

June 2003

FDD20AN06A0

N-Channel PowerTrench® MOSFET **60V**, **45A**, **20m** Ω

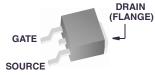
Features

- $r_{DS(ON)} = 17m\Omega$ (Typ.), $V_{GS} = 10V$, $I_D = 45A$
- $Q_q(tot) = 15nC (Typ.), V_{GS} = 10V$
- Low Miller Charge
- Low Q_{RR} Body Diode
- UIS Capability (Single Pulse and Repetitive Pulse)
- Qualified to AEC Q101

Formerly developmental type 82547

Applications

- Motor / Body Load Control
- ABS Systems
- Powertrain Management
- · Injection Systems
- DC-DC converters and Off-line UPS
- · Distributed Power Architectures and VRMs
- · Primary Switch for 12V and 24V systems



TO-252AA





FDD SERIES

MOSFET Maximum Ratings T_C = 25°C unless otherwise noted

Symbol	Parameter	Ratings	Units
V _{DSS}	Drain to Source Voltage	60	V
V _{GS}	Gate to Source Voltage	±20	V
	Drain Current		
	Continuous (T _C = 25°C, V _{GS} = 10V)	45	Α
I_D	Continuous (T _C = 100°C, V _{GS} = 10V)	32	А
	Continuous ($T_{amb} = 25^{\circ}C$, $V_{GS} = 10V$, $R_{\theta JA} = 52^{\circ}C/W$)	8	Α
	Pulsed	Figure 4	А
E _{AS}	Single Pulse Avalanche Energy (Note 1)	50	mJ
В	Power dissipation	90	W
P_{D}	Derate above 25°C	0.60	W/°C
T _J , T _{STG}	Operating and Storage Temperature	-55 to 175	°C

Thermal Characteristics

$R_{\theta JC}$	Thermal Resistance Junction to Case TO-252	1.67	°C/W
$R_{\theta JA}$	Thermal Resistance Junction to Ambient TO-252	100	°C/W
$R_{\theta JA}$	Thermal Resistance Junction to Ambient TO-252, 1in ² copper pad area	52	°C/W

This product has been designed to meet the extreme test conditions and environment demanded by the automotive industry. For a copy of the requirements, see AEC Q101 at: http://www.aecouncil.com/

Reliability data can be found at: http://www.fairchildsemi.com/products/discrete/reliability/index.html. All Fairchild Semiconductor products are manufactured, assembled and tested under ISO9000 and QS9000 quality systems certification.

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Package	Marking	and	Orderina	Information
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Device Marking	Device	Package	Reel Size	Tape Width	Quantity
FDD20AN06A0	FDD20AN06A0	TO-252AA	330mm	16mm	2500 units

Electrical Characteristics $T_C = 25^{\circ}C$ unless otherwise noted

Symbol	Parameter	Test Co	nditions	Min	Тур	Max	Units
Off Characteristics							
B _{VDSS}	Drain to Source Breakdown Voltage	$I_D = 250 \mu A, V_G$	S = 0V	60	-	-	V
1	Jame Cata Valta de Ducia Comunit			-	-	1	^
IDSS	Zero Gate Voltage Drain Current	$V_{GS} = 0V$	$T_{\rm C} = 150^{\rm o}{\rm C}$	-	-	250	μΑ
I _{GSS}	Gate to Source Leakage Current	$V_{GS} = \pm 20V$		-	-	±100	nA

On Characteristics

V _{GS(TH)}	Gate to Source Threshold Voltage	$V_{GS} = V_{DS}$, $I_D = 250\mu A$	2	-	4	V
		I _D = 45A, V _{GS} = 10V	-	0.017	0.020	
r _{DS(ON)}	Drain to Source On Resistance	$I_D = 45A, V_{GS} = 10V,$ $T_J = 175^{\circ}C$	-	0.039	0.047	Ω

Dynamic Characteristics

C _{ISS}	Input Capacitance	V 05V V 0V	-	950	-	pF
C _{OSS}	Output Capacitance	$V_{DS} = 25V, V_{GS} = 0V,$ f = 1MHz	-	185	-	pF
C _{RSS}	Reverse Transfer Capacitance	1 – 1101112	-	60	-	pF
$Q_{g(TOT)}$	Total Gate Charge at 10V	V _{GS} = 0V to 10V		15	19	nC
$Q_{g(TH)}$	Threshold Gate Charge	$V_{GS} = 0V \text{ to } 2V$ $V_{DD} = 30V$	-	2	2.6	nC
Q _{gs}	Gate to Source Gate Charge	I _D = 45A	-	6	-	nC
Q _{gs} Q _{gs2}	Gate Charge Threshold to Plateau	$I_g = 1.0 \text{mA}$	-	4	-	nC
Q_{gd}	Gate to Drain "Miller" Charge		-	4.5	-	nC

Switching Characteristics $(V_{GS} = 10V)$

t_{ON}	Turn-On Time		-	-	164	ns
t _{d(ON)}	Turn-On Delay Time		-	11	-	ns
t _r		$V_{DD} = 30V, I_D = 45A$	-	98	-	ns
t _{d(OFF)}	Turn-Off Delay Time	$V_{GS} = 10V, R_{GS} = 20\Omega$	-	23	-	ns
t _f	Fall Time		-	33	-	ns
t _{OFF}	Turn-Off Time		-	-	84	ns

Drain-Source Diode Characteristics

V _{SD}	Source to Drain Diode Voltage	I _{SD} = 45A	-	-	1.25	V
		I _{SD} = 22A	-	-	1.0	V
t _{rr}	Reverse Recovery Time	$I_{SD} = 45A$, $dI_{SD}/dt = 100A/\mu s$	-	-	32	ns
Q _{RR}	Reverse Recovered Charge	$I_{SD} = 45A$, $dI_{SD}/dt = 100A/\mu s$	-	-	25	nC

Notes: 1: Starting $T_J = 25^{\circ}C$, $L = 80\mu H$, $I_{AS} = 36A$.

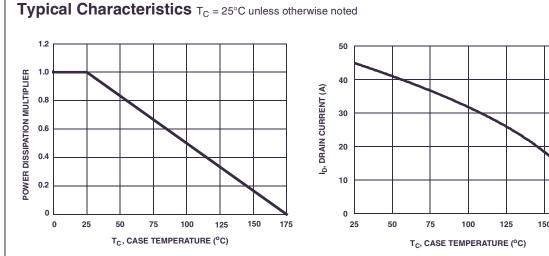


Figure 1. Normalized Power Dissipation vs
Ambient Temperature

Figure 2. Maximum Continuous Drain Current vs Case Temperature

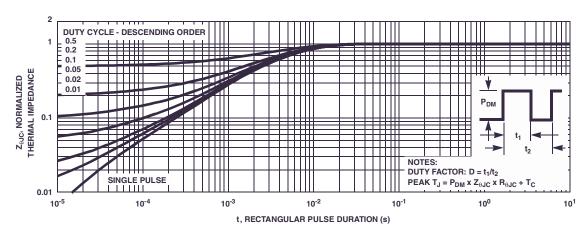


Figure 3. Normalized Maximum Transient Thermal Impedance

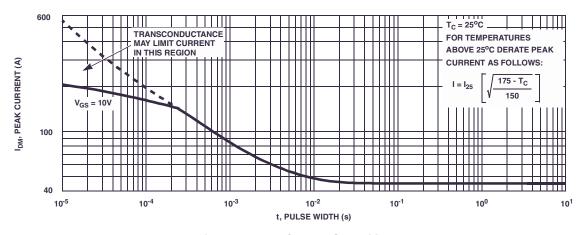
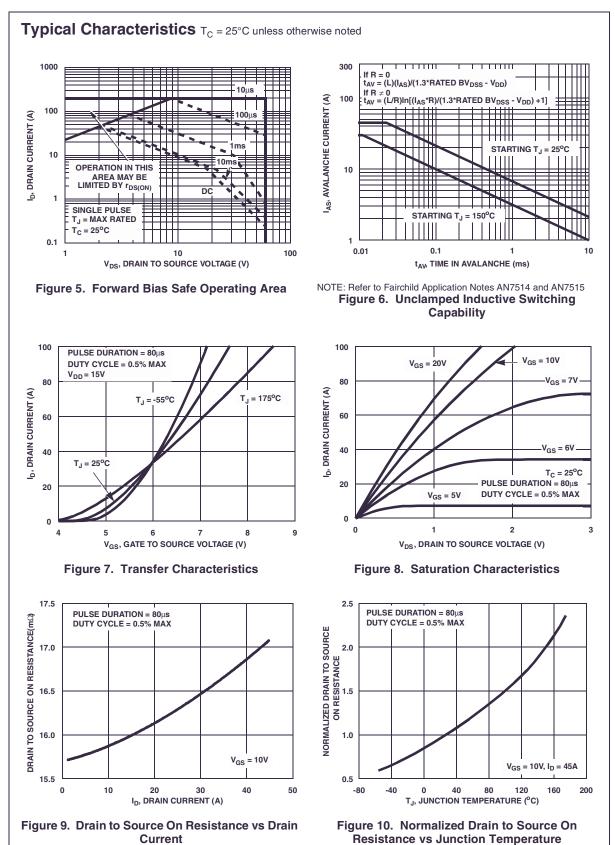


Figure 4. Peak Current Capability



Typical Characteristics $T_C = 25^{\circ}C$ unless otherwise noted

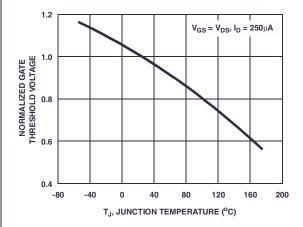


Figure 11. Normalized Gate Threshold Voltage vs
Junction Temperature

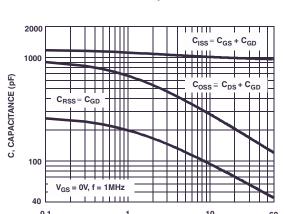


Figure 13. Capacitance vs Drain to Source Voltage

V_{DS}, DRAIN TO SOURCE VOLTAGE (V)

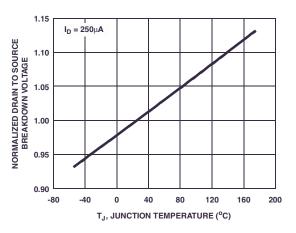


Figure 12. Normalized Drain to Source Breakdown Voltage vs Junction Temperature

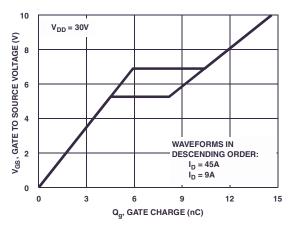


Figure 14. Gate Charge Waveforms for Constant Gate Current

Test Circuits and Waveforms

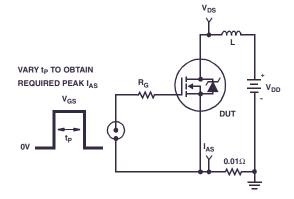


Figure 15. Unclamped Energy Test Circuit

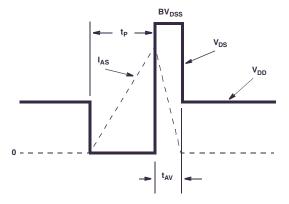


Figure 16. Unclamped Energy Waveforms

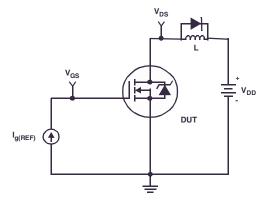


Figure 17. Gate Charge Test Circuit

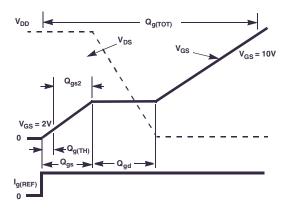


Figure 18. Gate Charge Waveforms

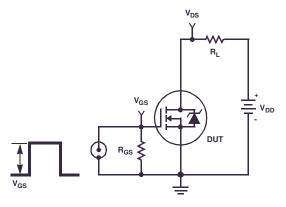


Figure 19. Switching Time Test Circuit

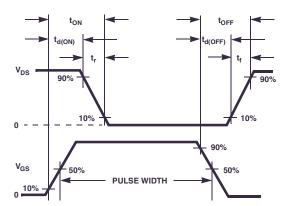


Figure 20. Switching Time Waveforms

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Thermal Resistance vs. Mounting Pad Area

The maximum rated junction temperature, T_{JM} , and the thermal resistance of the heat dissipating path determines the maximum allowable device power dissipation, P_{DM} , in an application. Therefore the application's ambient temperature, T_A (°C), and thermal resistance $R_{\theta JA}$ (°C/W) must be reviewed to ensure that T_{JM} is never exceeded. Equation 1 mathematically represents the relationship and serves as the basis for establishing the rating of the part.

$$P_{DM} = \frac{(T_{JM} - T_A)}{R_{\theta JA}} \tag{EQ. 1}$$

In using surface mount devices such as the TO-252 package, the environment in which it is applied will have a significant influence on the part's current and maximum power dissipation ratings. Precise determination of P_{DM} is complex and influenced by many factors:

- Mounting pad area onto which the device is attached and whether there is copper on one side or both sides of the board.
- 2. The number of copper layers and the thickness of the board.
- 3. The use of external heat sinks.
- 4. The use of thermal vias.
- 5. Air flow and board orientation.
- 6. For non steady state applications, the pulse width, the duty cycle and the transient thermal response of the part, the board and the environment they are in.

Fairchild provides thermal information to assist the designer's preliminary application evaluation. Figure 21 defines the $R_{\theta JA}$ for the device as a function of the top copper (component side) area. This is for a horizontally positioned FR-4 board with 1oz copper after 1000 seconds of steady state power with no air flow. This graph provides the necessary information for calculation of the steady state junction temperature or power dissipation. Pulse applications can be evaluated using the Fairchild device Spice thermal model or manually utilizing the normalized maximum transient thermal impedance curve.

Thermal resistances corresponding to other copper areas can be obtained from Figure 21 or by calculation using Equation 2 or 3. Equation 2 is used for copper area defined in inches square and equation 3 is for area in centimeters square. The area, in square inches or square centimeters is the top copper area including the gate and source pads.

$$R_{\theta JA} = 33.32 + \frac{23.84}{(0.268 + Area)}$$
 (EQ. 2)

Area in Inches Squared

$$R_{\theta JA} = 33.32 + \frac{154}{(1.73 + Area)}$$
 (EQ. 3)

Area in Centimeters Squared

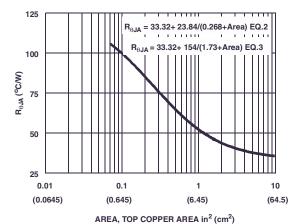
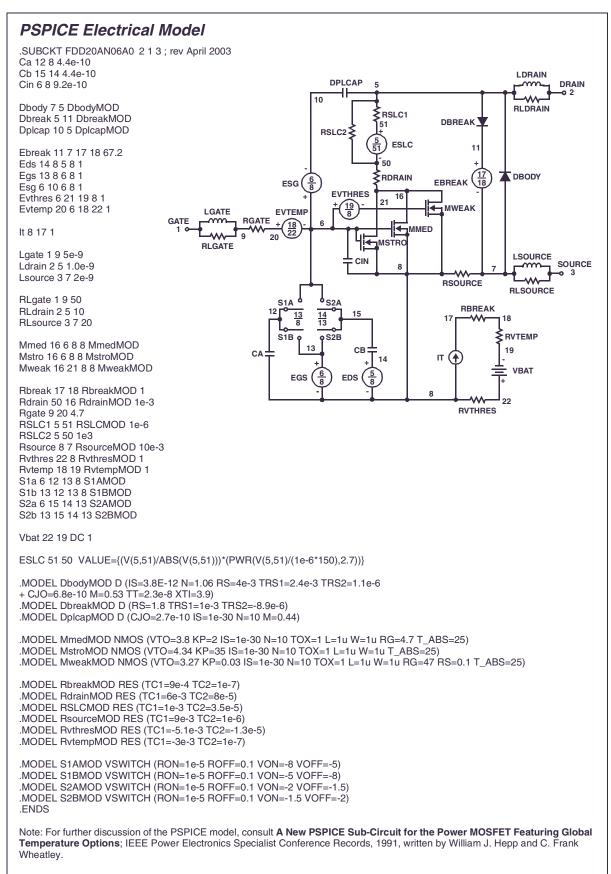
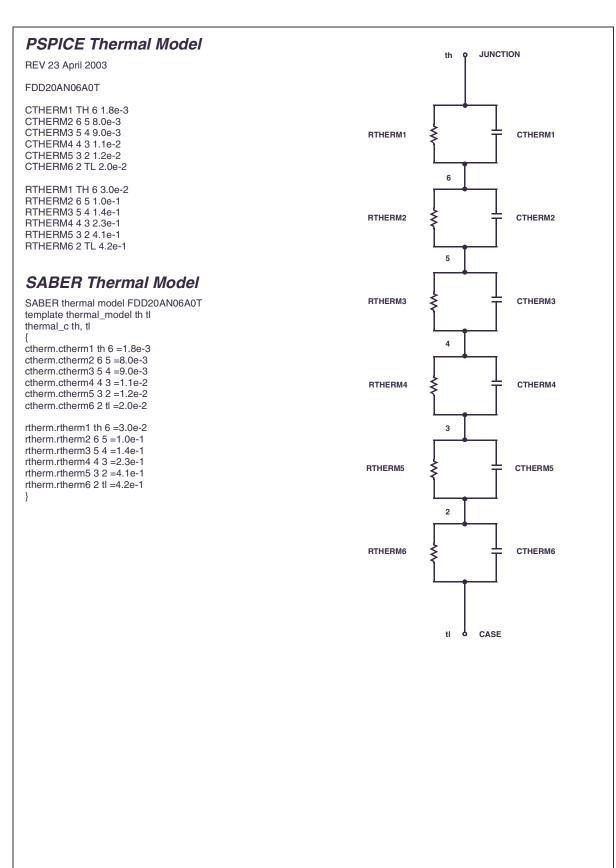


Figure 21. Thermal Resistance vs Mounting Pad Area



SABER Electrical Model rev April 2003 template FDD20AN06A0 n2,n1,n3 =m temp electrical n2,n1,n3 number m_temp=25 var i iscl dp.,model dbodymod = (isl=3.8e-12.nl=1.06.rs=4e-3.trs1=2.4e-3.trs2=1.1e-6.cio=6.8e-10.m=0.53.tt=2.3e-8.xti=3.9) dp..model dbreakmod = (rs=1.8,trs1=1e-3,trs2=-8.9e-6) dp..model dplcapmod = (cjo=2.7e-10,isl=10e-30,nl=10,m=0.44) m..model mmedmod = (type=_n,vto=3.8,kp=2,is=1e-30, tox=1) m..model mstrongmod = (type=_n,vto=4.34,kp=35,is=1e-30, tox=1) m..model mweakmod = $(type=_n, vto=3.27, kp=0.03, is=1e-30, tox=1, rs=0.1)$ **LDRAIN** sw_vcsp..model s1amod = (ron=1e-5,roff=0.1,von=-8,voff=-5) DPLCAP DRAIN sw_vcsp..model s1bmod = (ron=1e-5,roff=0.1,von=-5,voff=-8) 10 sw_vcsp..model s2amod = (ron=1e-5,roff=0.1,von=-2,voff=-1.5) BLDBAIN €RSLC1 sw_vcsp..model s2bmod = (ron=1e-5,roff=0.1,von=-1.5,voff=-2) c.ca n12 n8 = 4.4e-10RSLC2 ₹ c.cb n15 n14 = 4.4e-10 ISCL c.cin n6 n8 = 9.2e-10 DBREAK I dp.dbody n7 n5 = model=dbodymod **₹**RDRAIN 8 ESG(11 dp.dbreak n5 n11 = model=dbreakmod DBODY **EVTHRES** dp.dplcap n10 n5 = model=dplcapmod 16 (<u>19</u>) 8 MWEAK EVTEMP **LGATE** spe.ebreak n11 n7 n17 n18 = 67.2 GATE RGATE MMED EBREAK $\frac{1}{100}$ spe.eds n14 n8 n5 n8 = 1 20 MSTRO spe.egs n13 n8 n6 n8 = 1 **RLGATE** spe.esg n6 n10 n6 n8 = 1 LSOURCE CIN SOURCE spe.evthres n6 n21 n19 n8 = 1 spe.evtemp n20 n6 n18 n22 = 1 **RSOURCE** RLSOURCE i.it n8 n17 = 1**RBREAK** 14 13 17 I.lgate n1 n9 = 5e-9I.Idrain n2 n5 = 1.0e-9RVTEMP o S2B I.Isource n3 n7 = 2e-9СВ 19 CA IT 14 res.rlgate n1 n9 = 50VBAT EGS EDS res.rldrain n2 n5 = 10 res.rlsource n3 n7 = 20 **RVTHRES** m.mmed n16 n6 n8 n8 = model=mmedmod, l=1u, w=1u, temp=m_temp m.mstrong n16 n6 n8 n8 = model=mstrongmod, l=1u, w=1u ,temp=m_temp m.mweak n16 n21 n8 n8 = model=mweakmod, l=1u, w=1u ,temp=m_temp res.rbreak n17 n18 = 1, tc1=9e-4,tc2=1e-7 res.rdrain n50 n16 = 1e-3, tc1=6e-3,tc2=8e-5 res.rgate n9 n20 = 4.7res.rslc1 n5 n51 = 1e-6, tc1=1e-3,tc2=3.5e-5 res.rslc2 n5 n50 = 1e3res.rsource n8 n7 = 10e-3, tc1=9e-3,tc2=1e-6 res.rvthres n22 n8 = 1, tc1=-5.1e-3, tc2=-1.3e-5res.rvtemp n18 n19 = 1. tc1=-3e-3.tc2=1e-7sw_vcsp.s1a n6 n12 n13 n8 = model=s1amod sw_vcsp.s1b n13 n12 n13 n8 = model=s1bmod sw_vcsp.s2a n6 n15 n14 n13 = model=s2amod sw_vcsp.s2b n13 n15 n14 n13 = model=s2bmod v.vbat n22 n19 = dc=1 equations { i (n51->n50) +=iscl iscl: v(n51,n50) = ((v(n5,n51)/(1e-9+abs(v(n5,n51))))*((abs(v(n5,n51)*1e6/150))** 2.7))

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