect | VIN: 2.3V to 10V, VOUT(MAX): 34V, IQ: 25µA, ISD: <1µA, ThinSOT Package |