Contents TSM1014

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TSM1014 Pin descriptions

1 Pin descriptions

Table 2 gives the pin descriptions for the SO-8 package.

Table 2. Pin descriptions

Name	Pin no.	Туре	Function
V_{Ref}	1	Analog output	Voltage reference
Cc-	2	Analog input	Input pin of the operational amplifier
Cc+	3	Analog input	Input pin of the operational amplifier
CV-	4	Analog input	Input pin of the operational amplifier
CV _{OUT}	5	Analog output	Output of the operational amplifier
GND	6	Power supply	Ground line. 0 V reference for all voltages.
CC _{OUT}	7	Analog output	Output of the operational amplifier
VCC	8	Power supply	Power supply line

2 Absolute maximum ratings

Table 3. Absolute maximum ratings

Symbol	DC supply voltage	Value	Unit
VCC	DC supply voltage (50 mA =< I _{CC})	-0.3V to Vz	V
Vi	Input voltage	-0.3 to VCC	V
Toper	Operational temperature	-40 to 105	°C
Tstg	Storage temperature	-55 to 150	°C
Tj	Junction temperature	150	°C
Iref	Voltage reference output current	2.5	mA
ESD	Electrostatic discharge	2	kV
Rthja	Thermal resistance junction to ambient SO8 package	175	°C/W

3 Operating conditions

Table 4. Operating conditions

Symbol	Parameter	Value	Unit
VCC	DC supply conditions	4.5 to Vz	V
Toper	Operational temperature	-40 to 105	°C



Electrical characteristics TSM1014

4 Electrical characteristics

 T_{amb} = 25 °C and VCC = +18 V (unless otherwise specified).

Table 5. Electrical characteristics

Symbol	Parameter	Test condition	Min.	Тур.	Max.	Unit	
Total curre	Total current consumption						
I _{CC}	Total supply current, excluding current in voltage reference ⁽¹⁾	VCC = 18 V, no load $T_{min.} < T_{amb} < T_{max}$.		100	180	μA	
Vz	VCC clamp voltage	I _{CC} = 50 mA		28		V	
Operator 1	: Op Amp with non-inverting input conne	ected to the internal V _{Re}	ef	•	1		
V _{Ref} + V _{io}	Input offset voltage + voltage reference TSM1014 TSM1014A	$\begin{split} T_{amb} &= 25~^{\circ}\text{C} \\ T_{min.} &\leq T_{amb} \leq T_{max.} \\ T_{amb} &= 25~^{\circ}\text{C} \\ T_{min.} &\leq T_{amb} \leq T_{max.} \end{split}$		1.251 1.25	1.266 1.279 1.258 1.267	V	
DV _{io}	Input offset voltage drift			7		μV/°C	
Operator 2	2	I		I			
V _{io}	Input offset voltage TSM1014 TSM1014A	T_{amb} = 25 °C $T_{min.} \le T_{amb} \le T_{max.}$ T_{amb} = 25 °C $T_{min.} \le T_{amb} \le T_{max.}$		1 0.5	4 5 2 3	mV	
DV _{io}	Input offset voltage drift			7		μV/°C	
l _{ib}	Input bias current	T_{amb} = 25 °C $T_{min.} \le T_{amb} \le T_{max.}$		20 50	150 200	nA	
SVR	Supply voltage rejection ration	VCC = 4.5 V to 28 V	65	100		dB	
Vicm	Input common mode voltage range		0		VCC -1.5	V	
CMR	Common mode rejection ratio	T_{amb} = 25 °C $T_{min.} \le T_{amb} \le T_{max.}$	70 60	85		dB	
Output sta	Output stage						
Gm	Transconduction gain. Sink current only ⁽²⁾	T_{amb} = 25 °C $T_{min.} \le T_{amb} \le T_{max.}$	0.5	1 1		mA/m V	
Vol	Low output voltage at 5 mA sinking current	$T_{min.} \le T_{amb} \le T_{max.}$		250	400	mV	
los	Output short-circuit current. Output to (VCC -0.6 V). Sink current only.	T_{amb} = 25 °C $T_{min.} \le T_{amb} \le T_{max.}$	6 5	10		mA	



Table 5. Electrical characteristics (continued)

Symbol	Parameter	Test condition	Min.	Тур.	Max.	Unit	
Voltage re	Voltage reference						
V _{Ref}	Reference input voltage TSM1014 1% precision TSM1014A 0.5% precision	$\begin{split} T_{amb} &= 25~^{\circ}\text{C} \\ T_{min.} &\leq T_{amb} \leq T_{max.} \\ T_{amb} &= 25~^{\circ}\text{C} \\ T_{min.} &\leq T_{amb} \leq T_{max.} \end{split}$	1.238 1.225 1.244 1.237	1.25 1.25	1.262 1.273 1.256 1.261	V	
ΔV_{Ref}	Reference input voltage deviation over the temperature range	$T_{min.} \le T_{amb} \le T_{max.}$		20	30	mV	
RegLine	Reference input voltage deviation over the VCC range	Iload = 1 mA			20	mV	
RegLoad	Reference input voltage deviation over the output current	VCC = 18 V, 0 < Iload < 2.5 mA			10	mV	

^{1.} Test conditions: pin 2 and 6 connected to GND, pin 4 and 5 connected to 1.25 V, pin 3 connected to 200 mV.



^{2.} The current depends on the voltage difference between the negative and the positive inputs of the amplifier. If the voltage on the minus input is 1 mV higher than the positive amplifier, the sinking current at the output OUT will be increased by Gm *1 mA.

Internal schematic TSM1014

5 Internal schematic

Figure 2. Internal schematic

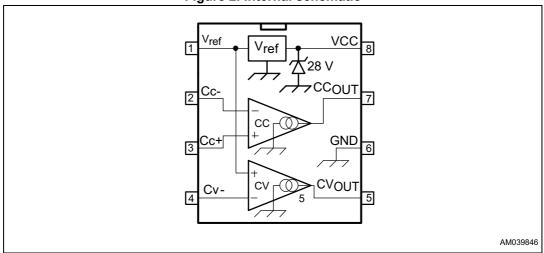
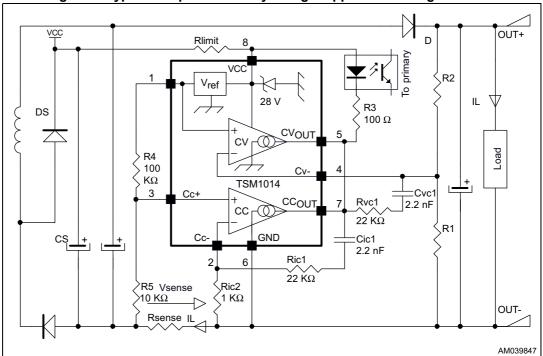


Figure 3. Typical adapter or battery charger application using TSM1014



In the application schematic shown in *Figure 3*, the TSM1014 is used on the secondary side of a flyback adapter (or battery charger) to provide an accurate voltage and current control. The above feedback loop is made with an optocoupler.

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6 Principles of operation and application tips

6.1 Voltage control

The voltage loop is controlled via a first transconductance operational amplifier, the resistor bridge *R1*, *R2*, and the optocoupler which is directly connected to the output.

The relation between the values of R1 and R2 should be chosen as written in Equation 1:

Equation 1

$$R1 = R2 \times V_{Ref} / (V_{out} - V_{Ref})$$

where V_{out} is the desired output voltage.

To avoid the discharge of the load, the resistor bridge R1, R2 should be highly resistive. For this type of application, a total value of 100 K Ω (or more) would be appropriate for the resistors R1 and R2.

As an example, with R2 = 100 K Ω , V_{out} = 4.10 V, V_{Ref} = 1.210 V, then R1 = 41.9 K Ω .

Note that if the low drop diode is inserted between the load and the voltage regulation resistor bridge to avoid current flowing from the load through the resistor bridge, this drop should be taken into account in the above calculations by replacing V_{out} by $(V_{out} + V_{drop})$.

6.2 Current control

The current loop is controlled via the second transconductance operational amplifier, the sense resistor R_{sense} , and the optocoupler.

 V_{sense} threshold is achieved externally by a resistor bridge tied to the V_{Ref} voltage reference. Its middle point is tied to the positive input of the current control operational amplifier, and its foot is to be connected to lower potential point of the sense resistor as shown in *Figure 4*. The resistors of this bridge are matched to provide the best precision possible.

The control equation verifies:

Equation 2

$$R_{\text{sense}} \times I_{\text{lim}} = V_{\text{sense}}$$

$$V_{\text{sense}} = \frac{R_5 \cdot V_{\text{ref}}}{(R_4 + R_5)}$$

Equation 3

$$I_{lim} = \frac{R_5 \cdot V_{ref} \cdot R_{sense}}{(R_4 + R_5)}$$

where I_{lim} is the desired limited current, and V_{sense} is the threshold voltage for the current control loop.

Note that the R_{sense} resistor should be chosen taking into account the maximum dissipation (P_{lim}) through it during full load operation.



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Equation 4

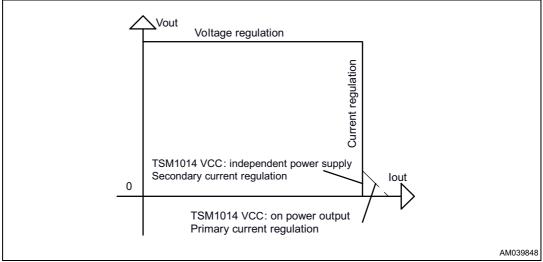
$$P_{lim} = I_{lim} \times V_{sense}$$

Therefore, for most adapter and battery charger applications, a quarter-watt, or half-watt resistor to make the current sensing function is sufficient.

The current sinking outputs of the two transconductance operational amplifiers are common (to the output of the IC). This makes an ORing function which ensures that whenever the current or the voltage reaches too high values, the optocoupler is activated.

The relation between the controlled current and the controlled output voltage can be described with a square characteristic as shown in the following V/I output power graph.

Figure 4. Output voltage versus output current



6.3 Compensation

The voltage control transconductance operational amplifier can be fully compensated. Both its output and negative input are directly accessible for external compensation components.

An example of a suitable voltage control compensation network is shown in *Figure 3 on* page 3. It consists of a capacitor Cvc1 = 2.2 nF and a resistor Rcv1 = 22 K Ω in series.

The current control transconductance operational amplifier can be fully compensated. Both of its output and negative input are directly accessible for external compensation components.

An example of a suitable current control compensation network is also shown in *Figure 3*. It consists of a capacitor Cic1 = 2.2 nF and a resistor Ric1 = 22 K Ω in series.

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6.4 Start-up and short-circuit conditions

Under start-up or short-circuit conditions the TSM1014 is not provided with a high enough supply voltage. This is due to the fact that the chip has its power supply line in common with the power supply line of the system.

Therefore, the current limitation can only be ensured by the primary PWM module, which should be chosen accordingly.

If the primary current limitation is considered not to be precise enough for the application, then a sufficient supply for the TSM1014 has to be ensured under all conditions. For this, it would be necessary to add some circuitry to supply the chip with a separate power line. This can be achieved in a number of ways, including putting an additional winding on the transformer.

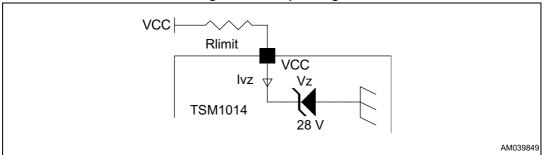
6.5 Voltage clamp

Figure 6 shows how to realize a low-cost power supply for the TSM1014 (with no additional windings). Please pay attention to the fact that in the particular case presented here, this low-cost power supply can reach voltages as high as twice the voltage of the regulated line. Since the absolute maximum rating of the TSM1014 supply voltage is 28 V. In the aim to protect the TSM1014 against such high voltage values an internal Zener clamp is integrated (see Figure 5).

Equation 5

$$R_{limit} = (VCC - V_z) \cdot I_{vz}$$

Figure 5. Clamp voltage





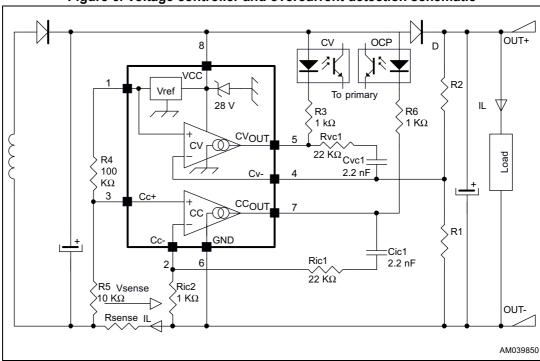


Figure 6. Voltage controller and overcurrent detection schematic

TSM1014 **Package information**

Package information 7

In order to meet environmental requirements, ST offers these devices in different grades of ECOPACK® packages, depending on their level of environmental compliance. ECOPACK specifications, grade definitions and product status are available at: www.st.com. ECOPACK is an ST trademark.

7.1 **SO-8 package information**

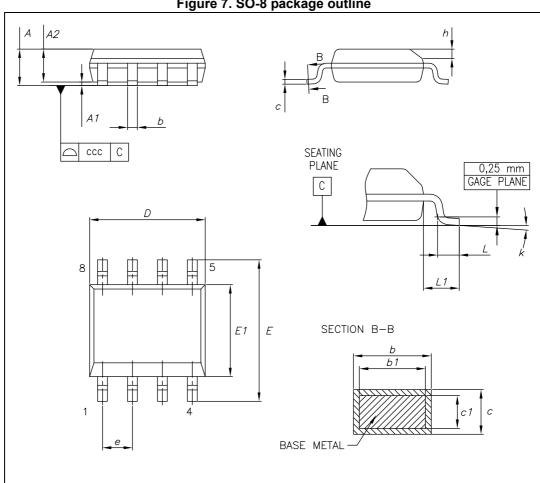


Figure 7. SO-8 package outline

Package information TSM1014

Table 6. SO-8 package mechanical data

Symbol	Dimensions (mm)			
Symbol	Min.	Тур.	Max.	
А			1.75	
A1	0.10		0.25	
A2	1.25			
b	0.28		0.48	
С	0.17		0.23	
D ⁽¹⁾	4.80	4.90	5.00	
E	5.80	6.00	6.20	
E1 ⁽²⁾	3.80	3.90	4.00	
е		1.27		
h	0.25		0.50	
L	0.40		1.27	
L1		1.04		
k	0°		8°	
ccc			0.10	

Dimension "D" does not include mold flash, protrusions or gate burrs. Mold flash, protrusions or gate burrs shall not exceed 0.15 mm in total (both sides).

^{2.} Dimension "E1" does not include interlead flash or protrusions. Interlead flash or protrusions shall not exceed 0.25 mm per side.

TSM1014 Revision history

8 Revision history

Table 7. Document revision history

Date	Revision	Changes
01 -Jul-2004	1	Initial release.
03-Mar-2016	2	Removed Mini SO8 package from the whole document. Minor modifications throughout document.
15-Apr-2016	3	Updated Section 7: Package information on page 11 (replaced Figure 7 on page 11 by new figure, updated Table 6 on page 12).

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