



# N-Channel UltraFET $^{\otimes}$ Trench MOSFET 100V, 44A, 28m $\Omega$

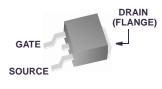
### **Features**

- $r_{DS(ON)} = 24m\Omega$  (Typ.),  $V_{GS} = 10V$ ,  $I_D = 44A$
- $Q_q(tot) = 24nC (Typ.), V_{GS} = 10V$
- Low Miller Charge
- · Low Qrr Body Diode
- · Optimized efficiency at high frequencies
- UIS Capability (Single Pulse and Repetitive Pulse)

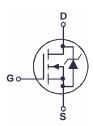
### **Applications**

- DC/DC converters and Off-Line UPS
- Distributed Power Architectures and VRMs
- Primary Switch for 24V and 48V Systems
- High Voltage Synchronous Rectifier

Formerly developmental type 82760







### **MOSFET Maximum Ratings** $T_C = 25^{\circ}C$ unless otherwise noted

Symbol	Parameter	Ratings	Units
V <sub>DSS</sub>	Drain to Source Voltage	100	V
V <sub>GS</sub>	Gate to Source Voltage	±20	V
	Drain Current		
	Continuous ( $T_C = 25^{\circ}C$ , $V_{GS} = 10V$ )	44	Α
$I_D$	Continuous (T <sub>C</sub> = 100°C, V <sub>GS</sub> = 10V)	31	А
	Continuous ( $T_{amb} = 25^{\circ}C$ , $V_{GS} = 10V$ , $R_{\theta JA} = 52^{\circ}C/W$ )	6.5	А
	Pulsed	Figure 4	А
E <sub>AS</sub>	Single Pulse Avalanche Energy (Note 1)	120	mJ
	Power dissipation	135	W
$P_{D}$	Derate above 25°C	0.9	W/°C
T <sub>J</sub> , T <sub>STG</sub>	Operating and Storage Temperature	-55 to 175	°C

### **Thermal Characteristics**

$R_{\theta JC}$	Thermal Resistance Junction to Case TO-252	1.11	°C/W
$R_{\theta JA}$	Thermal Resistance Junction to Ambient TO-252	100	°C/W
$R_{\theta JA}$	Thermal Resistance Junction to Ambient TO-252, 1in <sup>2</sup> copper pad area	52	°C/W

Reliability data can be found at: http://www.fairchildsemi.com/products/discrete/reliability/index.html.

All Fairchild Semiconductor products are manufactured, assembled and tested under ISO9000 and QS9000 quality systems certification.

Device Marking	Device	Package	Reel Size	Tape Width	Quantity
FDD3672	FDD3672	TO-252AA	330mm	16mm	2500 units

## **Electrical Characteristics** $T_C = 25^{\circ}C$ unless otherwise noted

Symbol	Parameter	Test Condition	ns	Min	Тур	Max	Units
Off Characteristics							
B <sub>VDSS</sub>	Drain to Source Breakdown Voltage	$I_D = 250 \mu A, V_{GS} = 0 V$		100	-	-	V
1	Zoro Coto Voltago Droin Current	$V_{DS} = 80V$		-	-	1	
IDSS	Zero Gate Voltage Drain Current	$V_{GS} = 0V$ $T_{C} = 0$	= 150°C	-	-	250	μΑ
I <sub>GSS</sub>	Gate to Source Leakage Current	$V_{GS} = \pm 20V$		-	-	±100	nA

### **On Characteristics**

V <sub>GS(TH)</sub>	Gate to Source Threshold Voltage	$V_{GS} = V_{DS}, I_{D} = 250 \mu A$	2	-	4	V
r <sub>DS(ON)</sub>	Drain to Source On Resistance	$I_D = 44A, V_{GS} = 10V$	-	0.024	0.028	
		$I_D = 21A, V_{GS} = 6V,$	-	0.031	0.047	Ω
		I <sub>D</sub> =44A, V <sub>GS</sub> =10V, T <sub>C</sub> =175°C	-	0.054	0.068	

### **Dynamic Characteristics**

C <sub>ISS</sub>	Input Capacitance	V 25V V 0V	-	1710	-	pF
Coss	Output Capacitance	$V_{DS} = 25V, V_{GS} = 0V,$ f = 1MHz	-	247	-	pF
C <sub>RSS</sub>	Reverse Transfer Capacitance	1 – 1111112	-	62	-	pF
$Q_{g(TOT)}$	Total Gate Charge at 10V	V <sub>GS</sub> = 0V to 10V	-	24	36	nC
$Q_{g(TH)}$	Threshold Gate Charge	$V_{GS} = 0V \text{ to } 2V$ $V_{DD} = 50V$	-	3	4.5	nC
$Q_{gs}$	Gate to Source Gate Charge I <sub>D</sub> = 44A		-	8.6	-	nC
Q <sub>gs2</sub>	Gate Charge Threshold to Plateau	$I_g = 1.0 \text{mA}$	-	5.6	-	nC
$Q_{gd}$	Gate to Drain "Miller" Charge		-	5.6	-	nC

### **Resistive Switching Characteristics** (V<sub>GS</sub> = 10V)

t <sub>ON</sub>	Turn-On Time		-	-	104	ns
t <sub>d(ON)</sub>	Turn-On Delay Time		-	11	-	ns
t <sub>r</sub>	Rise Time	$V_{DD} = 50V, I_{D} = 44A$	-	59	-	ns
t <sub>d(OFF)</sub>	Turn-Off Delay Time	$V_{GS} = 10V, R_{GS} = 11.0\Omega$	-	26	-	ns
t <sub>f</sub>	Fall Time		-	44	-	ns
t <sub>OFF</sub>	Turn-Off Time		-	-	104	ns

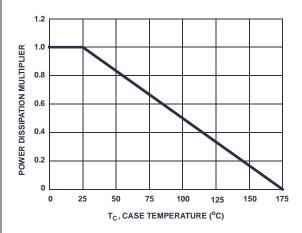
### **Drain-Source Diode Characteristics**

V <sub>SD</sub>	Source to Drain Diode Voltage	I <sub>SD</sub> = 44A	-	-	1.25	V
	Source to Drain Diode Voltage	I <sub>SD</sub> = 21A	-	-	1.0	V
t <sub>rr</sub>	Reverse Recovery Time	$I_{SD} = 44A$ , $dI_{SD}/dt = 100A/\mu s$	-	-	52	ns
Q <sub>RR</sub>	Reverse Recovery Charge	$I_{SD} = 44A$ , $dI_{SD}/dt = 100A/\mu s$	-	-	80	nC

Notes: 1: Starting  $T_J = 25^{\circ}C$ , L = 0.6mH,  $I_{AS} = 20A$ . 2: Pulse Width = 100s

FDD3672 Rev. 1.2





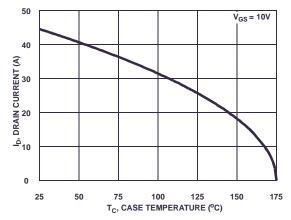


Figure 1. Normalized Power Dissipation vs Ambient Temperature

Figure 2. Maximum Continuous Drain Current vs Case Temperature

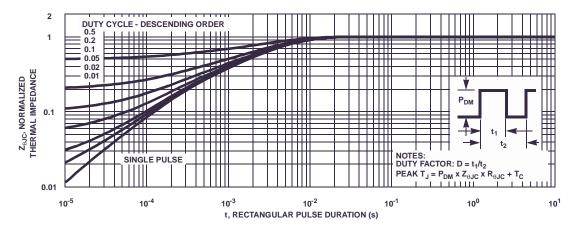


Figure 3. Normalized Maximum Transient Thermal Impedance

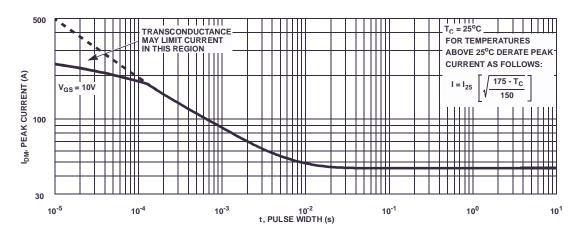
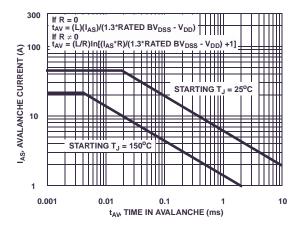


Figure 4. Peak Current Capability

### **Typical Characteristics** T<sub>C</sub> = 25°C unless otherwise noted



80 PULSE DURATION = 80 µs DUTY CYCLE = 0.5% MAX VDD = 15V

40 TJ = 175°C

TJ = -55°C

TJ = -55°C

TJ = -55°C

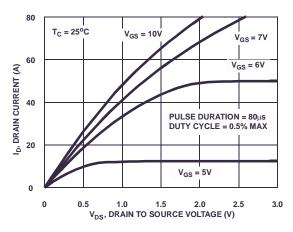
VGS, GATE TO SOURCE VOLTAGE (V)

NOTE: Refer to Fairchild Application Notes AN7514 and AN7515

Figure 5. Unclamped Inductive Switching

Capability

Figure 6. Transfer Characteristics



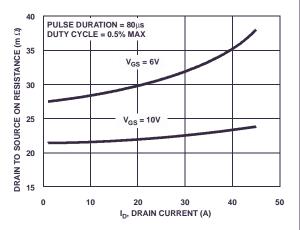
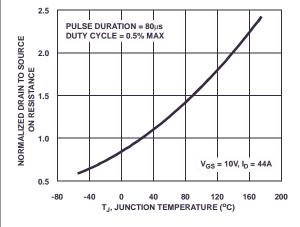


Figure 7. Saturation Characteristics

Figure 8. Drain to Source On Resistance vs Drain Current



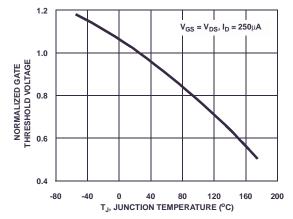


Figure 9. Normalized Drain to Source On Resistance vs Junction Temperature

Figure 10. Normalized Gate Threshold Voltage vs Junction Temperature

## Typical Characteristics $T_C = 25^{\circ}C$ unless otherwise noted

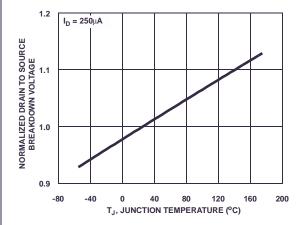


Figure 11. Normalized Drain to Source Breakdown Voltage vs Junction Temperature

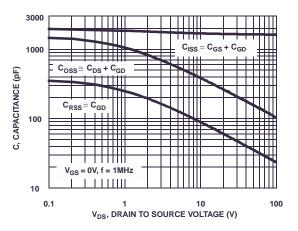


Figure 12. Capacitance vs Drain to Source Voltage

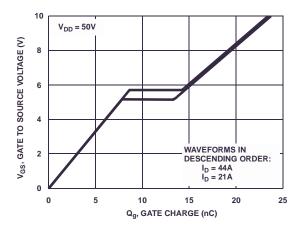


Figure 13. Gate Charge Waveforms for Constant Gate Currents

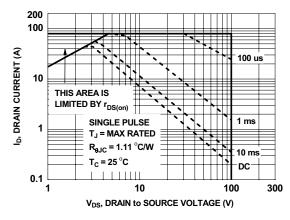
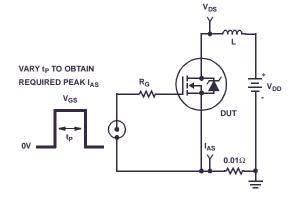


Figure 14. Forward Bias Safe Operating Area

### **Test Circuits and Waveforms**



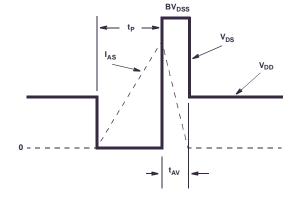


Figure 14. Unclamped Energy Test Circuit

Figure 15. Unclamped Energy Waveforms

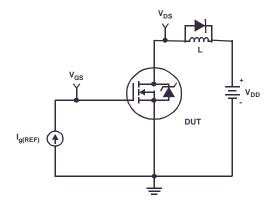


Figure 16. Gate Charge Test Circuit

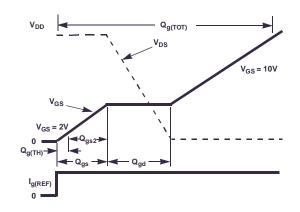


Figure 17. Gate Charge Waveforms

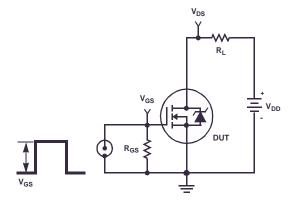


Figure 18. Switching Time Test Circuit

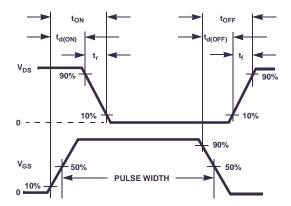


Figure 19. Switching Time Waveforms

### Thermal Resistance vs. Mounting Pad Area

The maximum rated junction temperature,  $T_{JM}$ , and the thermal resistance of the heat dissipating path determines the maximum allowable device power dissipation,  $P_{DM}$ , in an application. Therefore the application's ambient temperature,  $T_A$  (°C), and thermal resistance  $R_{\theta JA}$  (°C/W) must be reviewed to ensure that  $T_{JM}$  is never exceeded. Equation 1 mathematically represents the relationship and serves as the basis for establishing the rating of the part.

$$P_{DM} = \frac{(T_{JM} - T_A)}{R_{\theta JA}} \tag{EQ. 1}$$

In using surface mount devices such as the TO-252 package, the environment in which it is applied will have a significant influence on the part's current and maximum power dissipation ratings. Precise determination of  $P_{DM}$  is complex and influenced by many factors:

- Mounting pad area onto which the device is attached and whether there is copper on one side or both sides of the board.
- The number of copper layers and the thickness of the board.
- 3. The use of external heat sinks.
- 4. The use of thermal vias.
- 5. Air flow and board orientation.
- For non steady state applications, the pulse width, the duty cycle and the transient thermal response of the part, the board and the environment they are in.

Fairchild provides thermal information to assist the designer's preliminary application evaluation. Figure 20 defines the  $R_{\theta JA}$  for the device as a function of the top copper (component side) area. This is for a horizontally positioned FR-4 board with 1oz copper after 1000 seconds of steady state power with no air flow. This graph provides the necessary information for calculation of the steady state junction temperature or power dissipation. Pulse applications can be evaluated using the Fairchild device Spice thermal model or manually utilizing the normalized maximum transient thermal impedance curve.

Thermal resistances corresponding to other copper areas can be obtained from Figure 20 or by calculation using Equation 2 or 3. Equation 2 is used for copper area defined in inches square and equation 3 is for area in centimeters square. The area, in square inches or square centimeters is the top copper area including the gate and source pads.

$$R_{\theta JA} = 33.32 + \frac{23.84}{(0.268 + Area)}$$
 (EQ. 2)

Area in Inches Squared

$$R_{\theta JA} = 33.32 + \frac{154}{(1.73 + Area)}$$
 (EQ. 3)

Area in Centimeters Squared

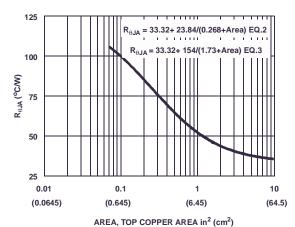
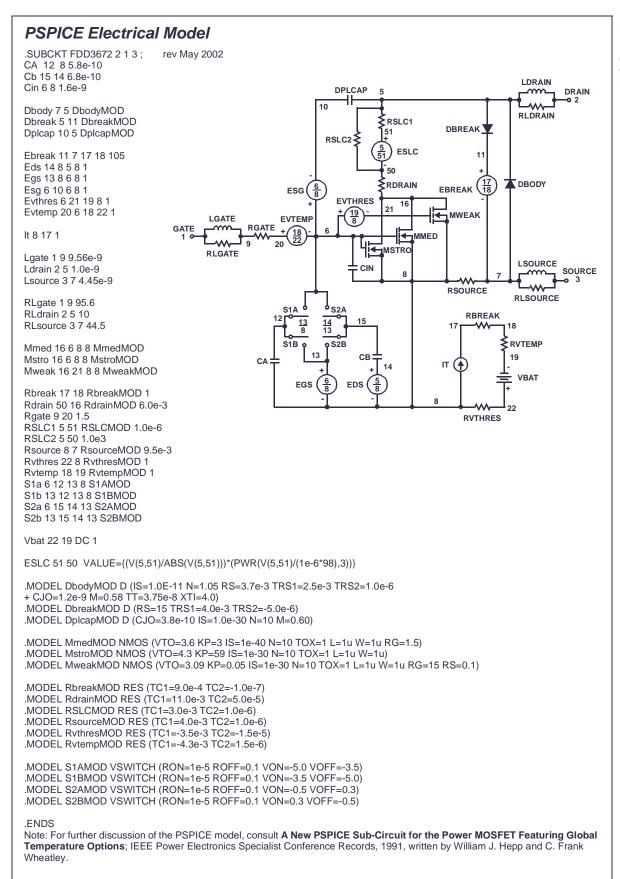
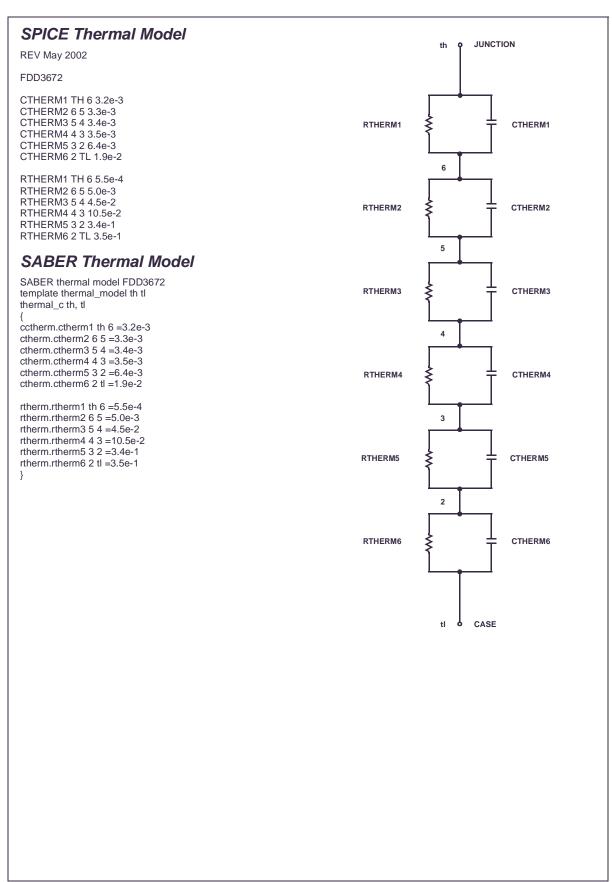


Figure 20. Thermal Resistance vs Mounting
Pad Area



#### SABER Electrical Model REV May 2002 template FDD3672 n2,n1,n3 electrical n2,n1,n3 var i iscl dp..model dbodymod = (isl=1.0e-11,nl=1.05,rs=3.7e-3,trs1=2.5e-3,trs2=1.0e-6,cjo=1.2e-9,m=0.58,tt=3.75e-8,xti=4.0) dp..model dbreakmod = (rs=15.trs1=4.0e-3.trs2=-5.0e-6)dp..model dplcapmod = (cjo=3.8e-10,isl=10.0e-30,nl=10,m=0.60) $m..model mmedmod = (type=\_n, vto=3.6, kp=3, is=1e-40, tox=1)$ m..model mstrongmod = (type=\_n,vto=4.3,kp=59,is=1e-30, tox=1) m..model mstronginod = (type=\_n,vto=3.09,kp=0.05,is=1e-30, tox=1,rs=0.1) m..model mweakmod = (type=\_n,vto=3.09,kp=0.05,is=1e-30, tox=1,rs=0.1) **LDRAIN** DRAIN sw\_vcsp..model s1amod = (ron=1e-5,roff=0.1,von=-5.0,voff=-3.5) sw\_vcsp..model s1bmod = (ron=1e-5,roff=0.1,von=-3.5,voff=-5.0) 10 RLDRAIN sw\_vcsp..model s2amod = (ron=1e-5,roff=0.1,von=-0.5,voff=0.3) **≨**RSLC1 sw\_vcsp..model s2bmod = (ron=1e-5,roff=0.1,von=0.3,voff=-0.5) c.ca n12 n8 = 5.8e-10RSLC2 € c.cb n15 n14 = 6.8e-10ISCI c.cin n6 n8 = 1.6e-9DBREAK 3 50 dp.dbody n7 n5 = model=dbodymod **≷**RDRAIN 8 FSG ( 11 dp.dbreak n5 n11 = model=dbreakmod DBODY **EVTHRES** dp.dplcap n10 n5 = model=dplcapmod MWFAK LGATE **EVTEMP RGATE** spe.ebreak n11 n7 n17 n18 = 105 GATE 18 22 **←**MMED spe.eds n14 n8 n5 n8 = 120 ← MSTRO spe.egs n13 n8 n6 n8 = 1 RLGATE spe.esg n6 n10 n6 n8 = 1 **LSOURCE** CIN SOURCE spe.evthres n6 n21 n19 n8 = 1 spe.evtemp n20 n6 n18 n22 = 1 RSOURCE RLSOURCE i.it n8 n17 = 1RBREAK 17 I.lgate n1 n9 = 95.6e-9I.ldrain n2 n5 = 1.0e-9 RVTEMP S<sub>1</sub>B oS2B I.lsource n3 n7 = 4.45e-9СВ 19 14 res.rlgate n1 n9 = 9.56 VBAT EGS EDS res.rldrain n2 n5 = 10res.rlsource n3 n7 = 44.5 **RVTHRES** m.mmed n16 n6 n8 n8 = model=mmedmod, l=1u, w=1u m.mstrong n16 n6 n8 n8 = model=mstrongmod, l=1u, w=1u m.mweak n16 n21 n8 n8 = model=mweakmod, l=1u, w=1u res.rbreak n17 n18 = 1, tc1=9.0e-4,tc2=-1.0e-7 res.rdrain n50 n16 = 6.0e-3, tc1=11.0e-3,tc2=5.0e-5 res.rgate n9 n20 = 1.5 res.rslc1 n5 n51 = 1.0e-6, tc1=3.0e-3,tc2=1.0e-6 res.rslc2 n5 n50 = 1.0e3 res.rsource n8 n7 = 9.5e-3, tc1=4.0e-3,tc2=1.0e-6 res.rvthres n22 n8 = 1, tc1=-3.5e-3,tc2=-1.5e-5 res.rvtemp n18 n19 = 1, tc1=-4.3e-3,tc2=1.5e-6 sw vcsp.s1a n6 n12 n13 n8 = model=s1amod sw\_vcsp.s1b n13 n12 n13 n8 = model=s1bmod sw\_vcsp.s2a n6 n15 n14 n13 = model=s2amod sw\_vcsp.s2b n13 n15 n14 n13 = model=s2bmod v.vbat n22 n19 = dc=1 equations { i (n51->n50) +=iscl (v(n51,n50) = ((v(n5,n51)/(1e-9+abs(v(n5,n51))))\*((abs(v(n5,n51)\*1e6/98))\*\*3))







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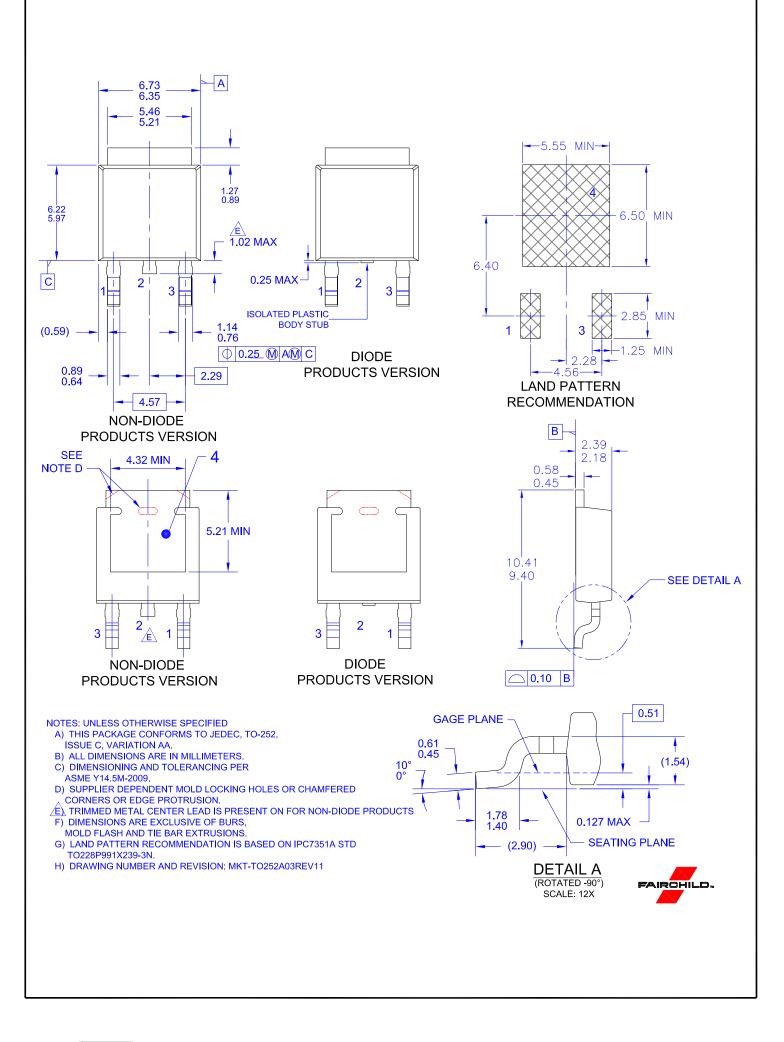
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