# **Absolute Maximum Ratings**

RS+, RS- to GND0.3V to +30V
OUT to GND0.3V to +6V
RS+ to RS±30V
Short-Circuit Duration: OUT to GNDContinuous
Continuous Input Current (Any Pin)±20mA
Continuous Power Dissipation (T <sub>A</sub> = +70°C)
4-Bump UCSP (derate 3.0mW/°C above +70°C)238mW
5-Pin SOT23 (derate 3.9mW/°C above +70°C)312mW
6-Pin µDFN (derate 4.5mW/°C above +70°C)358mW

Operating Temperature Range	40°C to +85°C
Junction Temperature	+150°C
Storage Temperature Range	-65°C to +150°C
Lead Temperature (excluding UCSP, soldering	, 10s) +300°C
Soldering Temperature (reflow)	+260°C

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

#### **Electrical Characteristics**

 $(V_{RS+} = V_{RS-} = 3.6V, V_{SENSE} = (V_{RS+} - V_{RS-}) = 0V, T_A = -40^{\circ}C \text{ to } +85^{\circ}C, \text{ unless otherwise noted. Typical values are at } T_A = +25^{\circ}C.) \text{ (Note 1)}$ 

PARAMETER	SYMBOL	CONDITIONS		MIN	TYP	MAX	UNITS
		V <sub>RS+</sub> = 5V, T <sub>A</sub> = +25°C			0.5	0.85	
Supply Current (Note 2)		V <sub>RS+</sub> = 5V, -40°C < T <sub>A</sub> < +85°C				1.1	- μΑ
	Icc	V <sub>RS+</sub> = 28V, T <sub>A</sub> = +25°C			1.1	1.8	
		V <sub>RS+</sub> = 28V, -40°C < T <sub>A</sub> < +85°C				2.5	
Common-Mode Input Range	V <sub>CM</sub>	Guaranteed by CMRR,	-40°C < T <sub>A</sub> < +85°C	1.6		28	V
Common-Mode Rejection Ratio	CMRR	1.6V < V <sub>RS+</sub> < 28V, -40°	C < T <sub>A</sub> < +85°C	94	130		dB
logget Offeet Voltage (Nata 2)		T <sub>A</sub> = +25°C			±100	±500	μV
Input Offset Voltage (Note 3)	Vos	-40°C < T <sub>A</sub> < +85°C				±600	
		MAX9938T			25		
		MAX9938F			50		.,,,,
Gain	G	MAX9938H			100		V/V
		MAX9938W			200		1
Gain Error (Note 4)	GE	MAX9938T/MAX9938F/	T <sub>A</sub> = +25°C		±0.1	±0.5	% %
		MAX9938H	-40°C < T <sub>A</sub> < +85°C			±0.6	
		MAX9938W	T <sub>A</sub> = +25°C		±0.1	±0.7	
			-40°C < T <sub>A</sub> < +85°C			±0.8	
	R <sub>OUT</sub>	(Note 5)	MAX9938T/F/H	7.0	10	13.2	
Output Resistance			MAX9938W	14.0	20	26.4	
	V <sub>OL</sub>	Gain = 25			1.5	15	
OLIT Law Vallage		Gain = 50			3	30	mV
OUT Low Voltage		Gain = 100			6	60	
		Gain = 200			12	120	
OUT High Voltage	V <sub>OH</sub>	V <sub>OH</sub> = V <sub>RS-</sub> - V <sub>OUT</sub> (Note 6)			0.1	0.2	V
Small-Signal Bandwidth (Note 5)	BW	V <sub>SENSE</sub> = 50mV, gain =	25		125		V
		V <sub>SENSE</sub> = 50mV, gain = 50			60		
		V <sub>SENSE</sub> = 50mV, gain = 100			30		kHz
		V <sub>SENSE</sub> = 50mV, gain = 200			15		
Output Settling Time	ts	1% final value, V <sub>SENSE</sub> = 50mV			100		μs

## **Electrical Characteristics (continued)**

 $(V_{RS+} = V_{RS-} = 3.6V, V_{SENSE} = (V_{RS+} - V_{RS-}) = 0V, T_A = -40^{\circ}C \text{ to } +85^{\circ}C, \text{ unless otherwise noted. Typical values are at } T_A = +25^{\circ}C.) \text{ (Note 1)}$ 

Note 1: All devices are 100% production tested at T<sub>A</sub> = +25°C. All temperature limits are guaranteed by design.

**Note 2:**  $V_{OUT} = 0$ .  $I_{CC}$  is the total current into RS+ plus RS- pins.

Note 3: V<sub>OS</sub> is extrapolated from measurements for the gain-error test.

Note 4: Gain error is calculated by applying two values of V<sub>SENSE</sub> and calculating the error of the slope vs. the ideal:

Gain = 25,  $V_{SENSE}$  is 20mV and 120mV.

Gain = 50,  $V_{SENSE}$  is 10mV and 60mV.

Gain = 100,  $V_{SENSE}$  is 5mV and 30mV.

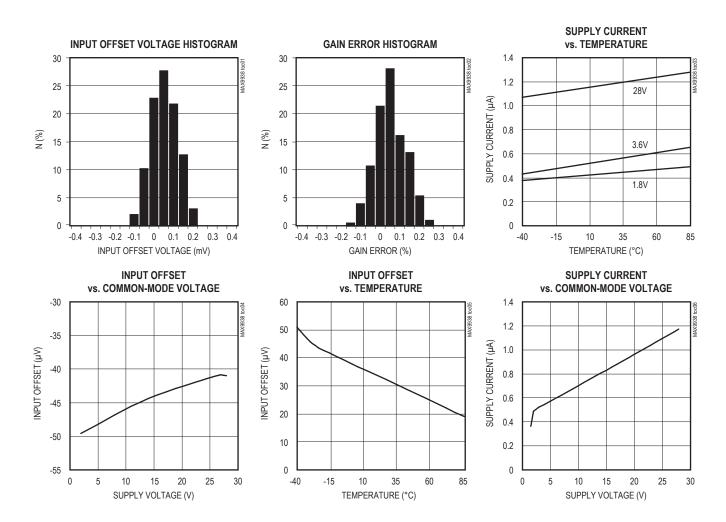
Gain = 200, V<sub>SENSE</sub> is 2.5mV and 15mV.

Note 5: The device is stable for any external capacitance value.

**Note 6:**  $V_{OH}$  is the voltage from  $V_{RS-}$  to  $V_{OUT}$  with  $V_{SENSE} = 3.6 \text{V/gain}$ .

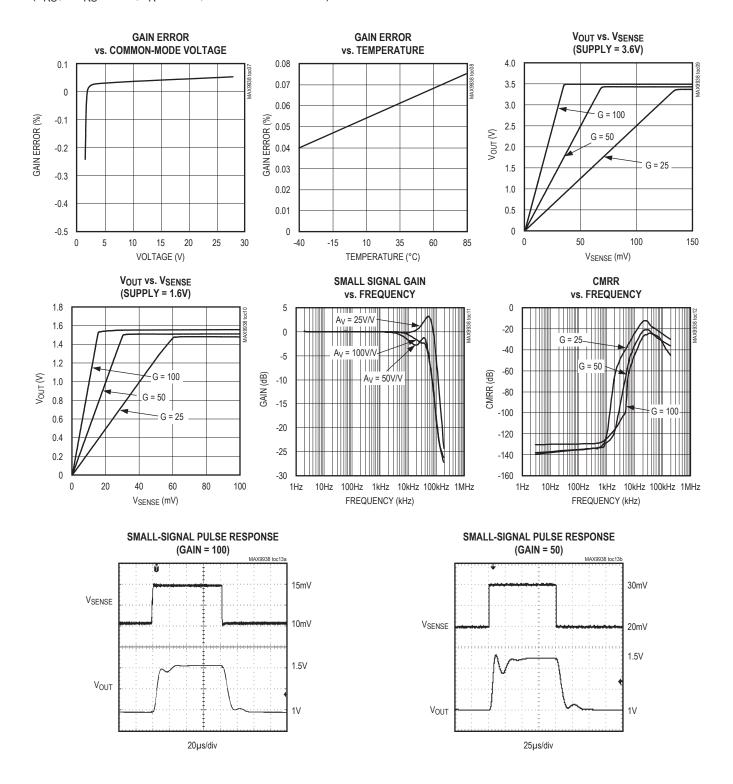
## **Typical Operating Characteristics**

 $(V_{RS+} = V_{RS-} = 3.6V, T_A = +25^{\circ}C, unless otherwise noted.)$ 



# **Typical Operating Characteristics (continued)**

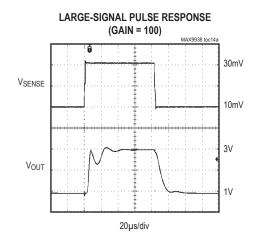
 $(V_{RS+} = V_{RS-} = 3.6V, T_A = +25^{\circ}C, unless otherwise noted.)$ 

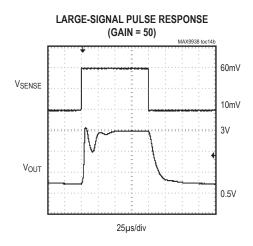


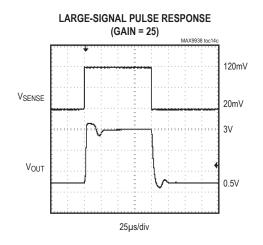
# **Typical Operating Characteristics (continued)**

 $(V_{RS+} = V_{RS-} = 3.6V, T_A = +25^{\circ}C, \text{ unless otherwise noted.})$ 

# SMALL-SIGNAL PULSE RESPONSE (GAIN = 25) MAX9938 toc13c 60mV VSENSE VOUT 1V 25µs/div



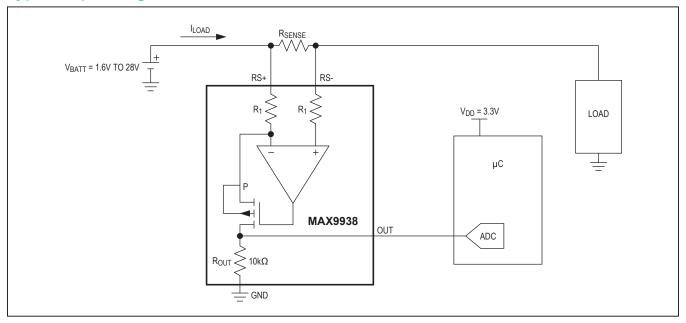




# **Pin Description**

	PIN		NAME	FUNCTION	
UCSP	SOT23	μDFN	NAME	FUNCTION	
A1	5	4	RS+	External Sense Resistor Power-Side Connection	
A2	4	6	RS-	External Sense Resistor Load-Side Connection	
B1	1, 2	3	GND	Ground	
B2	3	1	OUT	Output Voltage. V <sub>OUT</sub> is proportional to V <sub>SENSE</sub> = V <sub>RS+</sub> - V <sub>RS-</sub> .	
_	_	2, 5	N.C.	No Connection. Not internally connected.	

## **Typical Operating Circuit**



## **Detailed Description**

The MAX9938 unidirectional high-side, current-sense amplifier features a 1.6V to 28V input common-mode range. This feature allows the monitoring of current out of a battery with a voltage as low as 1.6V. The MAX9938 monitors current through a current-sense resistor and amplifies the voltage across that resistor.

The MAX9938 is a unidirectional current-sense amplifier that has a well-established history. An op amp is used to force the current through an internal gain resistor at RS+, which has a value of  $R_1$ , such that its voltage drop equals the voltage drop across an external sense resistor,  $R_{\text{SENSE}}$ . There is an internal resistor at RS- with the

same value as  $R_1$  to minimize offset voltage. The current through  $R_1$  is sourced by a high-voltage p-channel FET. Its source current is the same as its drain current, which flows through a second gain resistor,  $R_{OUT}$ . This produces an output voltage,  $V_{OUT}$ , whose magnitude is  $I_{LOAD} \times R_{SENSE} \times R_{OUT}/R_1$ . The gain accuracy is based on the matching of the two gain resistors  $R_1$  and  $R_{OUT}$  (see <u>Table 1</u>). Total gain = 25V/V for the MAX9938T, 50V/V for the MAX9938F, 100V/V for the MAX9938H, and 200V/V for the MAX9938W. The output is protected from input overdrive by use of an output current limiting circuit of 7mA (typical) and a 6V clamp protection circuit.

**Table 1. Internal Gain Setting Resistors (Typical Values)** 

GAIN (V/V)	R <sub>1</sub> (Ω)	R <sub>OUT</sub> (kΩ)
200	100	20
100	100	10
50	200	10
25	400	10

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## **Applications Information**

#### **Choosing the Sense Resistor**

Choose RSENSE based on the following criteria:

#### **Voltage Loss**

A high  $R_{SENSE}$  value causes the power-source voltage to drop due to IR loss. For minimal voltage loss, use the lowest  $R_{SENSE}$  value.

#### OUT Swing vs. VRS+ and VSENSE

The MAX9938 is unique since the supply voltage is the input common-mode voltage (the average voltage at RS+ and RS-). There is no separate  $V_{CC}$  supply voltage pin. Therefore, the OUT voltage swing is limited by the minimum voltage at RS+.

 $V_{OUT}$  (max) =  $V_{RS+}$  (min) -  $V_{SENSE}$  (max) -  $V_{OH}$  and

$$R_{SENSE} = \frac{V_{OUT} \text{ (max)}}{G \times I_{LOAD} \text{ (max)}}$$

V<sub>SENSE</sub> full scale should be less than V<sub>OUT</sub>/gain at the minimum RS+ voltage. For best performance with a 3.6V supply voltage, select R<sub>SENSE</sub> to provide approximately 120mV (gain of 25V/V), 60mV (gain of 50V/V), 30mV (gain of 100V/V), or 15mV (gain of 200V/V) of sense voltage for the full-scale current in each application. These can be increased by use of a higher minimum input voltage.

#### **Accuracy**

In the linear region (V<sub>OUT</sub> < V<sub>OUT</sub>(max)), there are two components to accuracy: input offset voltage (V<sub>OS</sub>) and gain error (GE). For the MAX9938, V<sub>OS</sub> =  $500\mu$ V (max) and gain error is 0.5% (max). Use the linear equation:

 $V_{OUT} = (gain \pm GE) \times V_{SENSE} \pm (gain \times V_{OS})$ 

to calculate total error. A high R<sub>SENSE</sub> value allows lower currents to be measured more accurately because offsets are less significant when the sense voltage is larger.

#### **Efficiency and Power Dissipation**

At high current levels, the I $^2$ R losses in R $_{SENSE}$  can be significant. Take this into consideration when choosing the resistor value and its power dissipation (wattage) rating. Also, the sense resistor's value might drift if it is allowed to heat up excessively. The precision V $_{OS}$  of the MAX9938 allows the use of small sense resistors to reduce power dissipation and reduce hot spots.

#### **Kelvin Connections**

Because of the high currents that flow through R<sub>SENSE</sub>, take care to eliminate parasitic trace resistance from causing errors in the sense voltage. Either use a four-terminal current-sense resistor or use Kelvin (force and sense) PCB layout techniques.

#### **Optional Output Filter Capacitor**

When designing a system that uses a sample-and-hold stage in the ADC, the sampling capacitor momentarily loads OUT and causes a drop in the output voltage. If sampling time is very short (less than a microsecond), consider using a ceramic capacitor across OUT and GND to hold  $V_{OUT}$  constant during sampling. This also decreases the small-signal bandwidth of the current-sense amplifier and reduces noise at OUT.

#### **Input Filters**

Some applications of current-sense amplifiers need to measure currents accurately even in the presence of both differential and common-mode ripple, as well as a wide variety of input transient conditions. For example, high-frequency ripple at the output of a switching buck or boost regulator results in a common-mode voltage at the inputs of the MAX9938. Alternatively, fast load-current transients, when measuring at the input of a switching buck or boost regulator, can cause high-frequency differential sense voltages to occur at the inputs of the MAX9938, although the signal of interest is the average DC value. Such high-frequency differential sense voltages may result in a voltage offset at the MAX9938 output.

#### MAX9938

# nanoPower, 4-Bump UCSP/SOT23, Precision Current-Sense Amplifier

The MAX9938 allows two methods of filtering to help improve performance in the presence of input common-mode voltage and input differential voltage transients. Figure 1 shows a differential input filter.

The capacitor  $C_{\text{IN}}$  between RS+ and RS- along with the resistor  $R_{\text{IN}}$  between the sense resistor and RS- helps filter against input differential voltages and prevents them from reaching the MAX9938.

The corner frequency of this filter is determined by the choice of  $R_{IN}$ ,  $C_{IN}$ , and the value of the input resistance at RS-  $(R_1)$ . See Table 1 for  $R_1$  values at the different gain options.

The value of  $R_{IN}$  should be chosen to minimize its effect on the input offset voltage due to the bias current at RS-.  $R_{IN} \times I_{BIAS}$  contributes to the input voltage offset.  $I_{BIAS}$  is typically  $0.2\mu A$ .

Placing  $R_{IN}$  at the RS- input does not affect the gain error of the device because the gain is given by the ratio between  $R_{OUT}$  and  $R_1$  at RS+.

Figure 2 shows the input common-mode filter.

Again, the corner frequency of the filter is determined by the choice of  $R_{IN}$ ,  $C_{IN}$  and is affected by  $R_1$ .

In this case  $R_{IN}$  affects both gain error and input offset voltage.  $R_{IN}$  should be smaller than  $R_1$  so that it has negligible effect on the device gain. If, for example, a filter with  $R_{IN}$  =  $10\Omega$  and  $C_{IN}$  =  $1\mu F$  is built, then depending upon the gain selection, the gain error is affected by either 2.5% (G =  $25\text{V/V},\,R_1$  =  $400\Omega$ ) or 5% (G =  $50\text{V/V},\,R_1$  =  $200\Omega$ ) or 10% (G =  $200\text{V/V},\,R_1$  =  $100\Omega$ ).

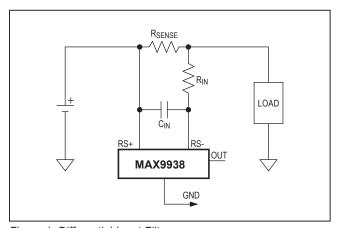


Figure 1. Differential Input Filter

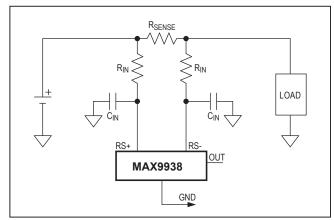


Figure 2. Input Common-Mode Filter

#### **Bidirectional Application**

Battery-powered systems may require a precise bidirectional current-sense amplifier to accurately monitor the battery's charge and discharge currents. Measurements of the two separate outputs with respect to GND yields an accurate measure of the charge and discharge currents respectively (Figure 3).

# **UCSP Applications Information**

For the latest application details on UCSP construction, dimensions, tape carrier information, PCB techniques, bump-pad layout, and recommended reflow temperature profile, as well as the latest information on reliability testing results, refer to the Application Note 1891: Wafer-Level Packaging (WLP) and Its Applications available on Maxim's website at <a href="https://www.maximintegrated.com/ucsp">www.maximintegrated.com/ucsp</a>.

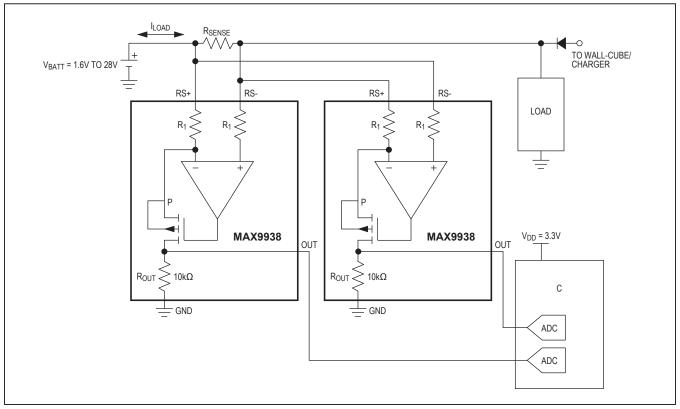


Figure 3. Bidirectional Application

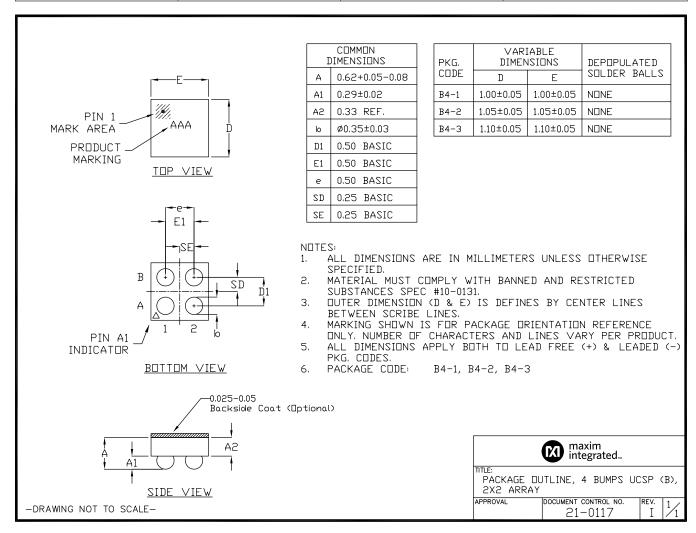
# **Chip Information**

PROCESS: BICMOS

## **Package Information**

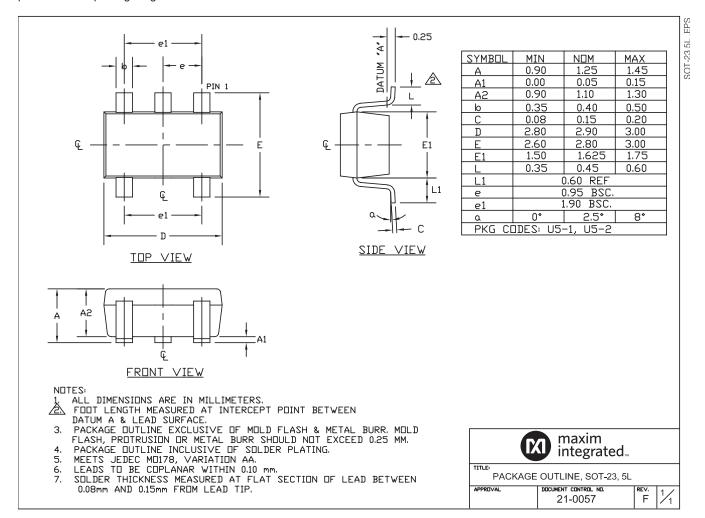
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PACKAGE TYPE	PACKAGE CODE	OUTLINE NO.	LAND PATTERN NO.
2 x 2 UCSP	B4+1	<u>21-0117</u>	_
5 SOT23	U5-2	<u>21-0057</u>	<u>90-0174</u>
6 μDFN	L622+1	<u>21-0164</u>	90-0004



## Package Information (continued)

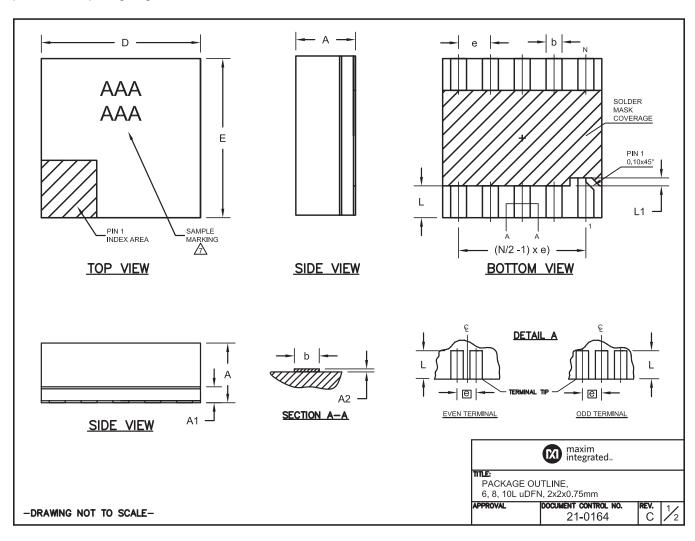
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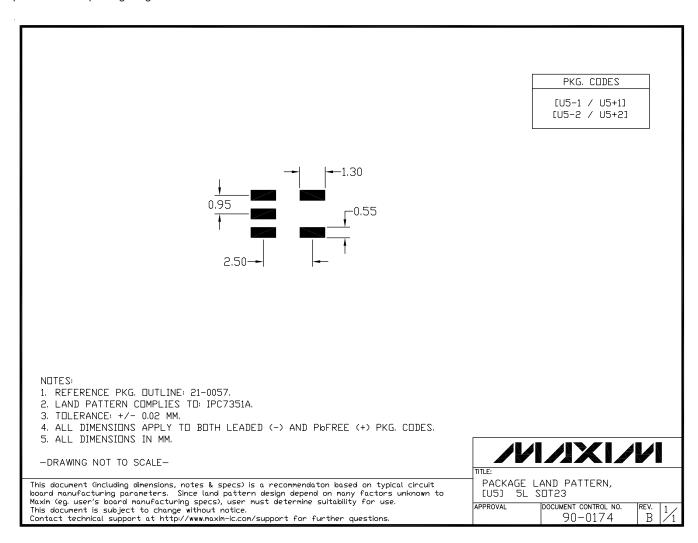
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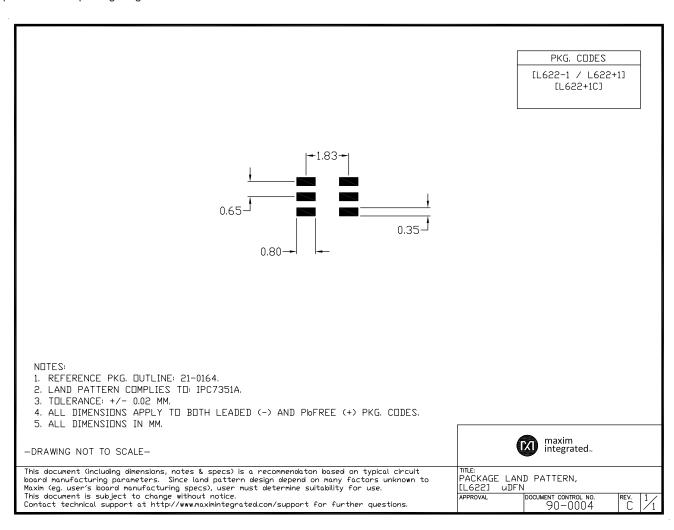
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# **Revision History**

REVISION NUMBER	REVISION DATE	DESCRIPTION	PAGES CHANGED
0	4/08	Initial release	_
1	9/08	Added µDFN package information	1, 2, 4, 5, 9
2	2/09	Added G45 designation to part number	1
3	10/09	Added Input Filters section and MAX9938W to the data sheet	1, 2, 6–9
4	2/10	Updated EC table and Input Filters section	2, 8
5	8/10	Removed Power-Up Time parameter	2
6	1/11	Corrected error on Figure 2	8
7	4/17	Updated title of data sheet to include "nanoPower"	1–14
7.1		Corrected broken links in Package Information	10

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