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SPECIFICATIONS

ELECTRICAL CHARACTERISTICS—1.8 V OPERATION

V_{SY} = 1.8 V, V_{CM} = V_{SY}/2, T_A = 25°C, R_L = 100 kΩ to GND, unless otherwise noted.

Table 1.

Parameter	Symbol	Conditions	Min	Typ	Max	Unit
INPUT CHARACTERISTICS						
Offset Voltage	V_{OS}	0 V ≤ V_{CM} ≤ 1.8 V		0.5	2.5	mV
		−40°C ≤ T_A ≤ +125°C			3.5	mV
Input Bias Current	I_B			1	10	pA
		−40°C ≤ T_A ≤ +85°C			100	pA
		−40°C ≤ T_A ≤ +125°C			600	pA
Input Offset Current	I_{OS}			0.5	5	pA
		−40°C ≤ T_A ≤ +85°C			50	pA
		−40°C ≤ T_A ≤ +125°C			100	pA
Input Voltage Range		−40°C ≤ T_A ≤ +125°C	0		1.8	V
Common-Mode Rejection Ratio	CMRR	0 V ≤ V_{CM} ≤ 1.8 V	85	100		dB
		−40°C ≤ T_A ≤ +85°C	85			dB
		−40°C ≤ T_A ≤ +125°C	80			dB
Large-Signal Voltage Gain	A_{VO}	0.05 V ≤ V_{OUT} ≤ 1.75 V, R_L = 100 kΩ to V_{CM}	95	115		dB
		−40°C ≤ T_A ≤ +125°C	95			dB
Offset Voltage Drift	$\Delta V_{OS}/\Delta T$	−40°C ≤ T_A ≤ +125°C		2.5		µV/°C
Input Resistance	R_{IN}			220		GΩ
Input Capacitance, Differential Mode	C_{INDM}			3		pF
Input Capacitance, Common Mode	C_{INCM}			4.2		pF
OUTPUT CHARACTERISTICS						
Output Voltage High	V_{OH}	R_L = 100 kΩ to GND	1.78	1.79		V
		−40°C ≤ T_A ≤ +125°C	1.78			V
		R_L = 10 kΩ to GND	1.65	1.75		V
		−40°C ≤ T_A ≤ +125°C	1.65			V
Output Voltage Low	V_{OL}	R_L = 100 kΩ to V_{SY}		2	5	mV
		−40°C ≤ T_A ≤ +125°C			5	mV
		R_L = 10 kΩ to V_{SY}		12	25	mV
		−40°C ≤ T_A ≤ +125°C			25	mV
Short-Circuit Limit	I_{SC}	V_{OUT} = V_{SY} or GND		±4.5		mA
POWER SUPPLY						
Power Supply Rejection Ratio	PSRR	V_{SY} = 1.8 V to 5 V	100	110		dB
		−40°C ≤ T_A ≤ +85°C	100			dB
		−40°C ≤ T_A ≤ +125°C	95			dB
Supply Current per Amplifier	I_{SY}					
AD8506/AD8508		V_{OUT} = V_{SY}/2		16.5	20	µA
		−40°C ≤ T_A ≤ +125°C			25	µA
AD8505		V_{OUT} = V_{SY}/2		16.5	24	µA
		−40°C ≤ T_A ≤ +125°C			27.5	µA
DYNAMIC PERFORMANCE						
Slew Rate	SR	R_L = 100 kΩ, C_L = 10 pF, G = 1		13		mV/µs
Gain Bandwidth Product	GBP	R_L = 1 MΩ, C_L = 20 pF, G = 1		95		kHz
Phase Margin	Φ_M	R_L = 1 MΩ, C_L = 20 pF, G = 1		60		Degrees
NOISE PERFORMANCE						
Voltage Noise	e_n p-p	f = 0.1 Hz to 10 Hz		2.8		µV p-p
Voltage Noise Density	e_n	f = 1 kHz		45		nV/√Hz
Current Noise Density	i_n	f = 1 kHz		15		fA/√Hz

ELECTRICAL CHARACTERISTICS—5 V OPERATION

V_{SY} = 5 V, V_{CM} = V_{SY}/2, T_A = 25°C, R_L = 100 kΩ to GND, unless otherwise noted.

Table 2.

Parameter	Symbol	Conditions	Min	Typ	Max	Unit
INPUT CHARACTERISTICS						
Offset Voltage	V_{OS}	0 V ≤ V_{CM} ≤ 5 V		0.5	2.5	mV
		−40°C ≤ T_A ≤ +125°C			3.5	mV
Input Bias Current	I_B			1	10	pA
		−40°C ≤ T_A ≤ +85°C			100	pA
		−40°C ≤ T_A ≤ +125°C			600	pA
Input Offset Current	I_{OS}			0.5	5	pA
		−40°C ≤ T_A ≤ +85°C			50	pA
		−40°C ≤ T_A ≤ +125°C			130	pA
Input Voltage Range		−40°C ≤ T_A ≤ +125°C	0		5	V
Common-Mode Rejection Ratio	CMRR	0 V ≤ V_{CM} ≤ 5 V	90	105		dB
		−40°C ≤ T_A ≤ +85°C	90			dB
		−40°C ≤ T_A ≤ +125°C	85			dB
Large-Signal Voltage Gain	A_{VO}	0.05 V ≤ V_{OUT} ≤ 4.95 V, R_L = 100 kΩ to V_{CM}	105	120		dB
		−40°C ≤ T_A ≤ +125°C	100			dB
Offset Voltage Drift	$\Delta V_{OS}/\Delta T$	−40°C ≤ T_A ≤ +125°C		2		µV/°C
Input Resistance	R_{IN}			220		GΩ
Input Capacitance, Differential Mode	C_{INDM}			3		pF
Input Capacitance, Common Mode	C_{INCM}			4.2		pF
OUTPUT CHARACTERISTICS						
Output Voltage High	V_{OH}	R_L = 100 kΩ to GND	4.98	4.99		V
		−40°C ≤ T_A ≤ +125°C	4.98			V
		R_L = 10 kΩ to GND	4.9	4.95		V
		−40°C ≤ T_A ≤ +125°C	4.9			V
Output Voltage Low	V_{OL}	R_L = 100 kΩ to V_{SY}		2	5	mV
		−40°C ≤ T_A ≤ +125°C			5	mV
		R_L = 10 kΩ to V_{SY}		10	25	mV
		−40°C ≤ T_A ≤ +125°C			30	mV
Short-Circuit Limit	I_{SC}	V_{OUT} = V_{SY} or GND		±45		mA
POWER SUPPLY						
Power Supply Rejection Ratio	PSRR	V_{SY} = 1.8 V to 5 V	100	110		dB
		−40°C ≤ T_A ≤ +85°C	100			dB
		−40°C ≤ T_A ≤ +125°C	95			dB
Supply Current per Amplifier	I_{SY}					
AD8506/AD8508		V_{OUT} = V_{SY}/2		15	20	µA
		−40°C ≤ T_A ≤ +125°C			25	µA
AD8505		−40°C ≤ T_A ≤ +125°C			25.5	µA
DYNAMIC PERFORMANCE						
Slew Rate	SR	R_L = 100 kΩ, C_L = 10 pF, G = 1		13		mV/µs
Gain Bandwidth Product	GBP	R_L = 1 MΩ, C_L = 20 pF, G = 1		95		kHz
Phase Margin	Φ_M	R_L = 1 MΩ, C_L = 20 pF, G = 1		60		Degrees
NOISE PERFORMANCE						
Voltage Noise	e_n p-p	f = 0.1 Hz to 10 Hz		2.8		µV p-p
Voltage Noise Density	e_n	f = 1 kHz		45		nV/√Hz
Current Noise Density	i_n	f = 1 kHz		15		fA/√Hz

ABSOLUTE MAXIMUM RATINGS

Table 3.

Parameter	Rating
Supply Voltage	5.5 V
Input Voltage	$\pm V_{SY} \pm 0.1$ V
Input Current[1]	± 10 mA
Differential Input Voltage[2]	$\pm V_{SY}$
Output Short-Circuit Duration to GND	Indefinite
Storage Temperature Range	−65°C to +150°C
Operating Temperature Range	−40°C to +125°C
Junction Temperature Range	−65°C to +150°C
Lead Temperature (Soldering, 60 sec)	300°C

[1] Input pins have clamp diodes to the supply pins. The input current must be limited to 10 mA or less whenever the input signal exceeds the power supply rail by 0.5 V.

[2] The differential input voltage is limited to 5 V or the supply voltage, whichever is less.

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

THERMAL RESISTANCE

θ_{JA} is specified for the worst-case conditions, that is, a device soldered in a circuit board for surface-mount packages with its exposed paddle soldered to a pad, if applicable. Table 4 shows simulated thermal values for a 4-layer (2S2P) JEDEC standard thermal test board, unless otherwise specified.

Table 4.

Package Type	θ_{JA}	θ_{JC}	Unit
5-Lead SOT-23 (RJ-5)	190	92	°C/W
6-Ball WLCSP (CB-6-7)	105	N/A	°C/W
8-Lead MSOP (RM-8)	142	45	°C/W
8-Ball WLCSP (CB-8-2)	82	N/A	°C/W
14-Lead TSSOP (RU-14)	112	35	°C/W
14-Ball WLCSP (CB-14-1)	64	N/A	°C/W

ESD CAUTION

ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

TYPICAL PERFORMANCE CHARACTERISTICS
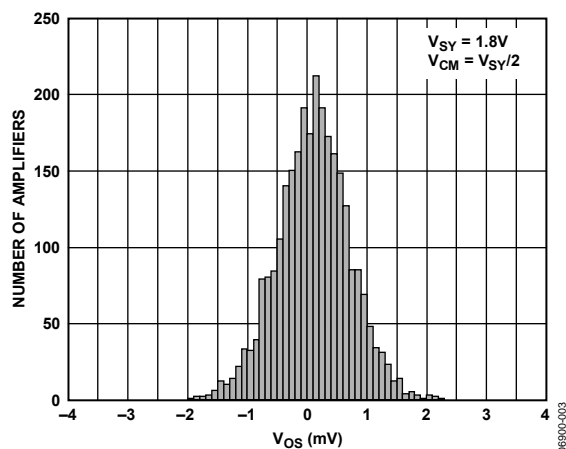
$T_A = 25°C$, unless otherwise noted.

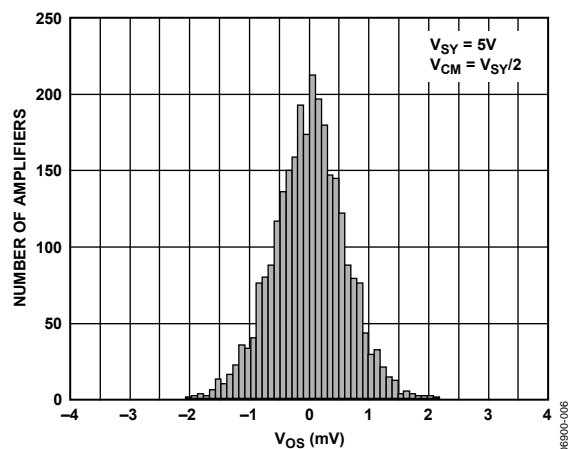Figure 7. Input Offset Voltage Distribution

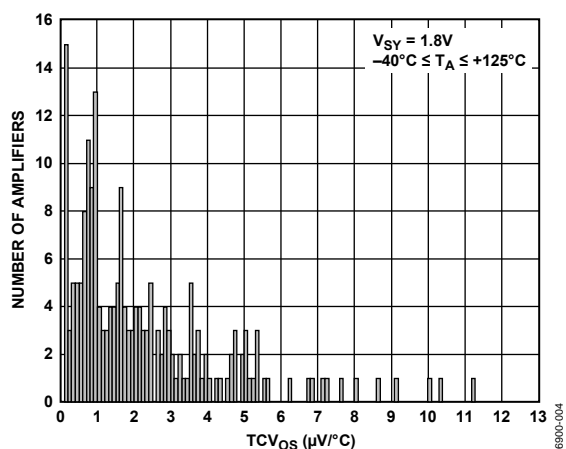Figure 10. Input Offset Voltage Distribution

Figure 8. Input Offset Voltage Drift Distribution
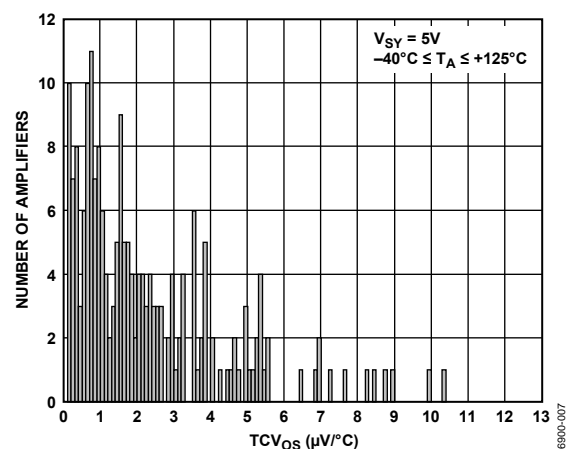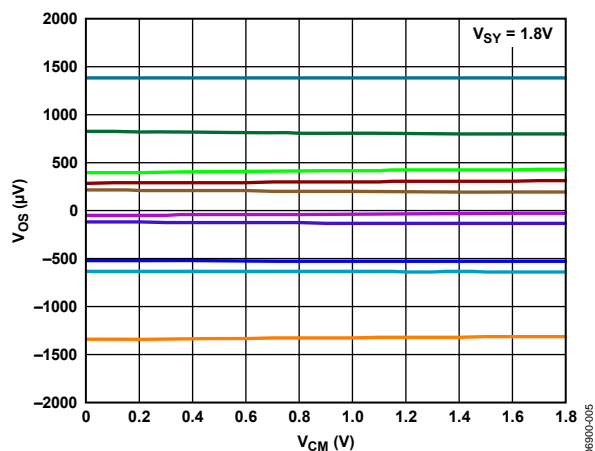

Figure 11. Input Offset Voltage Drift Distribution

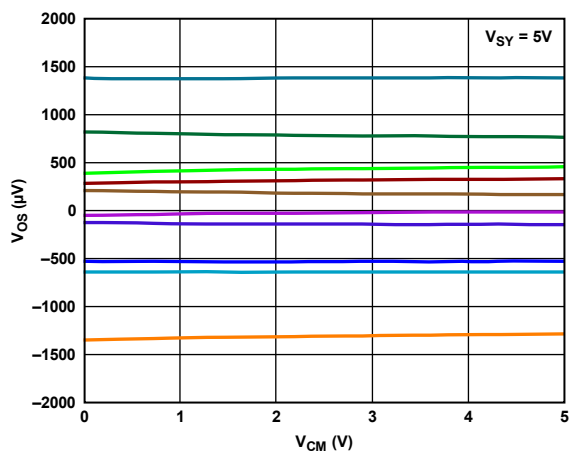Figure 9. Input Offset Voltage vs. Input Common-Mode Voltage

Figure 12. Input Offset Voltage vs. Input Common-Mode Voltage
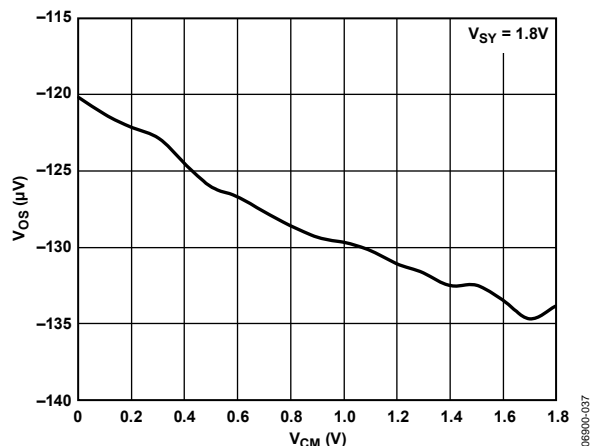
T$_A$ = 25°C, unless otherwise noted.

Figure 13. Input Offset Voltage vs. Input Common-Mode Voltage
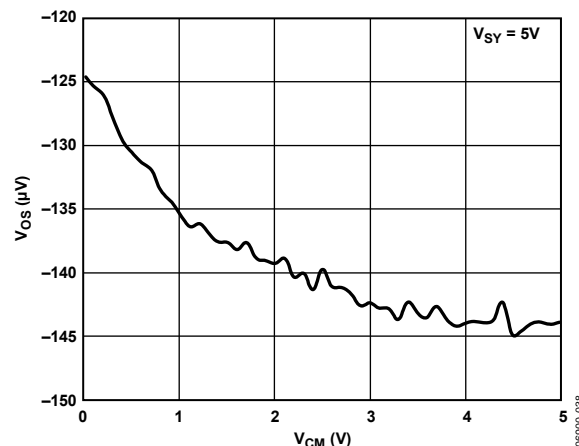

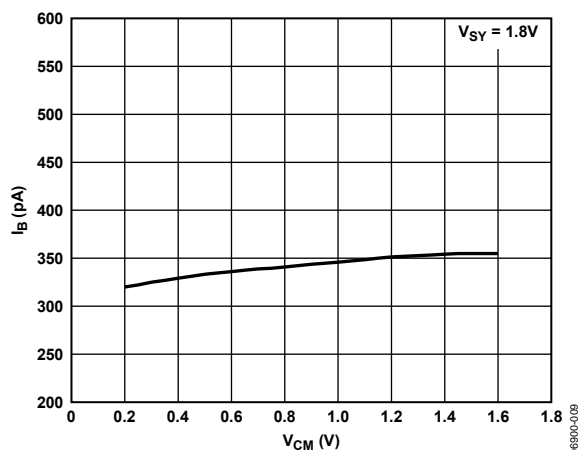Figure 16. Input Offset Voltage vs. Input Common-Mode Voltage

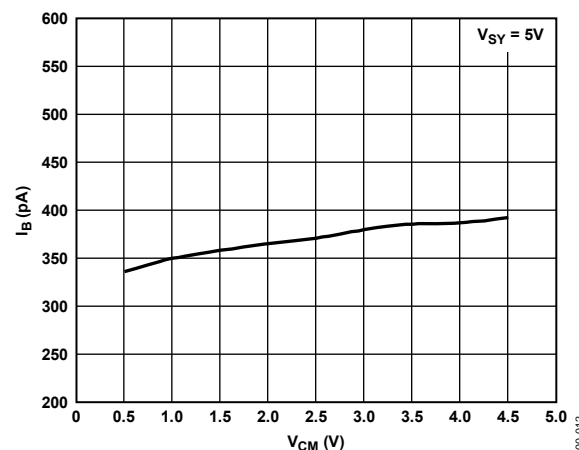Figure 14. Input Bias Current vs. Input Common-Mode Voltage at 125°C

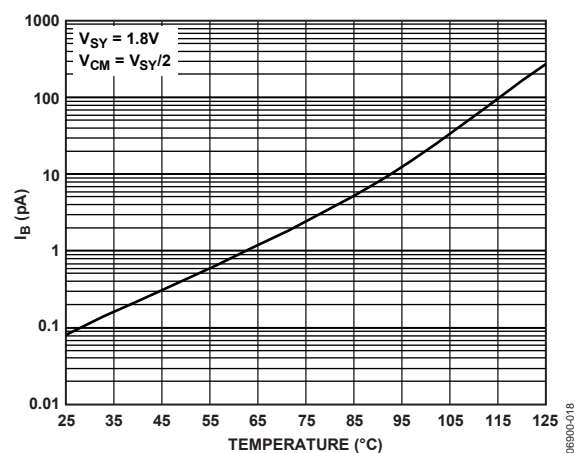Figure 17. Input Bias Current vs. Input Common-Mode Voltage at 125°C

Figure 15. Input Bias Current vs. Temperature
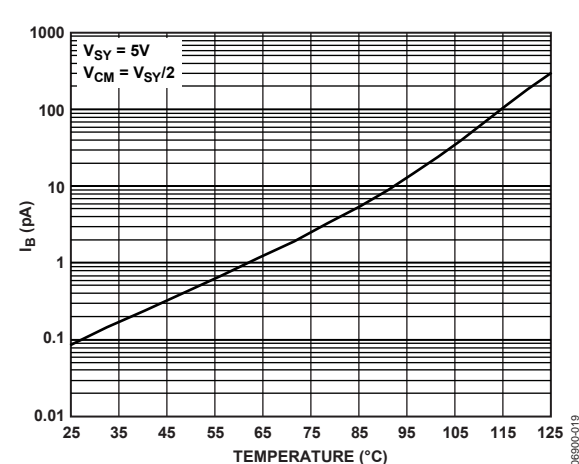
Figure 18. Input Bias Current vs. Temperature

$T_A = 25°C$, unless otherwise noted.
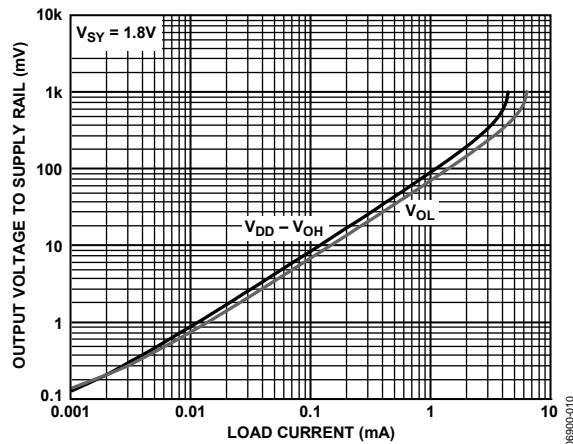
Figure 19. Output Voltage to Supply Rail vs. Load Current
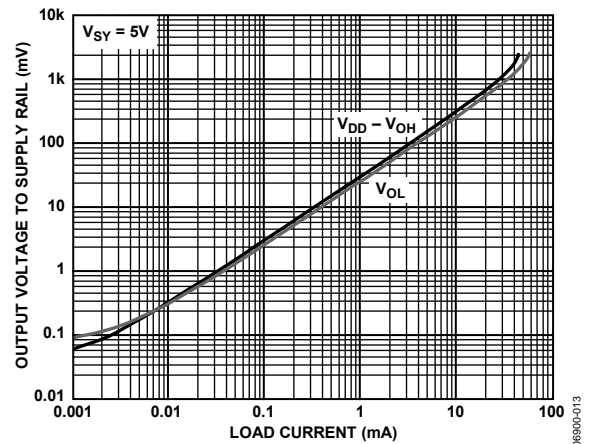
Figure 22. Output Voltage to Supply Rail vs. Load Current
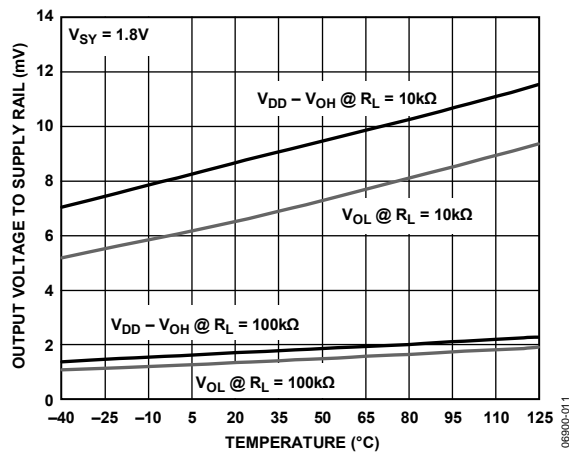
Figure 20. Output Voltage to Supply Rail vs. Temperature
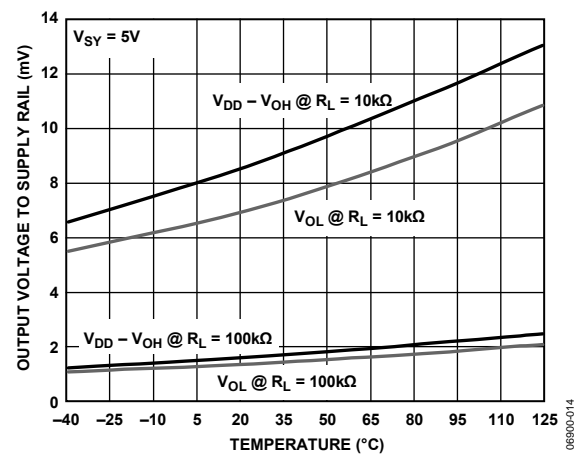
Figure 23. Output Voltage to Supply Rail vs. Temperature
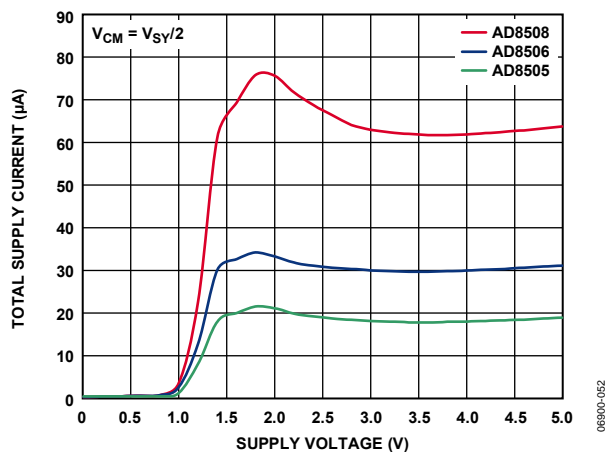
Figure 21. Total Supply Current vs. Supply Voltage
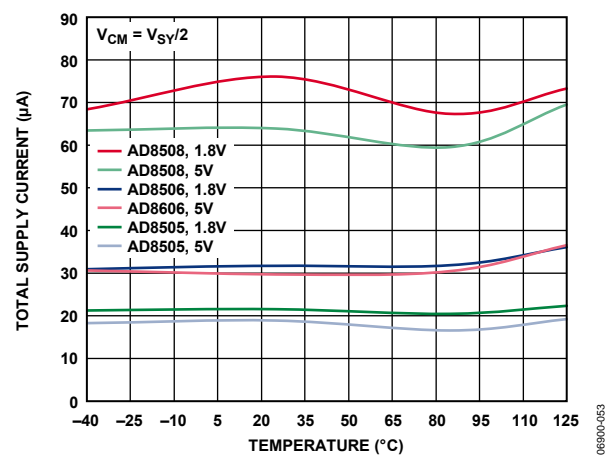
Figure 24. Total Supply Current vs. Temperature

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$T_A = 25°C$, unless otherwise noted.
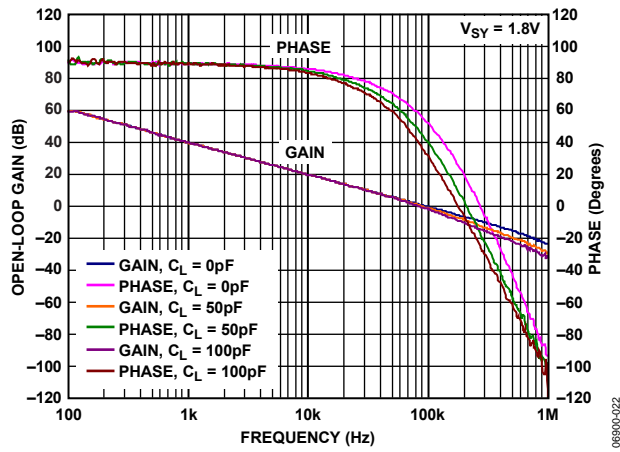
Figure 25. Open-Loop Gain and Phase vs. Frequency
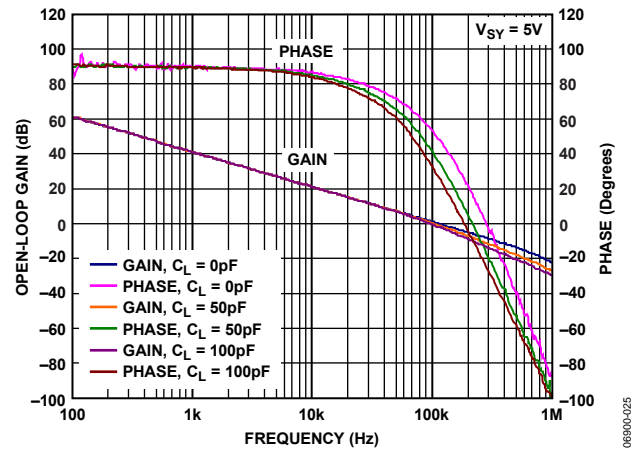
Figure 28. Open-Loop Gain and Phase vs. Frequency
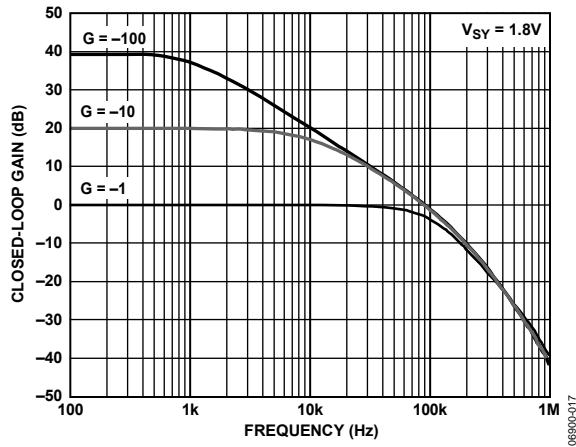
Figure 26. Closed-Loop Gain vs. Frequency
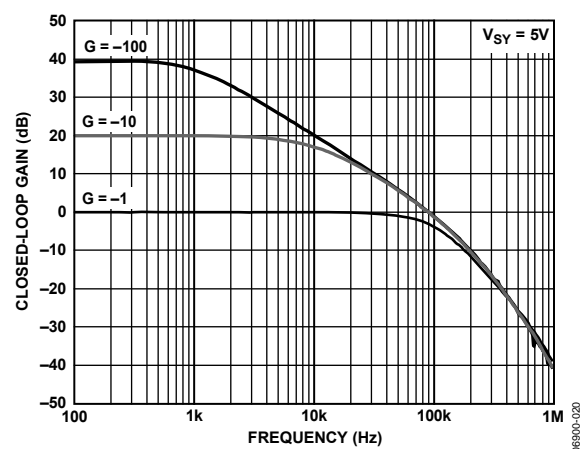
Figure 29. Closed-Loop Gain vs. Frequency
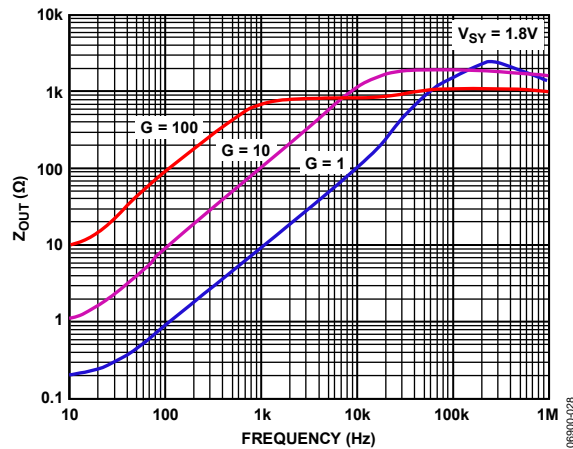
Figure 27. Z_{OUT} vs. Frequency
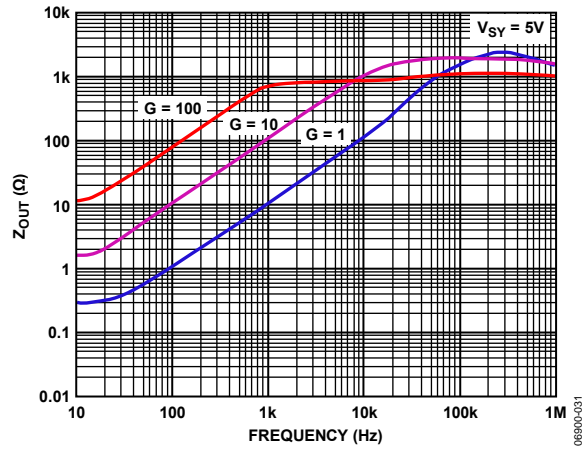
Figure 30. Z_{OUT} vs. Frequency

$T_A = 25°C$, unless otherwise noted.
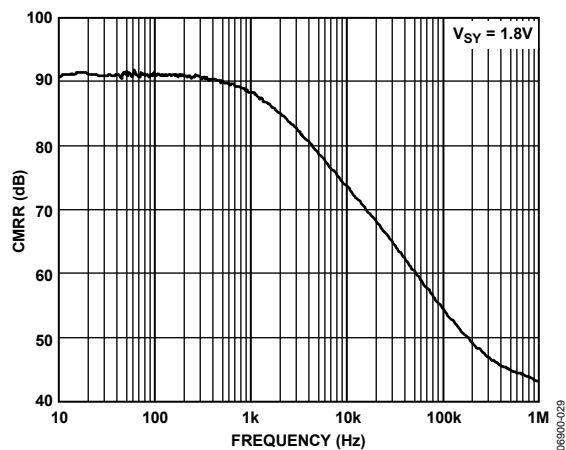
Figure 31. CMRR vs. Frequency
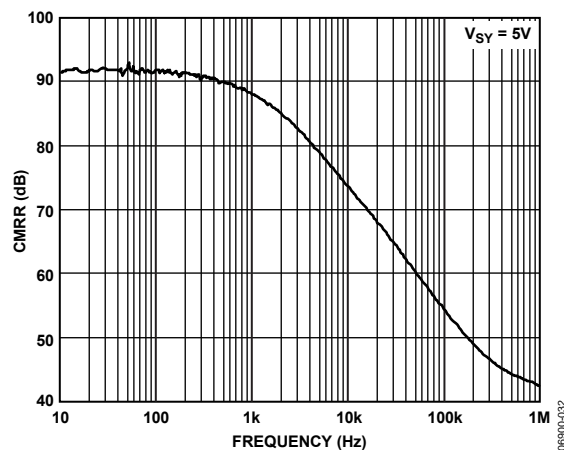
Figure 34. CMRR vs. Frequency
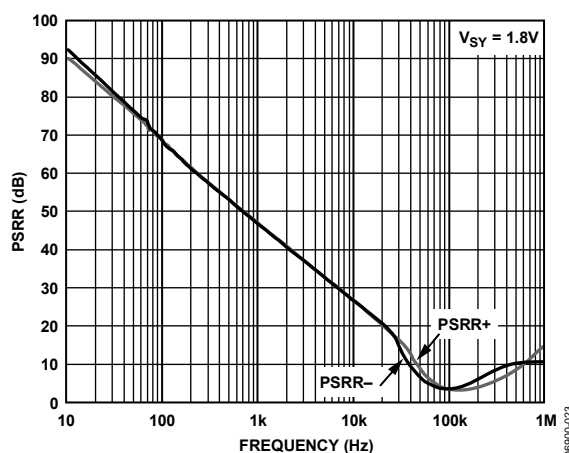
Figure 32. PSRR vs. Frequency
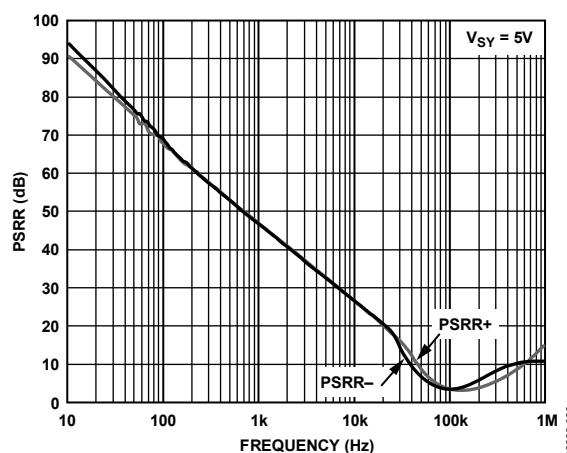
Figure 35. PSRR vs. Frequency
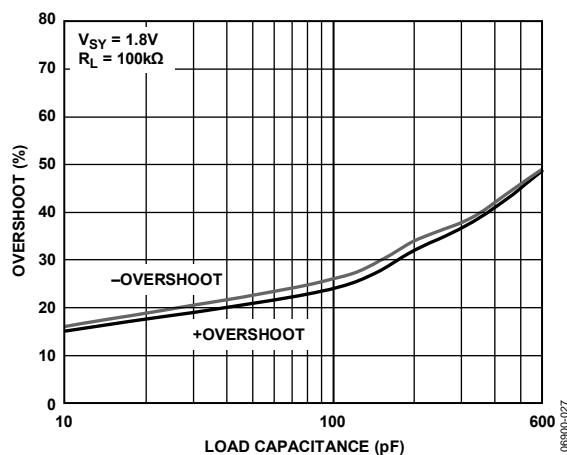
Figure 33. Small-Signal Overshoot vs. Load Capacitance
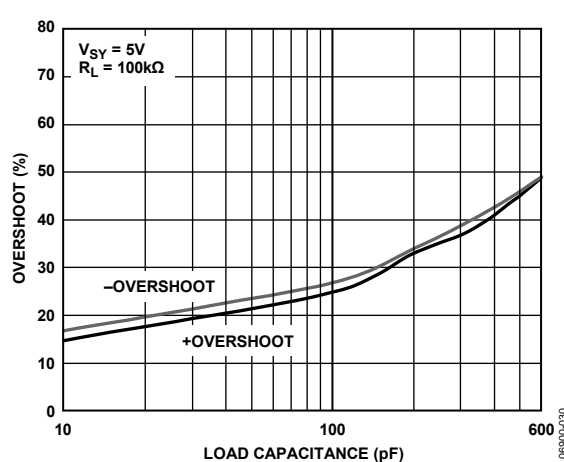
Figure 36. Small-Signal Overshoot vs. Load Capacitance

T_A = 25°C, unless otherwise noted.
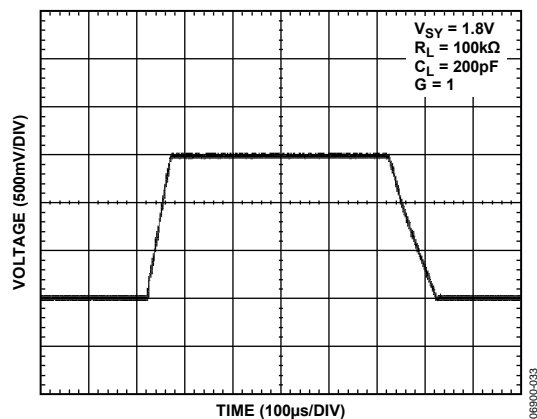
Figure 37. Large-Signal Transient Response
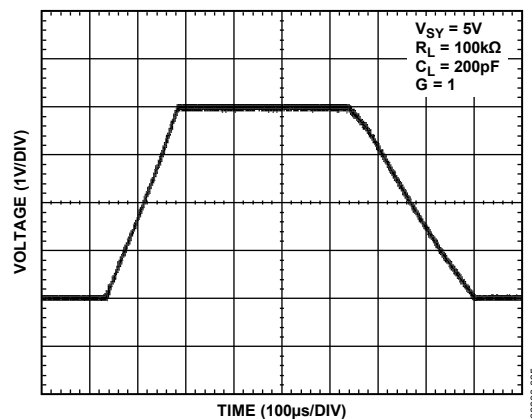
Figure 40. Large-Signal Transient Response
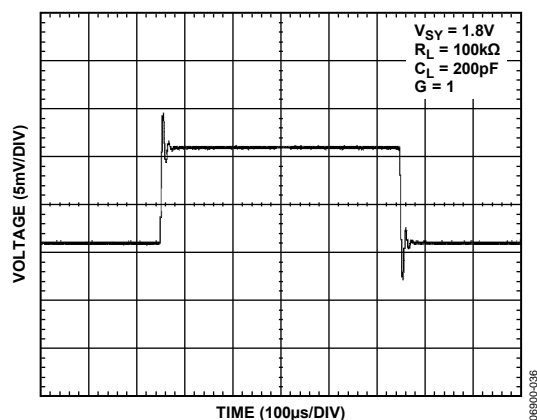
Figure 38. Small-Signal Transient Response
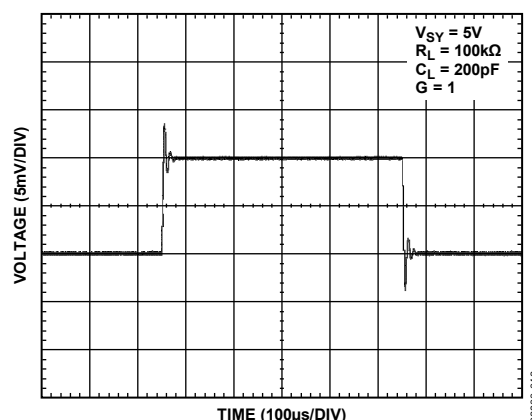
Figure 41. Small-Signal Transient Response
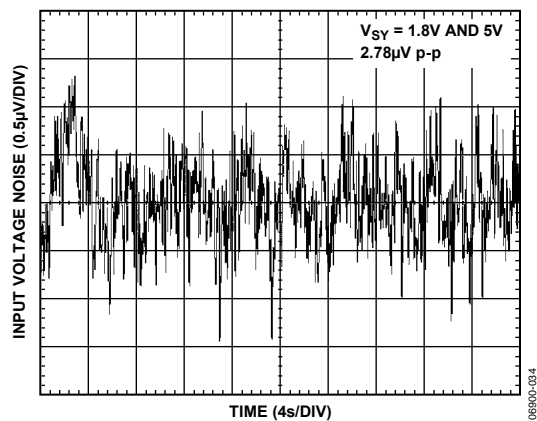
Figure 39. Input Voltage Noise 0.1 Hz to 10 Hz
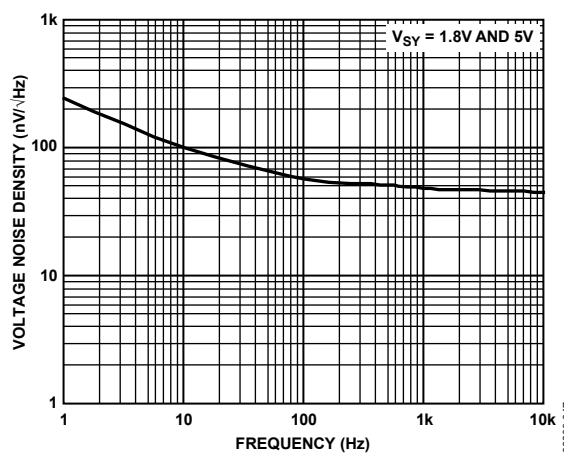
Figure 42. Voltage Noise Density vs. Frequency

$T_A = 25°C$, unless otherwise noted.
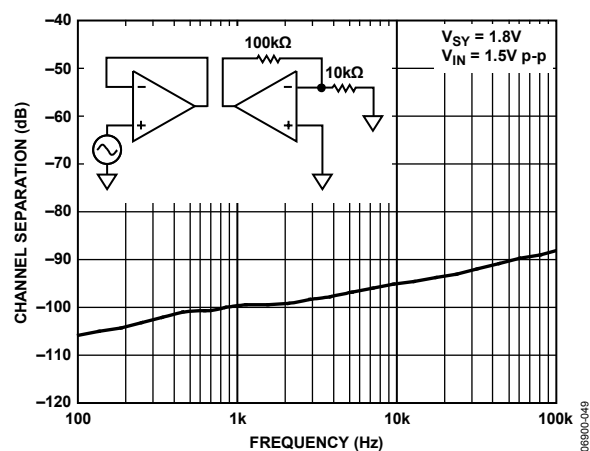
Figure 43. Channel Separation vs. Frequency
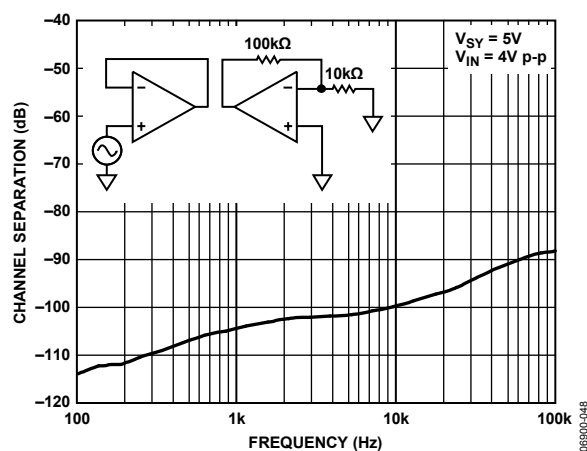
Figure 44. Channel Separation vs. Frequency

THEORY OF OPERATION

The AD8505/AD8506/AD8508 are unity-gain, stable, CMOS, rail-to-rail input/output operational amplifiers designed to optimize performance in current consumption, PSRR, CMRR, and zero crossover distortion, all embedded in a small package. The typical offset voltage is 500 μV, with a low peak-to-peak voltage noise of 2.8 μV from 0.1 Hz to 10 Hz and a voltage noise density of 45 nV/√Hz at 1 kHz.

The AD8505/AD8506/AD8508 amplifiers are designed to solve two key problems in low voltage battery-powered applications: the battery voltage decrease over time and the rail-to-rail input stage distortion.

In battery-powered applications, the supply voltage available to the IC is the voltage of the battery. Unfortunately, the voltage of a battery decreases as it discharges itself through the load. This voltage drop over the lifetime of the battery causes an error in the output of the op amps. Some applications requiring precision measurements during the entire lifetime of the battery use voltage regulators to power up the op amps as a solution. If a design uses standard battery cells, the op amps experience a supply voltage change from roughly 3.2 V to 1.8 V during the lifetime of the battery. This means that for a PSRR of 70 dB minimum in a typical op amp, the input-referred offset error is approximately 440 μV. If the same application uses the AD8505/AD8506/AD8508 amplifiers with a 100 dB minimum PSRR, the error is only 14 μV. It is possible to calibrate out this error or to use an external voltage regulator to power the op amp, but these solutions can increase system cost and complexity. The AD8505/AD8506/AD8508 amplifiers solve the impasse with no additional cost or error-nullifying circuitry.

The second problem with battery-powered applications is the distortion caused by the standard rail-to-rail input stage. Using a CMOS non-rail-to-rail input stage (that is, a single differential pair) limits the input voltage to approximately one V_{GS} (gate-source voltage) away from one of the supply lines. Because V_{GS} for normal operation is commonly over 1 V, a single differential pair input stage op amp greatly restricts the allowable input voltage range when using a low supply voltage. This limitation restricts the number of applications where the non-rail-to-rail input op amp was originally intended to be used. To solve this problem, a dual differential pair input stage is usually implemented (see Figure 45); however, this technique has its own drawbacks.

One differential pair amplifies the input signal when the common-mode voltage is on the high end, whereas the other pair amplifies the input signal when the common-mode voltage is on the low end. This method also requires control circuitry to operate the two differential pairs appropriately. Unfortunately, this topology leads to a very noticeable and undesirable problem: if the signal level moves through the range where one input stage turns off and the other one turns on, noticeable distortion occurs (see Figure 46).
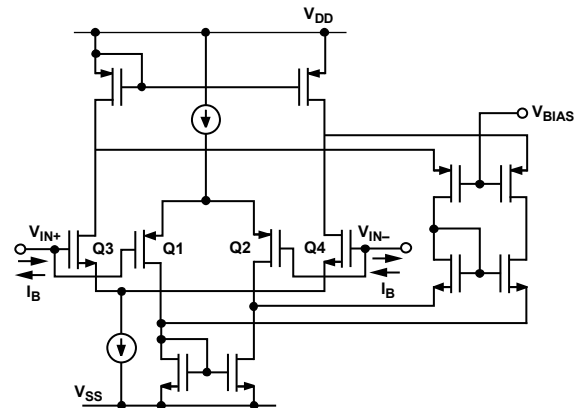
Figure 45. A Typical Dual Differential Pair Input Stage Op Amp (Dual PMOS Q1 and Q2 Transistors Form the Lower End of the Input Voltage Range, Whereas Dual NMOS Q3 and Q4 Compose the Upper End)
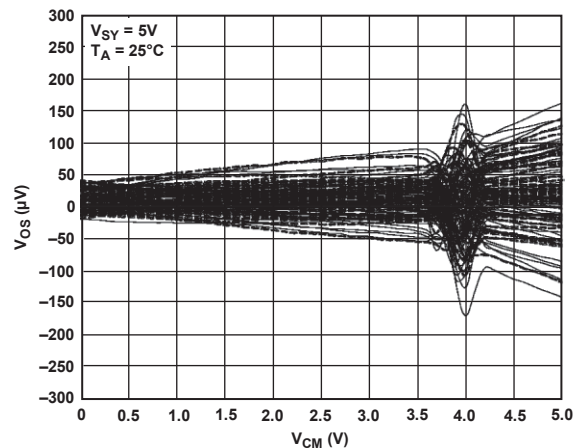
Figure 46. Typical Input Offset Voltage vs. Common-Mode Voltage Response in a Dual Differential Pair Input Stage Op Amp (Powered by 5 V Supply; Results of Approximately 100 Units per Graph Are Displayed)

This distortion forces the designer to devise impractical ways to avoid the crossover distortion areas, therefore narrowing the common-mode dynamic range of the operational amplifier. The AD8505/AD8506/AD8508 amplifiers solve this crossover distortion problem by using an on-chip charge pump to power the input differential pair. The charge pump creates a supply voltage higher than the voltage of the battery, allowing the input stage to handle a wide range of input signal voltages without using a second differential pair. With this solution, the input voltage can vary from one supply extreme to the other with no distortion, thereby restoring the full common-mode dynamic range of the op amp.

The charge pump has been carefully designed so that switching noise components at any frequency, both within and beyond the amplifier bandwidth, are much lower than the thermal noise floor. Therefore, the spurious-free dynamic range (SFDR) is limited only by the input signal and the thermal or flicker noise. There is no intermodulation between the input signal and the switching noise.

Figure 47 displays a typical front-end section of an operational amplifier with an on-chip charge pump.
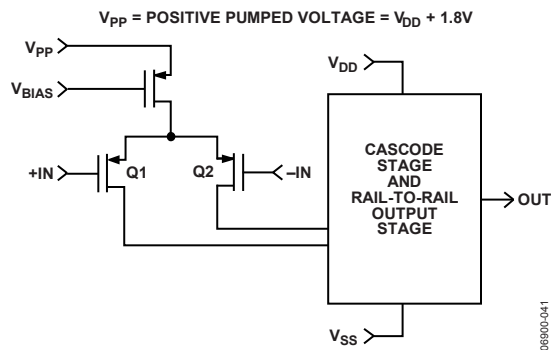
Figure 47. Typical Front-End Section of an Op Amp
with Embedded Charge Pump

Figure 48, the input offset voltage vs. input common-mode voltage response, shows the typical response of 12 devices. Figure 48 is expanded to make it easier to compare with Figure 46, the typical input offset voltage vs. common-mode voltage response in a dual differential pair input stage op amp.
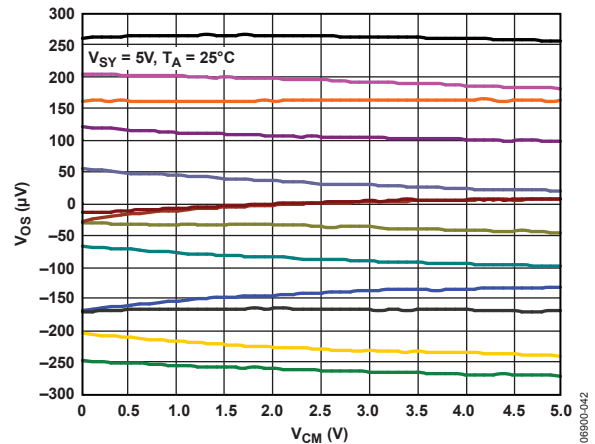
Figure 48. Input Offset Voltage vs. Input Common-Mode Voltage Response
(Powered by a 5 V Supply; Results of 12 Units Are Displayed)

This solution improves the CMRR performance tremendously. For instance, if the input varies from rail to rail on a 2.5 V supply rail, using a part with a CMRR of 70 dB minimum, an input-referred error of 790 μV is introduced. Another part with a CMRR of 52 dB minimum generates a 6.3 mV error. The AD8505/AD8506/AD8508 CMRR of 90 dB minimum causes only a 79 μV error. As with the PSRR error, there are complex ways to minimize this error, but the AD8505/AD8506/AD8508 amplifiers solve this problem without incurring unnecessary circuitry complexity or increased cost.

APPLICATIONS INFORMATION

PULSE OXIMETER CURRENT SOURCE

A pulse oximeter is a noninvasive medical device used for continuously measuring the percentage of hemoglobin (Hb) saturated with oxygen and the pulse rate of a patient. Hemoglobin that is carrying oxygen (oxyhemoglobin) absorbs light in the infrared (IR) region of the spectrum; hemoglobin that is not carrying oxygen (deoxyhemoglobin) absorbs visible red (R) light. In pulse oximetry, a clip containing two LEDs (sometimes more, depending on the complexity of the measurement algorithm) and the light sensor (photodiode) is placed on the finger or earlobe of the patient. One LED emits red light (600 nm to 700 nm) and the other emits light in the near IR (800 nm to 900 nm) region. The clip is connected by a cable to a processor unit. The LEDs are rapidly and sequentially excited by two current sources (one for each LED), whose dc levels depend on the LED being driven, based on manufacturer requirements, and the detector is synchronized to capture the light from each LED as it is transmitted through the tissue.

An example design of a dc current source driving the red and infrared LEDs is shown in Figure 49. These dc current sources allow 62.5 mA and 101 mA to flow through the red and infrared LEDs, respectively. First, to prolong battery life, the LEDs are driven only when needed. One-third of the ADG733 SPDT analog switch is used to disconnect or connect the 1.25 V voltage reference from or to each current circuit. When driving the LEDs, the ADR1581 1.25 V voltage reference is buffered by half of the AD8506; the presence of this voltage on the noninverting input forces the output of the op amp (due to the negative feedback) to maintain a level that causes its inverting input to track the noninverting pin. Therefore, the 1.25 V appears in parallel with the 20 Ω R1 or 12.4 Ω R5 current source resistor, creating the flow of 62.5 mA or 101 mA current through the red or infrared LED as the output of the op amp turns on the Q1 or Q2 N-MOSFET IRLMS2002.

The maximum total quiescent currents for the AD8506 (that is, half of the AD8506), ADR1581, and ADG733 are 25 µA, 70 µA, and 1 µA, respectively, resulting in a total of 96 µA current consumption (480 µW power consumption) per circuit, which is good for a system powered by a battery. If the accuracy and temperature drift of the total design need to be improved, then a more accurate and low temperature coefficient drift voltage reference and current source resistor must be utilized. C3 and C4 are used to improve stabilization of U1; R3 and R7 are used to provide some current limit into the U1 inverting pin; and R2 and R6 are used to slow down the rise time of the N-MOSFET when it turns on. These elements may not be needed, or some bench adjustments may be required.
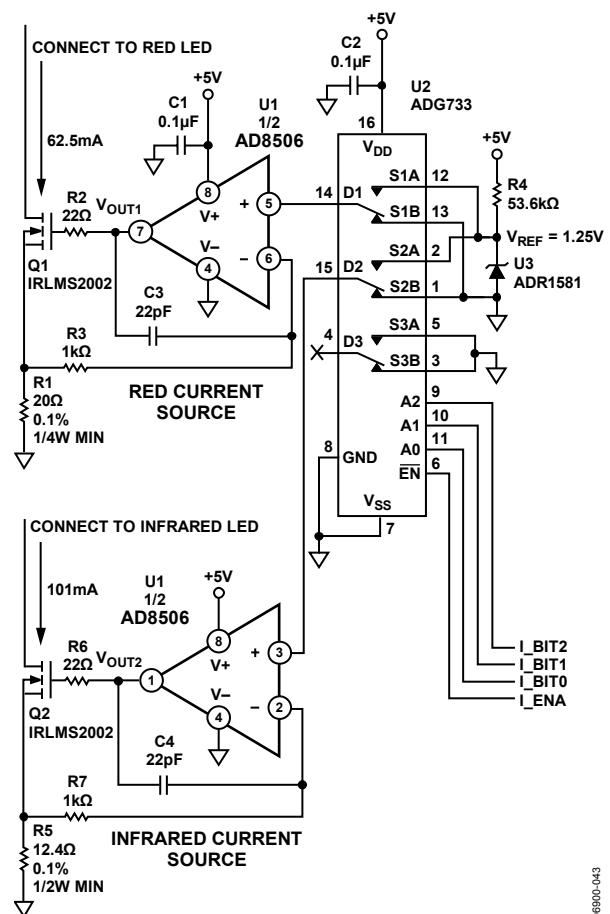

Figure 49. Pulse Oximeter Red and Infrared Current Sources Using the AD8506 as a Buffer to the Voltage Reference Device

FOUR-POLE, LOW-PASS BUTTERWORTH FILTER FOR GLUCOSE MONITOR

There are several methods of glucose monitoring: spectroscopic absorption of infrared light in the 2 μm to 2.5 μm range, reflectance spectrophotometry, and the amperometric type using electrochemical strips with glucose oxidase enzymes. The amperometric type generally uses three electrodes: a reference electrode, a control electrode, and a working electrode. Although this is a well established and widely used technique, signal-to-noise ratio and repeatability can be improved using the AD8505/AD8506/AD8508 amplifiers with their low peak-to-peak voltage noise of 2.8 μV from 0.1 Hz to 10 Hz and voltage noise density of 45 nV/√Hz at 1 kHz.

Another consideration is operation from a 3.3 V battery. Glucose signal currents are usually less than 3 μA full scale; therefore, the I-to-V converter requires low input bias current. The AD8505/AD8506/AD8508 are excellent choices because these amplifiers provide 1 pA typical and 10 pA maximum of input bias current at ambient temperature.

A low-pass filter with a cutoff frequency of 80 Hz to 100 Hz is desirable in a glucose meter device to remove extraneous noise; this can be a simple two-pole or four-pole Butterworth filter. Low power op amps with bandwidths of 50 kHz to 500 kHz are adequate. The AD8505/AD8506/AD8508 amplifiers with their 95 kHz GBP and 15 μA typical current consumption meet these requirements. A circuit design of a four-pole Butterworth filter (preceded by a one-pole, low-pass filter) is shown in Figure 50. With a 3.3 V battery, the total power consumption of this design is 297 μW typical at ambient temperature.
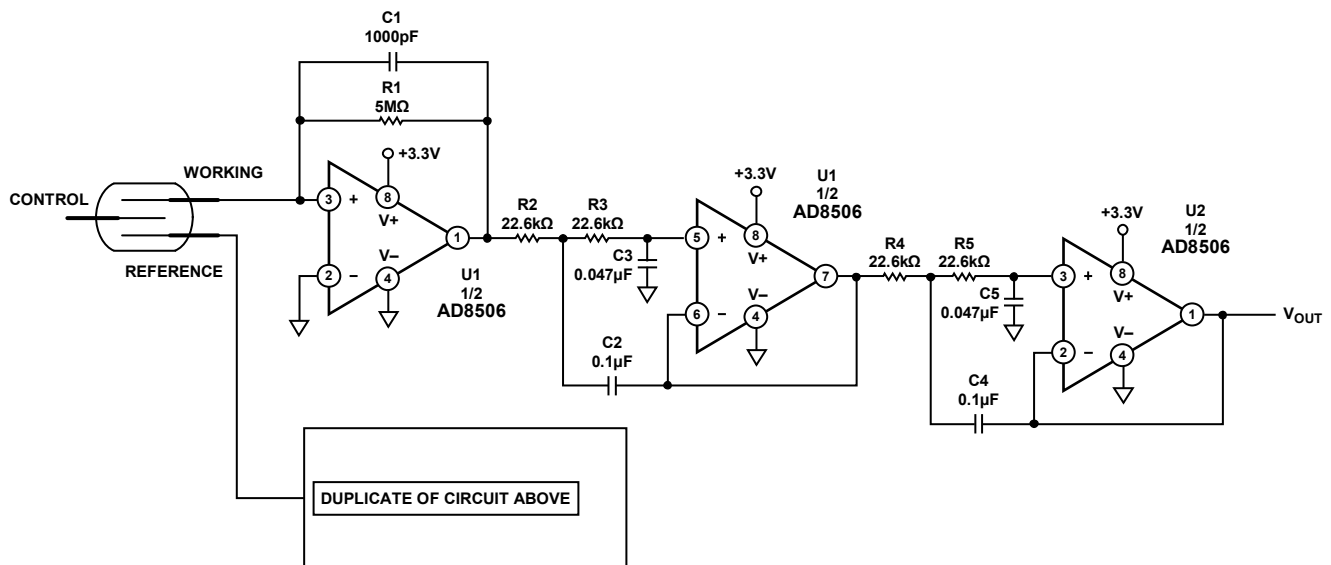
Figure 50. A Four-Pole Butterworth Filter That Can Be Used in a Glucose Meter

OUTLINE DIMENSIONS

3.00
2.90
2.80

1.70
1.60
1.50

3.00
2.80
2.60

5　　4

1　2　3

0.95 BSC

1.90 BSC

1.30
1.15
0.90

1.45 MAX
0.95 MIN

0.20 MAX
0.08 MIN

0.15 MAX
0.05 MIN

0.50 MAX
0.35 MIN

SEATING PLANE

10°
5°
0°

0.60 BSC

0.55
0.45
0.35

11-01-2010-A
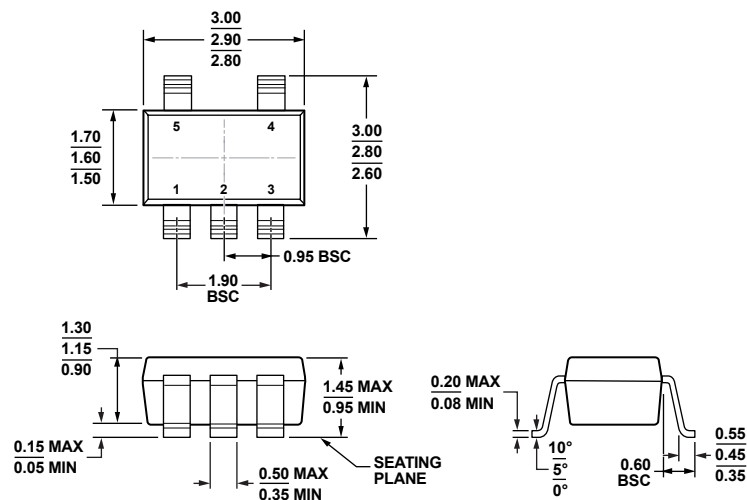
COMPLIANT TO JEDEC STANDARDS MO-178-AA

Figure 51. 5-Lead Small Outline Transistor Package [SOT-23]
(RJ-5)
Dimensions shown in millimeters

0.945
0.905
0.865

BALL A1 IDENTIFIER

1.425
1.385
1.345

TOP VIEW
(BALL SIDE DOWN)

2　　1

A

B

C

0.80 REF

0.40 BSC

0.40 BSC

BOTTOM VIEW
(BALL SIDE UP)

0.645
0.600
0.555

SIDE VIEW

0.415
0.400
0.385

COPLANARITY 0.05

SEATING PLANE

0.287
0.267
0.247

0.230
0.200
0.170

08-09-2012-A
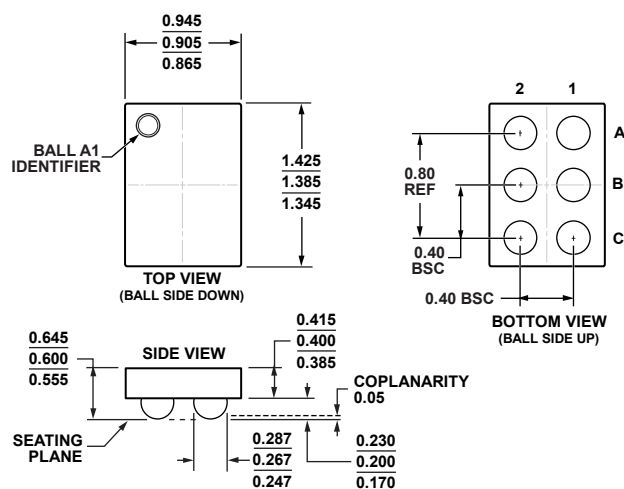
Figure 52. 6-Ball Wafer Level Chip Scale Package [WLCSP]
(CB-6-7)
Dimensions shown in millimeters

3.20
3.00
2.80

8   5

3.20
3.00
2.80

5.15
4.90
4.65

1   4

PIN 1
IDENTIFIER

0.65 BSC

0.95
0.85
0.75

1.10 MAX

15° MAX

0.15
0.05
COPLANARITY
0.10

0.40
0.25

6°
0°

0.23
0.09

0.80
0.55
0.40
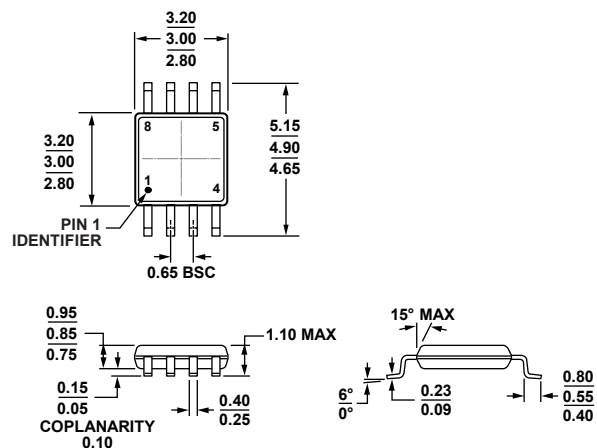
10-07-2009-B

COMPLIANT TO JEDEC STANDARDS MO-187-AA

Figure 53. 8-Lead Mini Small Outline Package [MSOP]
(RM-8)
Dimensions shown in millimeters

1.460
1.420 SQ
1.380

BALL A1
IDENTIFIER

3   2   1

A

B

C

TOP VIEW
(BALL SIDE DOWN)

0.50
BSC

BOTTOM VIEW
(BALL SIDE UP)

0.650
0.595
0.540

END VIEW

0.380
0.355
0.330

COPLANARITY
0.075

SEATING
PLANE
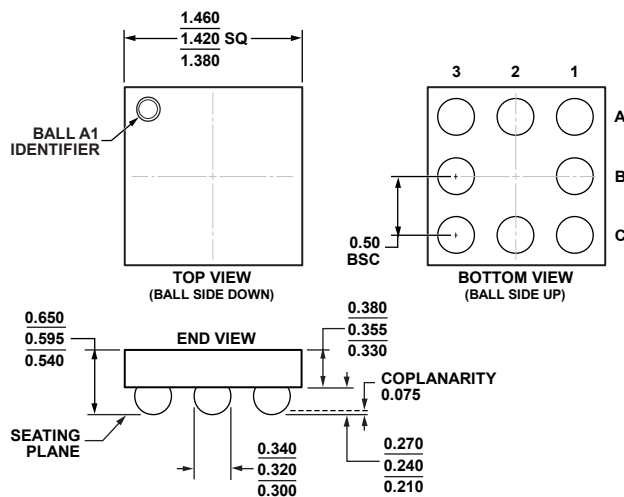
0.340
0.320
0.300

0.270
0.240
0.210

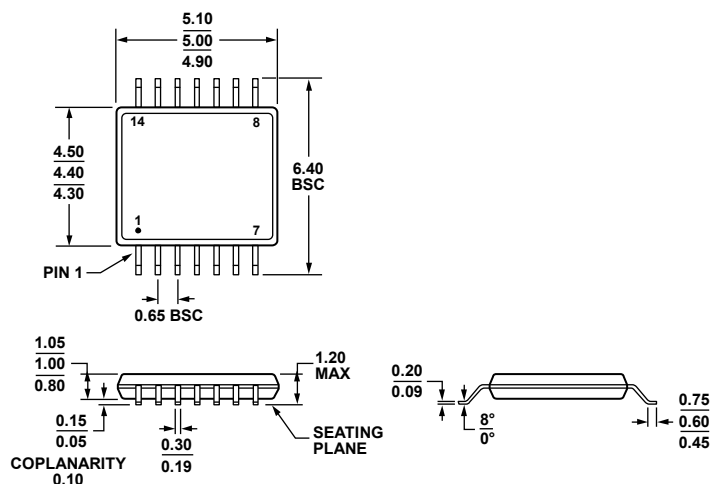08-30-2012-A

Figure 54. 8-Ball Wafer Level Chip Scale Package [WLCSP]
(CB-8-2)
Dimensions shown in millimeters

AD8505/AD8506/AD8508

COMPLIANT TO JEDEC STANDARDS MO-153-AB-1

Figure 55. 14-Lead Thin Shrink Small Outline Package [TSSOP]
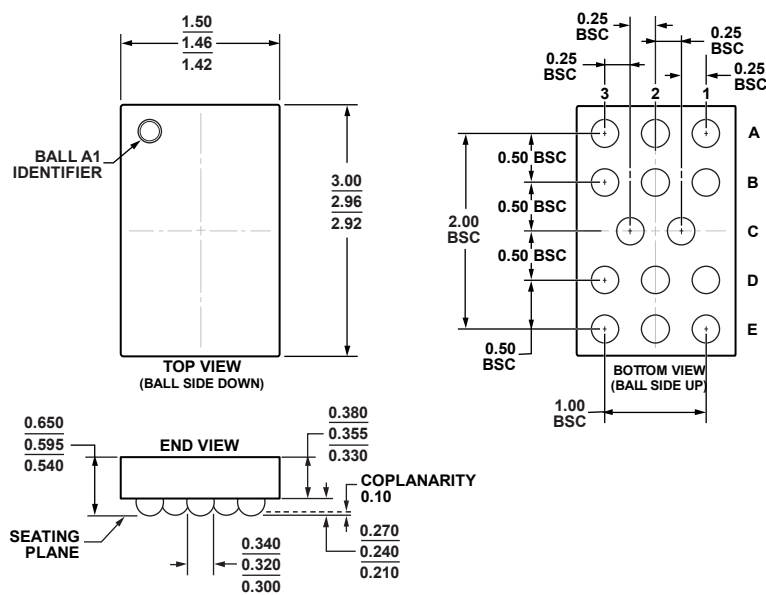*(RU-14)*
Dimensions shown in millimeters

Figure 56. 14-Ball Wafer Level Chip Scale Package [WLCSP]
(CB-14-1)
Dimensions shown in millimeters

ORDERING GUIDE

Model[1]	Temperature Range	Package Description	Package Option	Branding
AD8505ARJZ-R2	−40°C to +125°C	5-Lead Small Outline Transistor Package [SOT-23]	RJ-5	A2E
AD8505ARJZ-R7	−40°C to +125°C	5-Lead Small Outline Transistor Package [SOT-23]	RJ-5	A2E
AD8505ACBZ-R7	−40°C to +125°C	6-Ball Wafer Level Chip Scale Package [WLCSP]	CB-6-7	A2H
AD8505ACBZ-RL	−40°C to +125°C	6-Ball Wafer Level Chip Scale Package [WLCSP]	CB-6-7	A2H
AD8506ACBZ-REEL7	−40°C to +125°C	8-Ball Wafer Level Chip Scale Package [WLCSP]	CB-8-2	A1X
AD8506ARMZ	−40°C to +125°C	8-Lead Mini Small Outline Package [MSOP]	RM-8	A1X
AD8506ARMZ-R7	−40°C to +125°C	8-Lead Mini Small Outline Package [MSOP]	RM-8	A1X
AD8506ARMZ-REEL	−40°C to +125°C	8-Lead Mini Small Outline Package [MSOP]	RM-8	A1X
AD8508ARUZ	−40°C to +125°C	14-Lead Thin Shrink Small Outline Package [TSSOP]	RU-14	
AD8508ARUZ-REEL	−40°C to +125°C	14-Lead Thin Shrink Small Outline Package [TSSOP]	RU-14	
AD8508ACBZ-REEL7	−40°C to +125°C	14-Ball Wafer Level Chip Scale Package [WLCSP]	CB-14-1	A27

[1] Z = RoHS Compliant Part.

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