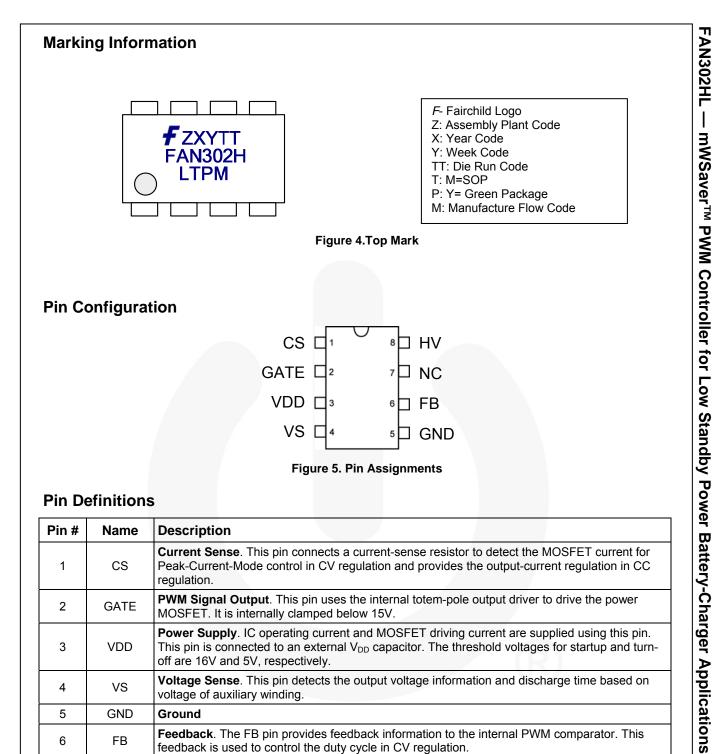


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FAN302HL — mWSaver[™] PWM Controller for Low Standby Power Battery-Charger Applications



Pin Definitions

Pin #	Name	Description
1	CS	Current Sense . This pin connects a current-sense resistor to detect the MOSFET current for Peak-Current-Mode control in CV regulation and provides the output-current regulation in CC regulation.
2	GATE	PWM Signal Output . This pin uses the internal totem-pole output driver to drive the power MOSFET. It is internally clamped below 15V.
3	VDD	Power Supply . IC operating current and MOSFET driving current are supplied using this pin. This pin is connected to an external V_{DD} capacitor. The threshold voltages for startup and turn-off are 16V and 5V, respectively.
4	VS	Voltage Sense. This pin detects the output voltage information and discharge time based on voltage of auxiliary winding.
5	GND	Ground
6	FB	Feedback . The FB pin provides feedback information to the internal PWM comparator. This feedback is used to control the duty cycle in CV regulation.
7	NC	No Connect
8	HV	High Voltage. This pin connects to bulk capacitor for high-voltage startup.

Absolute Maximum Ratings

Stresses exceeding the absolute maximum ratings may damage the device. The device may not function or be operable above the recommended operating conditions and stressing the parts to these levels is not recommended. In addition, extended exposure to stresses above the recommended operating conditions may affect device reliability. The absolute maximum ratings are stress ratings only.

Symbol		Parameter	Min.	Max.	Unit
V _{HV}	HV Pin Input Voltage			500	V
V _{VDD}	DC Supply Voltage ^(1,2)			30	V
V _{VS}	VS Pin Input Voltage			7.0	V
V _{CS}	CS Pin Input Voltage			7.0	V
V_{FB}	FB Pin Input Volta	age	-0.3	7.0	V
PD	Power Dissipation (T _A =25°C)			660	mW
Ө _{JA}	Thermal Resistan	ce (Junction-to-Air)		150	°C/W
ө _{лс}	Thermal Resistan	ce (Junction-to-Case)		39	°C/W
TJ	Operating Junctio	-40	+150	°C	
T _{STG}	Storage Tempera	ture Range	-55	+150	°C
TL	Lead Temperatur		+260	°C	
ESD	Electrostatic	Human Body Model, JEDEC:JESD22_A114 (Except HV Pin) ⁽³⁾	5		kV
ESD	D Discharge Capability Charged Device Model, JEDEC:JESD22_C101 (Except HV Pin) ⁽³⁾			1.5	ĸv

Notes:

1. All voltage values, except differential voltages, are given with respect to GND pin.

2. Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device.

3. ESD ratings including HV pin: HBM=400V, CDM=750V.

Electrical Characteristics

 $V_{\text{DD}}\text{=}15V$ and $T_{\text{A}}\text{=}25^{\circ}\text{C}$ unless noted.

Symbol		Parameter	Conditions	Min.	Тур.	Max.	Unit
HV Section	on		1				
$V_{\text{HV-MIN}}$	Minimum Startu	o Voltage on HV Pin				50	V
I _{HV}	Supply Current	Drawn from HV Pin	V _{AC} =90V, V _{DD} =0V, Controller Off	0.8	1.5	5.0	mA
I _{HV-LC}	Leakage Curren	t Drawn from HV Pin	With Auxiliary Supply, V_{HV} =500V, V_{DD} =15V, Controller On		0.8	3.0	μA
V _{DD} Secti	on						
V _{OP}	Continuously Op	peration Voltage				25	V
$V_{\text{DD-ON}}$	Turn-On Thresh	old Voltage		15	16	17	V
$V_{\text{DD-OFF}}$	Turn-Off Thresh	old Voltage		4.7	5.0	5.3	V
$V_{\text{DD-LH}}$	Threshold Voltag	ge for Latch-Off Release			2.50		V
I _{DD-ST}	Startup Current		$V_{DD}=V_{DD-ON}-0.16V$		400	450	μA
I _{DD-OP}	Operating Supply Current		V _{DD} =18V, f=f _{OSC} , C _L =1nF		3.5	4.0	mA
I _{DD-BURST}	Burst-Mode Ope	erating Supply Current	V _{DD} =8V, C _L =1nF		200	350	μA
V _{DD-OVP}	V _{DD} Over-Voltag	e Protection Level	Auto-Restart	25.5	26.5	27.5	V
t _{D-VDDOVP}	V _{DD} Over-Voltag Time	e Protection Debounce	f=85kHz		100	180	μs
Oscillato	r Section						
	_	Center Frequency	V _{CS} =5V, V _S =2.5, V _{FB} =5V	82	85	88	
fosc	Frequency	Hopping Range			±3		kHz
t _{FHR}	Frequency Hopp	bing Period			2.84		ms
f _{OSC-CM-MIN}	Minimum Frequency if CCM (Continuous Current Mode)			13	18	23	kHz
f _{osc-ссм}	Minimum Freque (Constant Curre	ency in CC Regulation nt Regulation)	V _{CS} =5V, V _S =0V	23	26	29	kHz
Feedback	Input Section						
Av	FB Input to Curr	ent Comparator Attenuation		1/3.5	1/3.0	1/2.5	V/V
Z _{FB}	Input Impedance	9		38	42	44	kΩ
V _{FB-OPEN}			FB Pin Open		5.3		V
$V_{\text{FB-G}}$	Green Mode En	ding Voltage		1.7	1.8	1.9	V
V _{FB-L}	Enter Zero Duty	Cycle of FB Voltage	V _{CS} =5V, V _S =0V	1.2	1.4	1.6	V
$V_{\text{FB-H}}$		/ Cycle of FB Voltage	V _{CS} =5V, V _S =0V	1.3	1.5	1.7	V
	perature Protect	· · ·	1		1	1	L
T _{OTP}	-	erature for Over-		+130	+140	+150	°C

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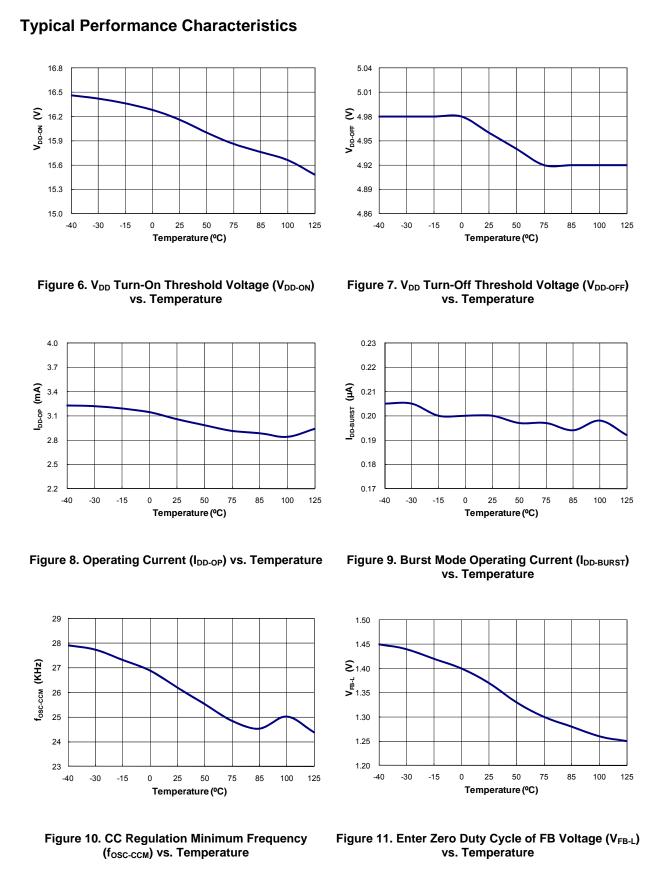
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Electrical Characteristics (Continued)

 $V_{\text{DD}}\text{=}15V$ and $T_{\text{A}}\text{=}25^{\circ}\text{C}$ unless noted.

Symbol	Parameter	Conditions	Min.	Тур.	Max.	Unit
Voltage-Se	ense Section					
I _{TC}	Bias Current	V _{CS} =5V	8.75	10.00	11.25	μA
V _{VS-CM-MIN}	V _S Threshold Voltage of ZCD Undetectable Protection			0.55		V
V _{VS-CM-MAX}	V _S Threshold Voltage of ZCD Undetectable Protection			0.75		V
V_{SN-CC}	Starting Voltage of Frequency Decreasing of CC	V _{CS} =5V, f _{S1} =f _{OSC} - 2KHz		2.15		V
V _{SG-CC}	Ending Voltage of Frequency Decreasing of CC		0.70		V	
S _{G-CC}	Frequency Decreasing Slop of CC Regulation	30	38	46	Hz/mV	
V _{VS-OFFSET}	ZCD Turn-Off Threshold			200		mV
V _{VS-OVP}	Output Over-Voltage Protection		2.7	2.80	2.85	V
t _{VS-OVP}	Output Over-Voltage Protection Debounce Time	f=85kHz		100	180	μs
Current-Se	ense Section					
V _{VR}	Reference Voltage		2.475	2.500	2.525	V
V _{CCR}	Variation Test Voltage on CS Pin for Constant Current Output	V _{CS} =0.47V	2.405	2.430	2.455	V
V _{STH}	Threshold Voltage for Current Limit			0.8		V
V _{STH-VA}	Threshold Voltage for Current Limit at Power Mode (V _{VS-CM-MAX} <0.75V)	V _{VS} =0.3V	0.25	0.30	0.35	V
t _{PD}	Propagation Delay to GATE Output			100	200	ns
t _{MIN}	Minimum On Time	V _{VS} =0V, V _{CS} =5V	430	530	630	ns
t _{LEB}	Leading-Edge Blanking Time		300	400	500	ns
VSLOPE	Slope Compensation	Maximum Duty Cycle		0.3		V
GATE Sec	tion					
DCY_{MAX}	Maximum Duty Cycle		64	67	70	%
$V_{\text{GATE-L}}$	Output Voltage Low	V_{DD} =25V, I_{O} =10mA			1.5	V
$V_{\text{GATE-H}}$	Output Voltage High	V _{DD} =8V, I _O =1mA	5		8	V
$V_{\text{GATE-H}}$	Output Voltage High	V_{DD} =5.5V, I _O =1mA	4.0		5.5	V
tr	Rising Time	V_{DD} =15V, C _L =1nF	100	140	180	ns
t _f	Falling Time	V_{DD} =15V, C _L =1nF	30	50	70	ns
V _{GATE-} CLAMP	Output Clamp Voltage	V _{DD} =25V	13	15	17	V

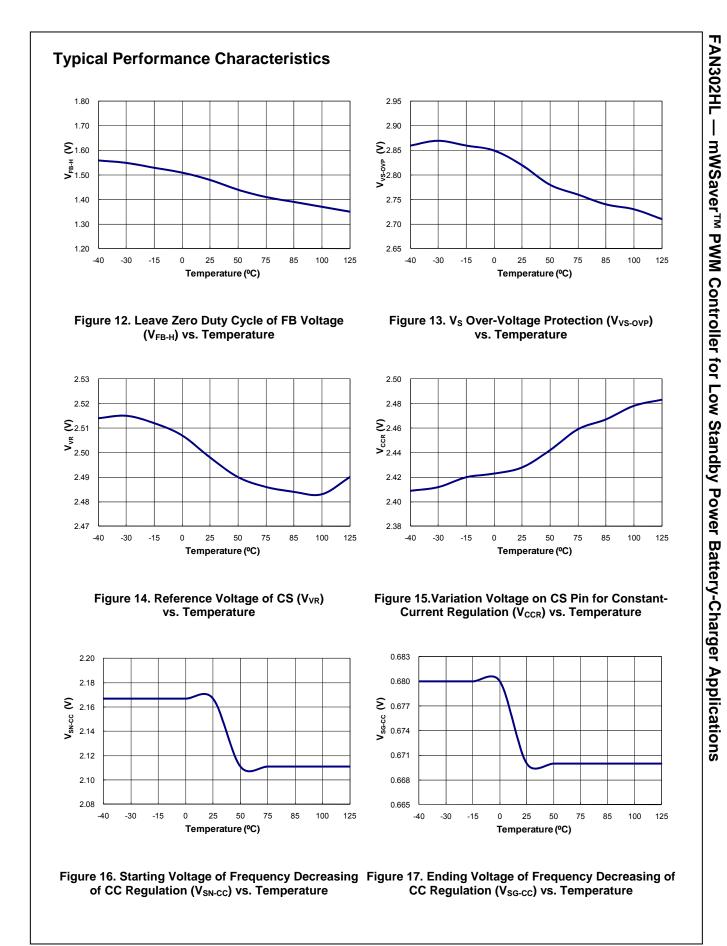
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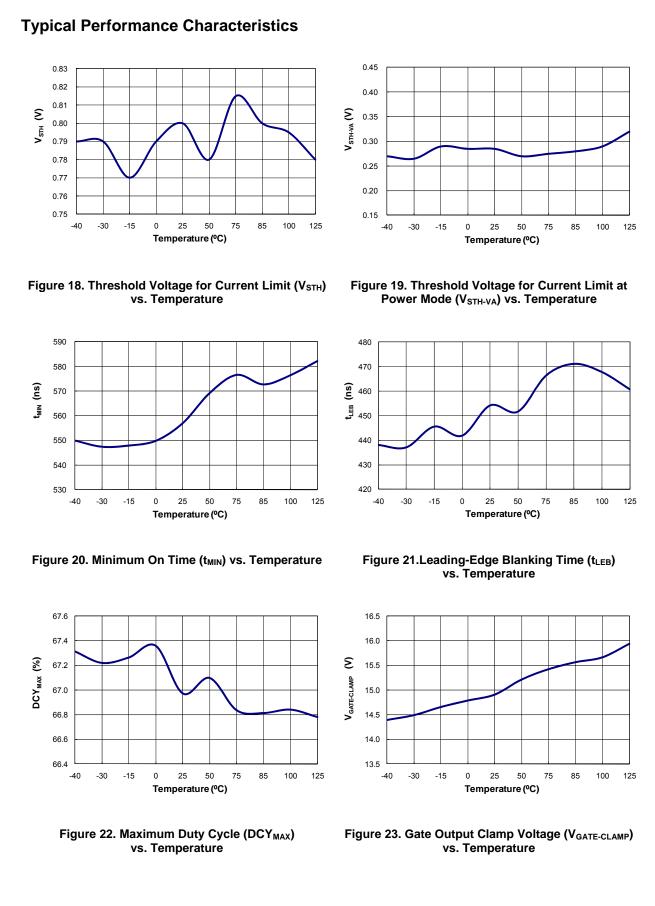


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FAN302HL — mWSaver™ PWM Controller for Low Standby Power Battery-Charger Applications





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FAN302HL — mWSaver™ PWM Controller for Low Standby Power Battery-Charger Applications

Operation Description

Constant-Voltage Regulation Operation

FAN302HL is the high-frequency and ultra-low standby power IC with Constant Voltage (CV) / Constant Current (CC) regulation.

When FAN302HL operates in CV regulation, the feedback voltage (V_{FB}) works as output load and modulates the PWM duty, as shown in Figure 24, causing fixed switching frequency (85kHz). Once the V_{FB} decreases below V_{FB-G}, frequency hopping is disabled and operation current decreases.

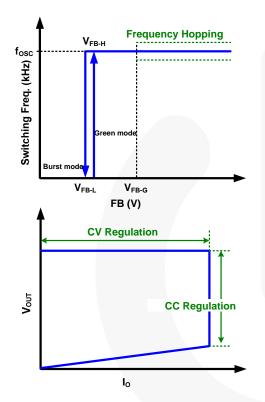


Figure 24. fosc vs. VFB in CV Regulation

Constant-Current Regulation Operation

During CC operation, the proprietary Primary-Side Regulation (PSR) topology simplifies circuit design without secondary feedback circuitry for battery-charger applications. The CC regulation achieved through PSR technique uses a mixed-signal algorithm to detect the primary-side current and to sample the voltage through primary-side auxiliary winding and calculate the average current on secondary side.

Figure 25 shows the basic circuit diagram of a flyback converter, with typical waveforms shown in Figure 26. Generally, Discontinuous Conduction Mode (DCM) operation is preferred for constant-current control since it allows better output regulation. The operation principles of DCM flyback converter are:

During the MOSFET on time (t_{ON}), input voltage (V_{DL}) is applied across the primary-side inductor (L_m). Then, MOSFET current (I_{ds}) increases linearly from zero to the

peak value (I_{pk}) . During this time, the energy is drawn from the input and stored in the inductor.

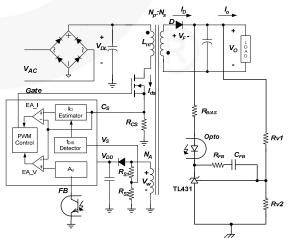
When the MOSFET is turned off, the energy stored in the inductor forces the rectifier diode (D) to be turned on. While the diode is conducting, the output voltage (V_O), together with diode forward voltage drop (V_F), are applied across the secondary-side inductor $(L_m \times N_s^2/N_p^2)$ and the diode current (I_D) decreases linearly from the peak value (I_pk×N_p/N_s) to zero. At the end of inductor current discharge time (t_{DIS}), all the energy stored in the inductor has been delivered to the output.

When the diode current reaches zero, V_S voltage drops quickly: if it is greater than the $V_{VS-OFFSET}$ drop voltage, the IC gets the t_{DIS} for CC regulation.

During the inductor current discharge time, the sum of output voltage and diode forward-voltage drop is reflected to the auxiliary winding side as $(V_O+V_F) \times N_a/N_s$. This voltage signal is proportional to the secondary winding. In constant-current output operation, this voltage signal is detected and examined by the precise constant-current regulation controller. The on time of the MOSFET is determined to control input power and provide constant-current output property. With feedback voltage V_{CS} across the current-sense resistor, the controller can obtain the input power of power supply. Therefore, the region of constant-current output operation can be adjusted by the current-sense resistor, as shown in Equation (1).

$$I_O = \frac{1}{2} \cdot i_{PK} \cdot \frac{N_P}{N_S} \cdot \frac{t_{DIS}}{t_s} = \frac{1}{2} \cdot \frac{N_P}{N_S} \cdot \frac{V_{CS}}{R_{CS}} \cdot \frac{t_{DIS}}{t_s}$$
(1)

During CC regulation, the V_S voltage decreases as output voltage decreases. The switching frequency reduces linearly from f_{OSC} to f_{OSC-CCM} as V_S voltage changes from V_{SN-CC} to V_{SG-CC}. Figure 27 shows the relationship between frequency and V_S voltage. Figure 28 shows the output V-I curve and V_S voltage.





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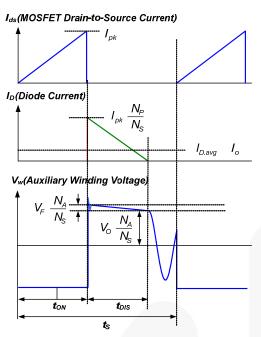
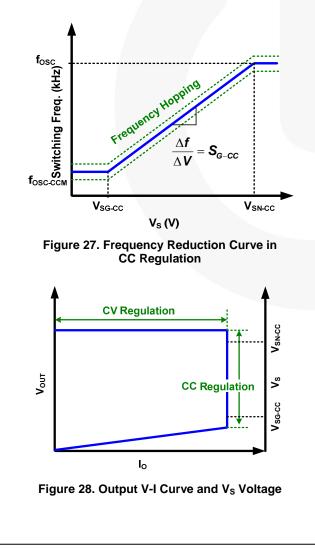


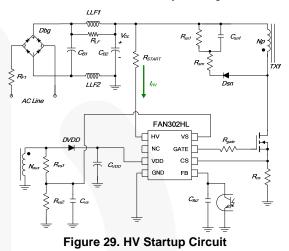
Figure 26. Waveforms of DCM Flyback Converter



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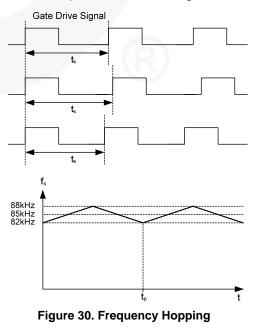
High-Voltage Startup

Figure 29 shows the high-voltage (HV) startup circuit for FAN302HL applications. The HV pin is connected to the line input or bulk capacitor through a resistor. During startup, the internal startup circuit is enabled and the line input supplies the current, I_{HV} , to charge the hold-up capacitor, C_{VDD} , through R_{START} . When the V_{DD} voltage reaches V_{DD-ON} , the internal HV startup circuit is disabled, blocking I_{HV} from flowing into the HV pin. Once the IC turns on, C_{VDD} is the only energy source to supply the IC consumption current before the PWM starts to switch. Therefore, C_{VDD} must be large enough to prevent V_{DD} from dropping to V_{DD-OFF} before the power can be delivered from the auxiliary winding.



Frequency Hopping

EMI reduction is accomplished by frequency hopping, which spreads the energy over a wider frequency range than the bandwidth measured by the EMI test equipment. The FAN302HL internal frequency-hopping circuit changes the switching frequency between 82kHz and 88kHz with a period, as shown in Figure 30.



Burst-Mode Operation

The power supply enters "Burst-Mode" at no-load conditions. As shown in Figure 31, when V_{FB} drops below V_{FBL} , the PWM output shuts off and the output voltage drops at a rate dependent on load current. This causes the feedback voltage to rise. Once V_{FB} exceeds V_{FBH} , the internal circuit starts to provide switching pulse. The feedback voltage then falls and the process repeats. Burst Mode operation alternately enables and disables switching of the MOSFET, reducing the switching losses in Standby Mode.

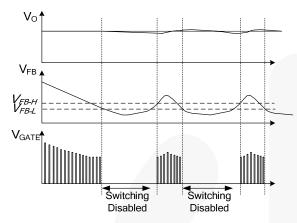


Figure 31. Burst-Mode Operation

Operating Current

The typical operating current is 3.5mA. This low operating current results in higher efficiency and reduces the V_{DD} hold-up capacitance requirement. Once FAN302HL enters Burst Mode, the operating current is reduced to 200µA, allowing the power supply to meet power conservation requirements.

Gate Output

The FAN302HL BiCMOS output stage is a fast totempole gate driver. Cross conduction has been avoided to minimize heat dissipation, increase efficiency, and enhance reliability. The output driver is clamped by an internal Zener diode to protect the power MOSFET transistors against over-voltage gate signals.

Slope Compensation

The sensed voltage across the current-sense resistor is used for Current-Mode control and pulse-by-pulse current limiting. Built-in slope compensation, a synchronized positively-sloped ramp built-in at each switching cycle, improves stability and prevents subharmonic oscillations due to Peak-Current Mode control.

Constant Power Mode Control

When $V_{\rm S}$ is lower than $V_{\rm S-CM-MIN},$ FAN302HL enters Constant-Power-Mode control, the primary-side current limit voltage (V_{CS}) changes from $V_{\rm STH}$ to $V_{\rm STH-VA}$ to avoid mis-sampling $V_{\rm S}$ through the Zero Current Detection (ZCD). Once $V_{\rm S}$ is higher than $V_{\rm S-CM-MAX},$ the $V_{\rm CS}$ returns to $V_{\rm STH}.$

Protections

The FAN302HL self-protection functions include V_{DD} Over-Voltage Protection (V_{DD} OVP), internal Over-Temperature Protection (OTP), V_S Over-Voltage Protection (V_S OVP), brownout protection, and pulse-by-pulse current limit.

The V_{DD} OVP protection is implemented as Auto-Restart Mode. Once an abnormal condition occurs, switching is terminated and the MOSFET remains off, causing V_{DD} to drop. When V_{DD} drops to the V_{DD} turn-off voltage of 5V, the internal startup circuit is enabled, and the supply current drawn from HV pin charges the hold-up capacitor. When V_{DD} reaches the turn-on voltage of 16V, FAN302HL resumes normal operation. In this manner, the auto-restart alternately enables and disables the switching of the MOSFET until the abnormal condition is eliminated (see Figure 32).

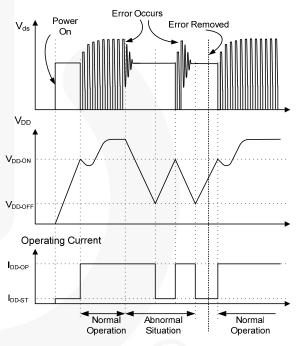


Figure 32. Auto-Restart Mode Operation

The V_S OVP and internal OTP protections are implemented as Latch Mode. If abnormal conditions occur, PWM switching is terminated and the MOSFET remains off. In this scenario, V_{DD} drops, but keeps working as auto-restart (V_{DD} auto-restart behavior doesn't trigger PWM pulses). FAN302HL enters Latch Mode, disables PWM switching of the MOSFET until V_{DD} is lower than V_{DD-LH} (AC power is removed), powers on again, then resumes normal operation (*see Figure 33*).

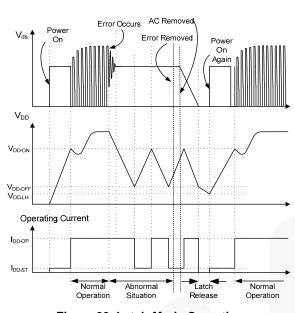


Figure 33. Latch-Mode Operation

V_S Over-Voltage Protection (OVP)

 $V_{\rm S}$ over-voltage protection prevents damage due to output over-voltage conditions. Figure 34 shows the $V_{\rm S}$ OVP protection method. When abnormal system conditions occur that cause $V_{\rm S}$ to exceed 2.8V, after a period of debounce time; PWM pulses are disabled and FAN302HL enters Latch Mode until $V_{\rm DD}$ drops to under $V_{\rm DD-LH}$. By that time, PWM pulses revive. $V_{\rm S}$ over-voltage conditions are usually caused by open feedback loops or abnormal behavior by the VS pin divider resistor.

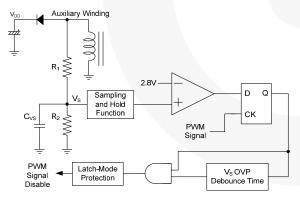


Figure 34. V_s OVP Protection

V_{DD} Over-Voltage Clamping

 V_{DD} over-voltage protection prevents damage due to over-voltage conditions. When the V_{DD} voltage exceeds 26.5V due to abnormal conditions, PWM pulses are disabled until the V_{DD} voltage drops below the UVLO, then starts again. Over-voltage conditions are usually caused by open feedback loops.

Over-Temperature Protection (OTP)

The FAN302HL temperature-sensing circuit shuts down PWM output if the junction temperature exceeds 140°C (T_{OTP}). The PWM pulses are disabled until V_{DD} voltage drops below the V_{DD-LH}.

Leading-Edge Blanking (LEB)

Each time the power MOSFET is switched on, a turn-on spike occurs at the sense resistor. To avoid premature termination of the switching pulse, a 350ns leading-edge blanking time is built in. Conventional RC filtering can therefore be omitted. During this blanking period, the current-limit comparator is disabled and it cannot switch off the gate driver.

Under Voltage Lockout (UVLO)

The turn-on and turn-off thresholds are fixed internally at 16V and 5V, respectively. During startup, the hold-up capacitor must be charged to 16V through the startup resistor to enable the FAN302HL. The hold-up capacitor continues to supply V_{DD} until power can be delivered from the auxiliary winding of the main transformer. V_{DD} must not drop below 5V during this startup process. This UVLO hysteresis window ensures that the hold-up capacitor is adequate to supply V_{DD} during startup.

Noise Immunity

Noise from the current sense or the control signal can cause significant pulse-width jitter, particularly in Continuous-Conduction Mode. While slope compensation helps alleviate these problems, further precautions should still be taken. Good placement and layout practices should be followed. Avoiding long PCB traces and component leads, locating compensation and filter components near the FAN302HL, and increasing the power MOS gate resistance are advised.

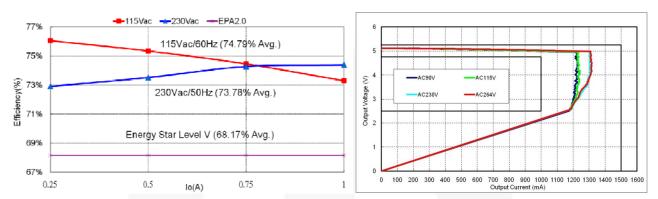
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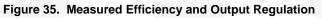
Typical Application Circuit (Flyback Charger)

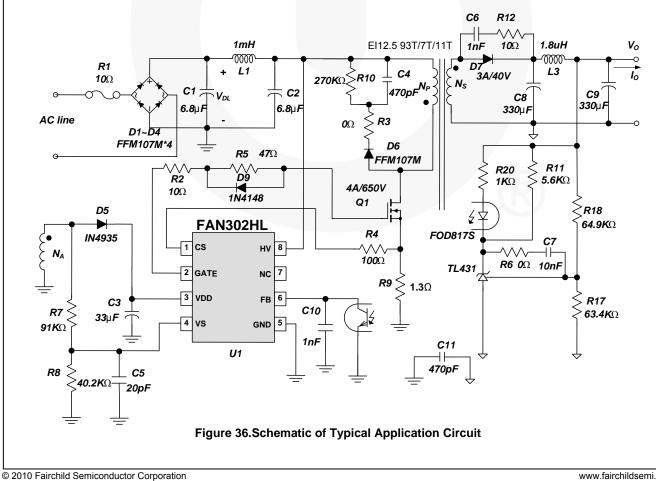
Application	Fairchild Devices	Input Voltage Range	Output
Cell Phone Charger	FAN302HL	90~265V _{AC}	5V/1.2A (6W)

Features

- High Efficiency (Avg. >71%), Meeting Energy Star V2.0 Standard (Avg. 68.17%)
- Ultra-Low Standby Power: Under 10mW at 230V_{AC} (Pin=6.3mW for 115V_{AC} and Pin=7.3mW for 230V_{AC}) .
- Output Regulation (CV: \pm 5%, CC: \pm 15%)







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Typical Application Circuit (Continued)

Transformer Specification

- Core: EI12.5
- Bobbin: EI12.5

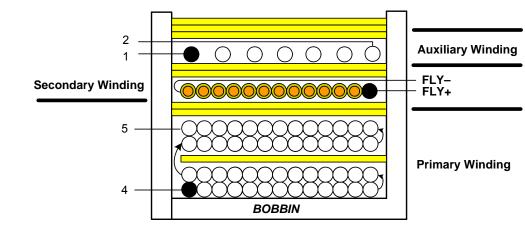


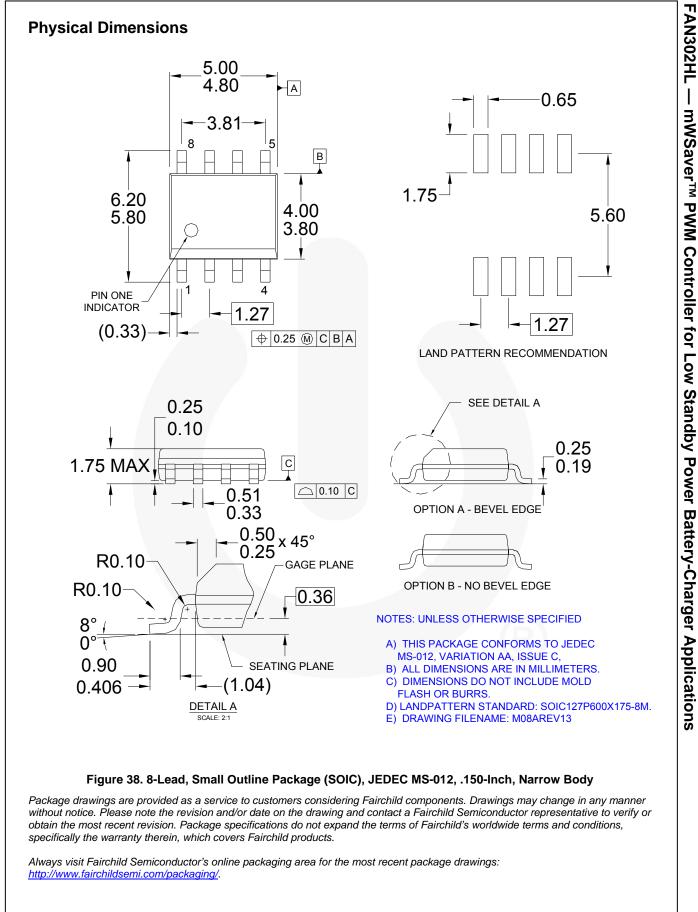
Figure 37.Transformer

- W1 is four winds; for each wind of turns, refer to Table 1. Add one insulating tape layer between the first and second layers.
- W2 is wound two layers and uses triple-insulated wire: end of positive fly line is 3.5cm, layer end of negative fly line is 2.5cm.
- W3 is spares winding in one layer.
- W4 is wound in the core of the outermost layer and sparse winding.

NO	Terminal		Wine	Turne	Insulation	
NO	Start Pin	End Pin	Wire	Turns	Turns	
				26	0	
W1	4	-		25	1	
		5	2UEW 0.1*1	24	0	
				18	2	
W2	Fly+	Fly-	TEX-E 0.45*1	7	2	
W3	1	2	2UEW 0.18*1	11	2	
			CORE ROUNDING TAPE		3	
			CORE		0	
W4	2		2UEW 0.18*1	5	2	

Table 1. Transformer Turns Specifications	Table 1.	Transforme	r Turns	Specifications
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	Pin	Specifications	Remark
Primary-Side Inductance	4-5	700μH ±7%	100kHz, 1V
Primary-Side Effective Leakage	4-5	200μH ±5%	Short one of the secondary windings.



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