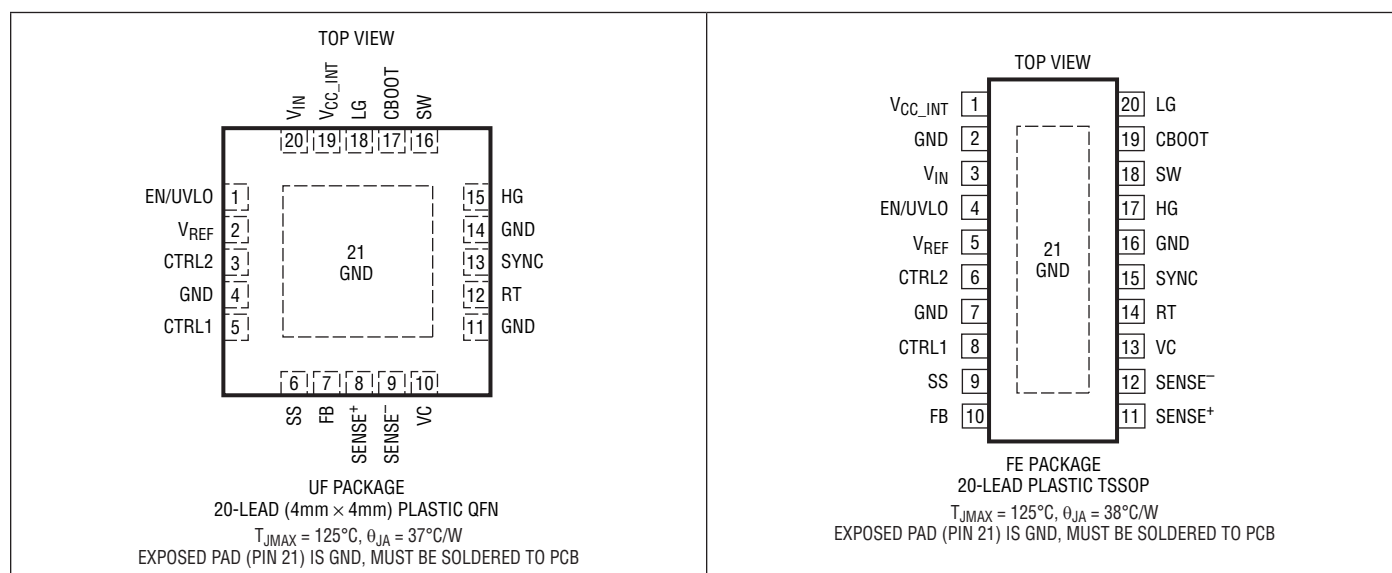


# LT3741/LT3741-1

## ABSOLUTE MAXIMUM RATINGS (Note 1)

$V_{IN}$ Voltage.....	40V	RT Voltage .....	3V
EN/UVLO Voltage.....	6V	FB Voltage.....	3V
$V_{REF}$ Voltage .....	3V	SS Voltage .....	6V
CTRL1 and CTRL2 Voltage.....	3V	$V_{CC\_INT}$ Voltage.....	6V
SENSE <sup>+</sup> Voltage .....	40V	SYNC Voltage.....	6V
SENSE <sup>-</sup> Voltage .....	40V	Storage Temperature Range .....	-65°C to 150°C
VC Voltage .....	3V	Lead Temperature (Soldering, 10 sec)	
SW Voltage .....	40V	TSSOP .....	300°C
CBOOT .....	46V		

## PIN CONFIGURATION



## ORDER INFORMATION <http://www.linear.com/product/LT3741#orderinfo>

LEAD FREE FINISH	TAPE AND REEL	PART MARKING*	PACKAGE DESCRIPTION	TEMPERATURE RANGE
LT3741EUF#PBF	LT3741EUF#TRPBF	3741	20-Lead (4mm × 4mm) Plastic QFN	-40°C to 125°C
LT3741IUF#PBF	LT3741IUF#TRPBF	3741	20-Lead (4mm × 4mm) Plastic QFN	-40°C to 125°C
LT3741EFE#PBF	LT3741EFE#TRPBF	LT3741FE	20-Lead Plastic TSSOP	-40°C to 125°C
LT3741IFE#PBF	LT3741IFE#TRPBF	LT3741FE	20-Lead Plastic TSSOP	-40°C to 125°C
LT3741EUF-1#PBF	LT3741EUF-1#TRPBF	37411	20-Lead (4mm × 4mm) Plastic QFN	-40°C to 125°C
LT3741IUF-1#PBF	LT3741IUF-1#TRPBF	37411	20-Lead (4mm × 4mm) Plastic QFN	-40°C to 125°C
LT3741EFE-1#PBF	LT3741EFE-1#TRPBF	LT3741FE-1	20-Lead Plastic TSSOP	-40°C to 125°C
LT3741IFE-1#PBF	LT3741IFE-1#TRPBF	LT3741FE-1	20-Lead Plastic TSSOP	-40°C to 125°C

Consult ADI Marketing for parts specified with wider operating temperature ranges. \*The temperature grade is identified by a label on the shipping container. For more information on lead free part marking, go to: <http://www.linear.com/leadfree/> For more information on tape and reel specifications, go to: <http://www.linear.com/tapeand reel/>. Some packages are available in 500 unit reels through designated sales channels with #TRMPBF suffix.

# ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at  $T_A = 25^\circ\text{C}$ .  $V_{IN} = 12\text{V}$ ,  $V_{EN/UVLO} = 5\text{V}$ ,  $V_{SYNC} = 0\text{V}$  unless otherwise noted.

PARAMETER	CONDITIONS		MIN	TYP	MAX	UNITS
Input Voltage Range		●	6		36	V
$V_{IN}$ Pin Quiescent Current (Note 2) Non-Switching Operation Shutdown Mode	Not Switching $V_{EN/UVLO} = 0\text{V}$ , $R_T = 40\text{k}\Omega$	●		1.8 0.1	2.5 1	mA $\mu\text{A}$
EN/UVLO Pin Falling Threshold			1.49	1.55	1.61	V
EN/UVLO Hysteresis				130		mV
EN/UVLO Pin Current	$V_{IN} = 6\text{V}$ , $V_{EN/UVLO} = 1.45\text{V}$			5.5		$\mu\text{A}$
SYNC Pin Threshold				1		V
CTRL1 Pin Control Range			0		1.5	V
CTRL1 Pin Current	CTRL1 = 1.5V			-100		nA
<b>Reference</b>						
Reference Voltage ( $V_{REF}$ Pin)		●	1.94	2	2.06	V
<b>Inductor Current Sensing</b>						
Full Range SENSE <sup>+</sup> to SENSE <sup>-</sup>	$V_{CTRL1} = 1.5\text{V}$	●	48	51	54	mV
SENSE <sup>+</sup> Pin Current	$V_{SENSE^+} = 6\text{V}$			50		nA
SENSE <sup>-</sup> Pin Current	With $V_{OUT} \sim 4\text{V}$ , $V_{CTRL1} = 0\text{V}$ , $V_{SENSE^-} = 6\text{V}$			10		$\mu\text{A}$
<b>Internal <math>V_{CC}</math> Regulator (<math>V_{CC\_INT}</math> Pin)</b>						
Regulation Voltage		●	4.7	5	5.2	V
<b>NMOS FET Driver</b>						
Non-Overlap time HG to LG	(Note 3)			100		ns
Non-Overlap time LG to HG	(Note 3)			60		ns
Minimum On-Time LG	(Note 3)			50		ns
Minimum On-Time HG	(Note 3)			80		ns
Minimum Off-Time LG	(Note 3)			65		ns
High Side Driver Switch On-Resistance Gate Pull Up Gate Pull Down	$V_{CBOOT} - V_{SW} = 5\text{V}$			2.3 1.3		$\Omega$ $\Omega$
Low Side Driver Switch On-Resistance Gate Pull Up Gate Pull Down	$V_{CC\_INT} = 5\text{V}$			2.3 1		$\Omega$ $\Omega$
<b>Switching Frequency</b>						
$f_{SW}$	$R_T = 40\text{k}\Omega$ $R_T = 200\text{k}\Omega$	●	900 185	1000 200	1070 233	kHz kHz
<b>Soft-Start</b>						
Charging Current				11		$\mu\text{A}$
<b>Voltage Regulation Amplifier</b>						
Input Bias Current	FB = 1.3V			850		nA
$g_m$				800		$\mu\text{A/V}$
Feedback Regulation Voltage	CTRL1 = 1.5V, $I_{SENSE^-} = 23\mu\text{A}$ , $V_{SENSE^+} = 2\text{V}$	●	1.192	1.21	1.228	V

# LT3741/LT3741-1

## ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at  $T_A = 25^\circ\text{C}$ .  $V_{IN} = 12\text{V}$ ,  $V_{EN/UVLO} = 5\text{V}$ ,  $V_{SYNC} = 0\text{V}$  unless otherwise noted.

PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
<b>Current Control Loop <math>g_m</math> Amp</b>					
Offset Voltage	$V_{CM} = 4\text{V}$ ●	-3	0	3	mV
Input Common Mode Range	$V_{CM(HIGH)}$ Measured from $V_{IN}$ to $V_{CM}$				V
$V_{CM(LOW)}$		0			V
$V_{CM(HIGH)}$		2			V
Output Impedance		3.5			$\text{M}\Omega$
$g_m$		375	475	625	$\mu\text{A/V}$
Differential Gain		1.7			V/mV

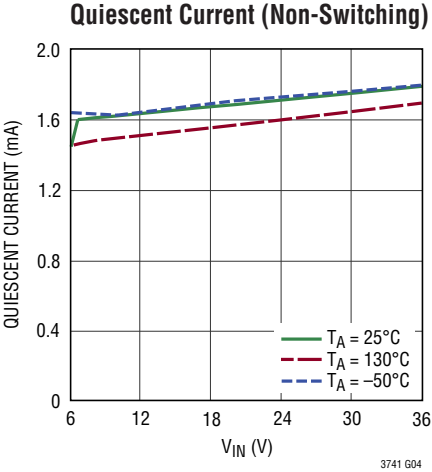
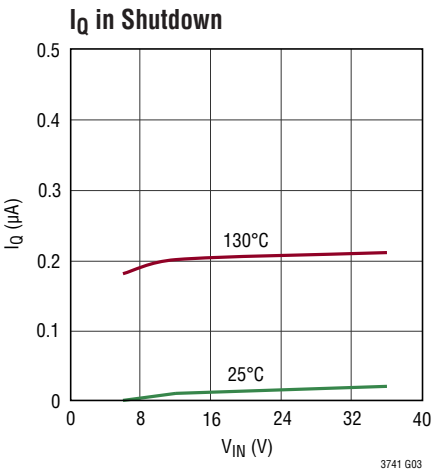
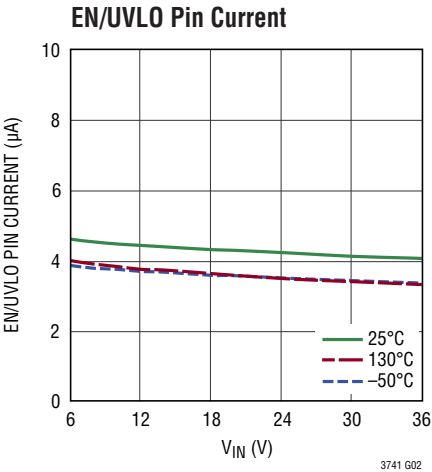
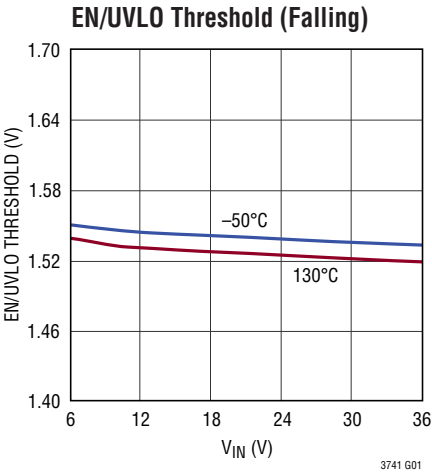
**Note 1:** Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

**Note 2:** The LT3741E is guaranteed to meet performance specifications from  $0^\circ\text{C}$  to  $125^\circ\text{C}$  junction temperature. Specifications over the  $-40^\circ\text{C}$

to  $125^\circ\text{C}$  operating junction temperature range are assured by design, characterization and correlation with statistical process controls. The LT3741I is guaranteed to meet performance specifications over the  $-40^\circ\text{C}$  to  $125^\circ\text{C}$  operating junction temperature range.

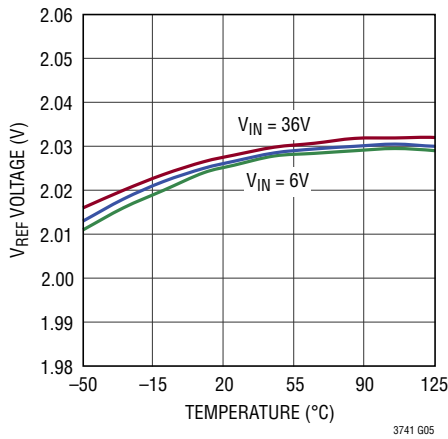
**Note 3:** The minimum on, off, and nonoverlap times are guaranteed by design and are not tested.

## TYPICAL PERFORMANCE CHARACTERISTICS

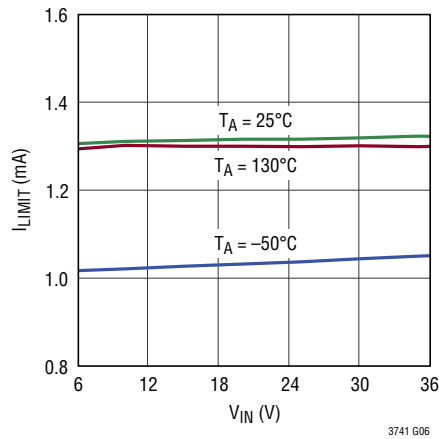


# TYPICAL PERFORMANCE CHARACTERISTICS

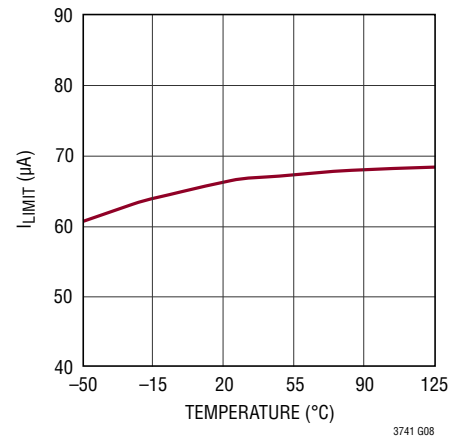
**V<sub>REF</sub> Pin Voltage**



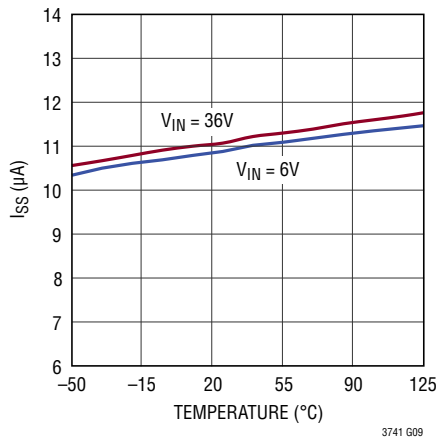
**V<sub>REF</sub> Current Limit**



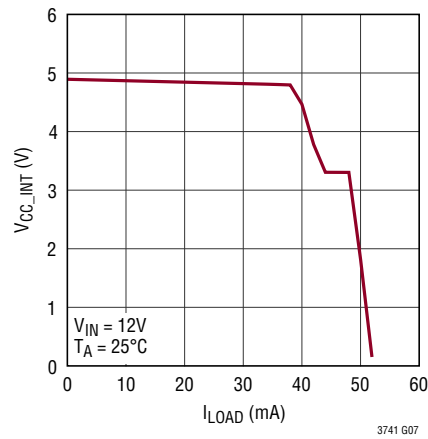
**RT Pin Current Limit**



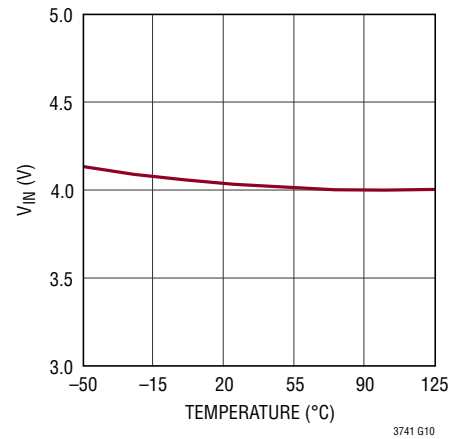
**Soft-Start Pin Current**



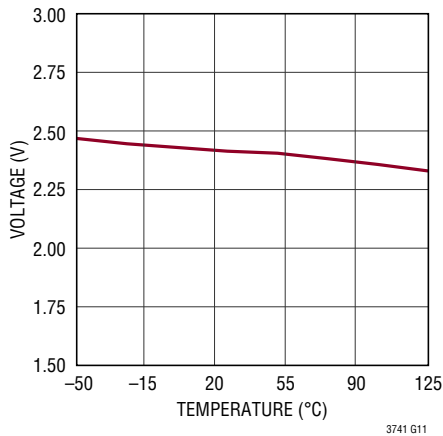
**V<sub>CC\_INT</sub> Current Limit**



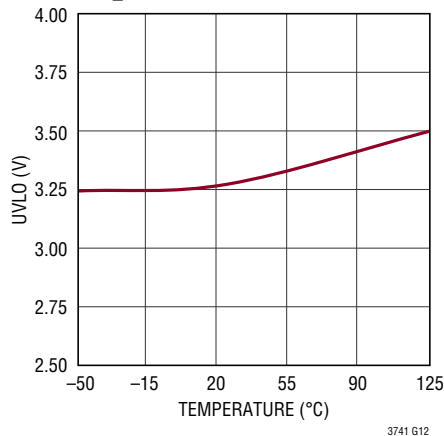
**Internal UVLO**



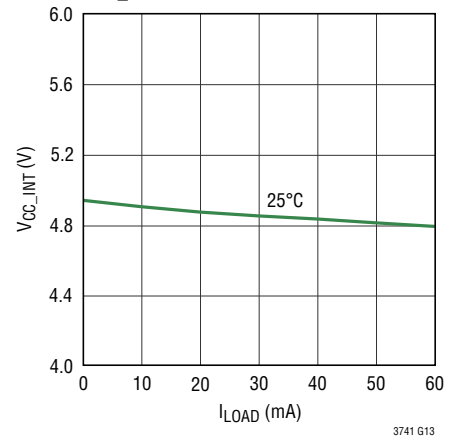
**CBOOT-SW UVLO Voltage**



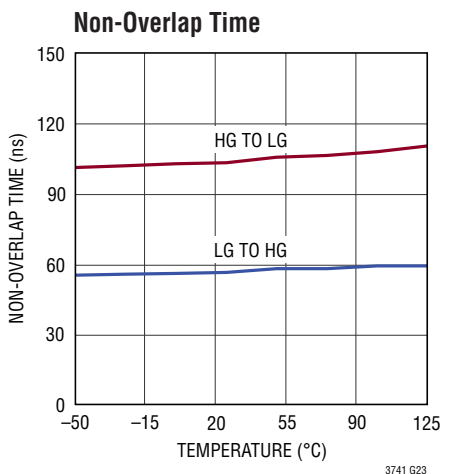
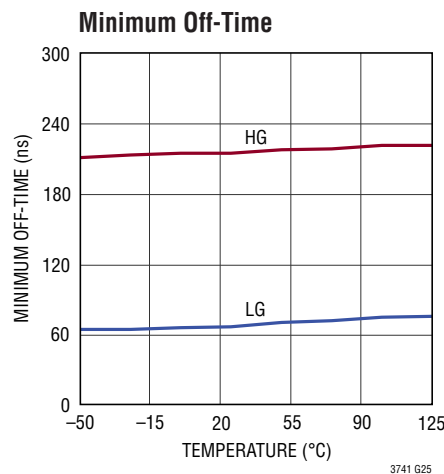
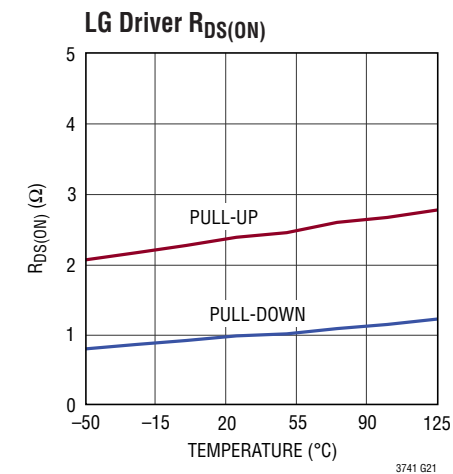
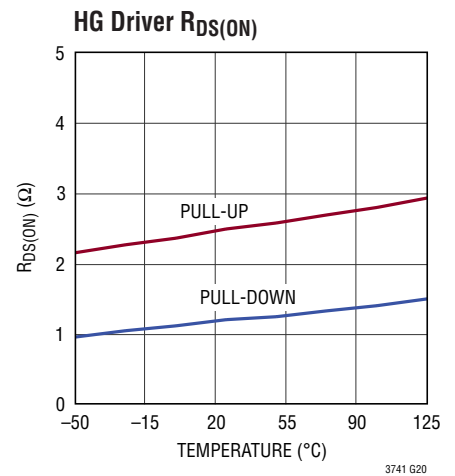
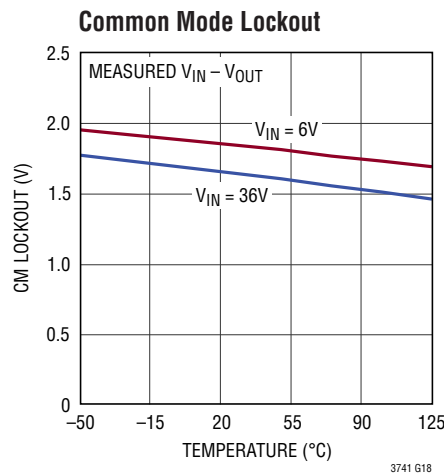
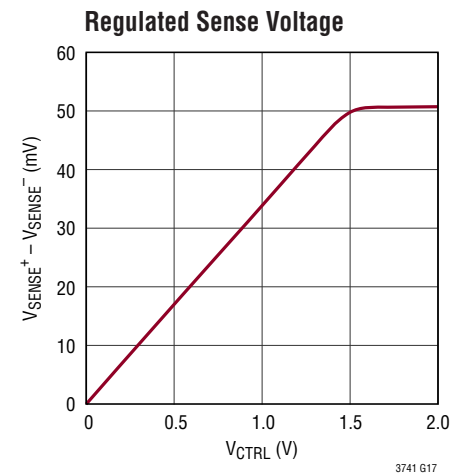
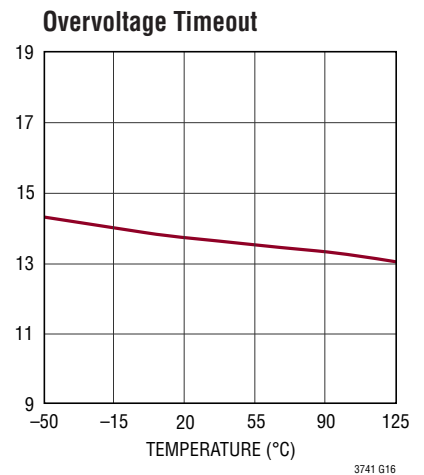
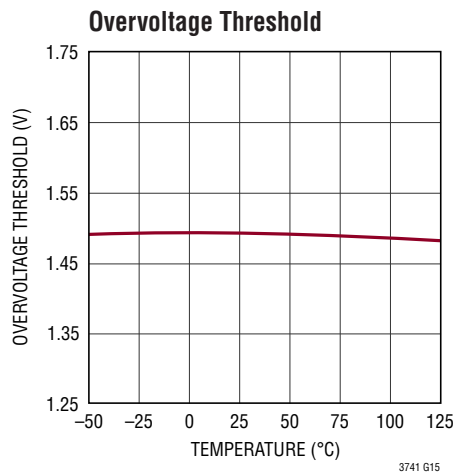
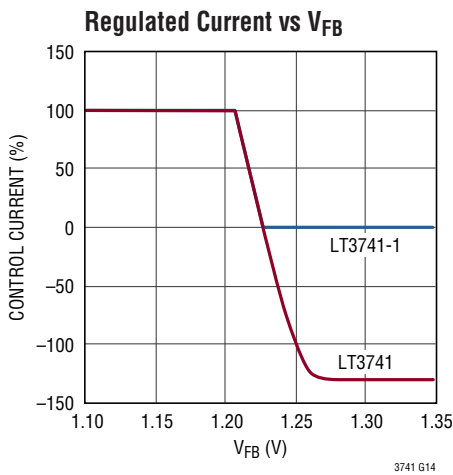
**V<sub>CC\_INT</sub> UVLO**



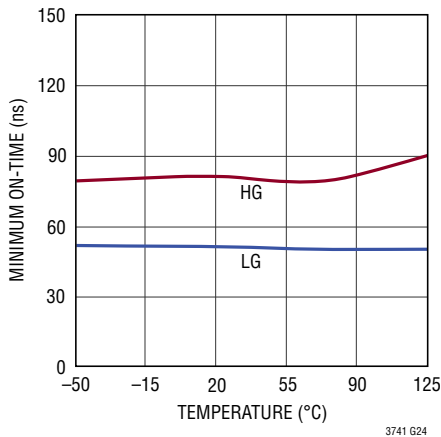
**V<sub>CC\_INT</sub> Load Reg at 12V**



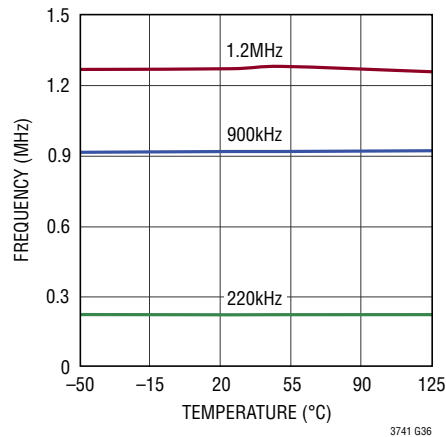
## TYPICAL PERFORMANCE CHARACTERISTICS



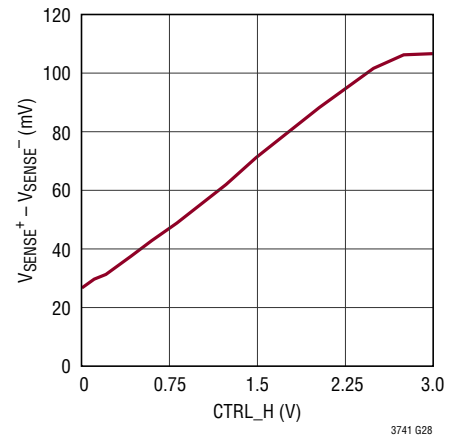
# TYPICAL PERFORMANCE CHARACTERISTICS

**Minimum On-Time**


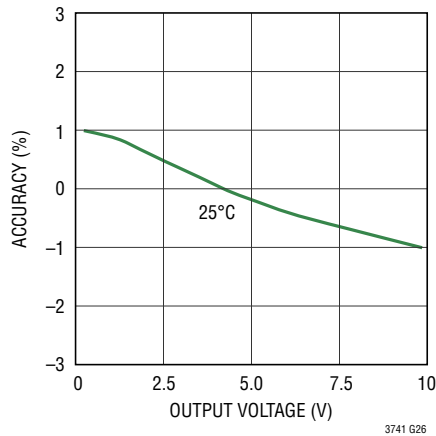
3741 G24

**Oscillator Frequency**


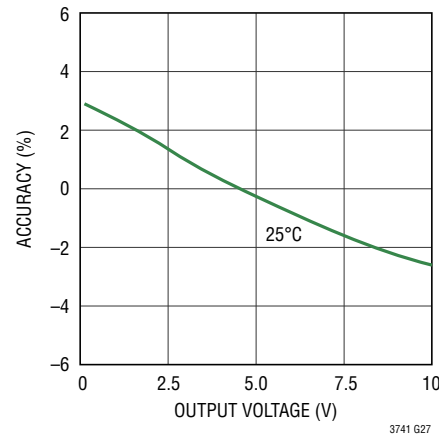
3741 G36

**Overcurrent Threshold**


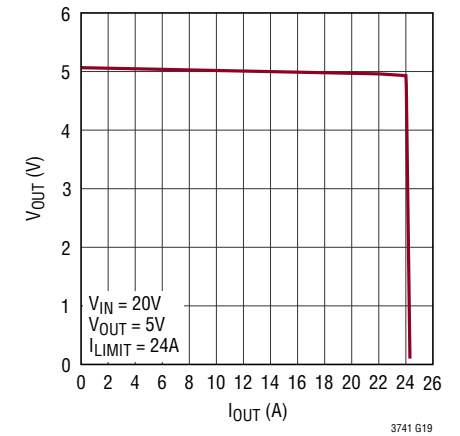
3741 G28

**Current Regulation Accuracy**  
CTRL1 = 1.5V,  $V_{IN} = 12V$ 


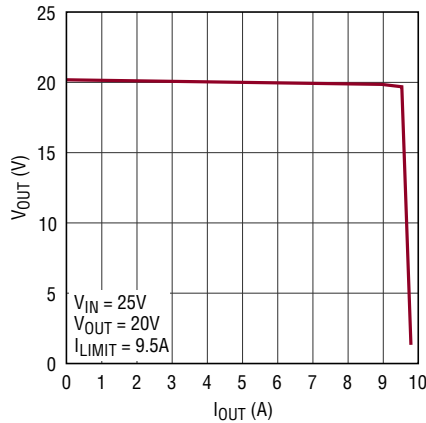
3741 G26

**Current Regulation Accuracy**  
CTRL1 = 0.75V,  $V_{IN} = 12V$ 


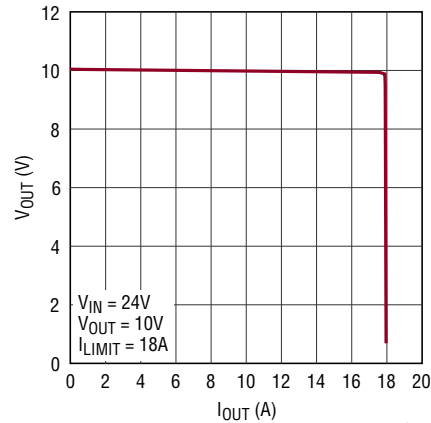
3741 G27

 **$V_{OUT}$  vs  $I_{OUT}$** 


3741 G19

 **$V_{OUT}$  vs  $I_{OUT}$** 


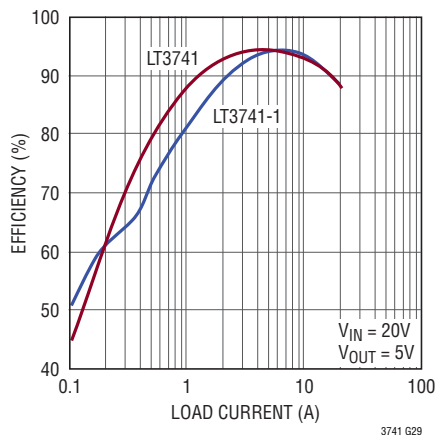
3741 G22

 **$V_{OUT}$  vs  $I_{OUT}$** 


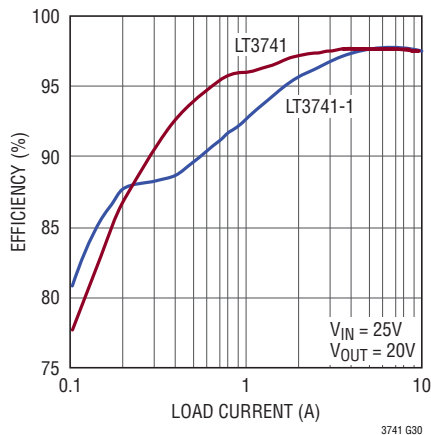
3741 G33

## TYPICAL PERFORMANCE CHARACTERISTICS

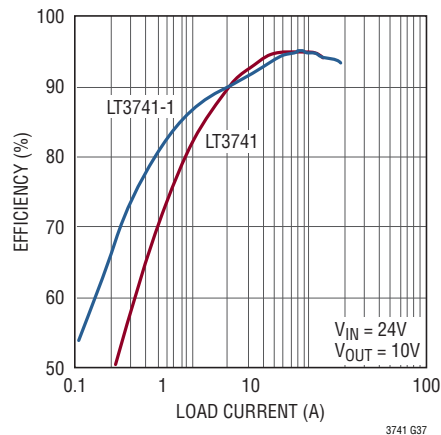
Efficiency and Power Loss  
vs Load Current



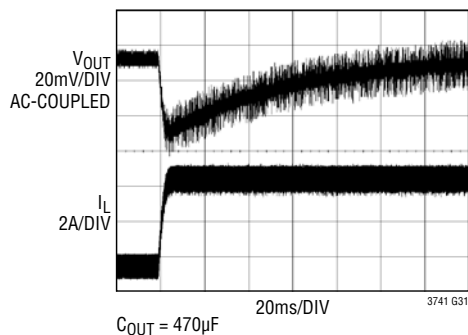
Efficiency and Power Loss  
vs Load Current



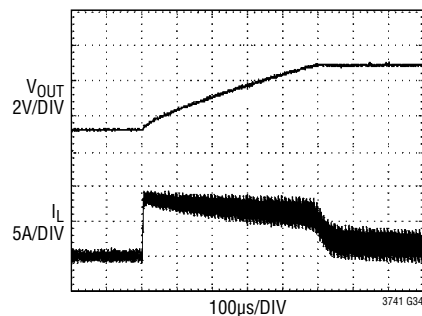
Efficiency and Power Loss  
vs Load Current



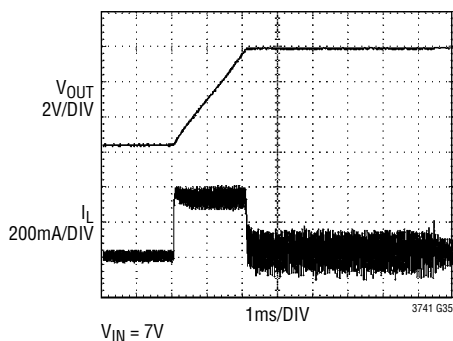
5A Load Step Recovery



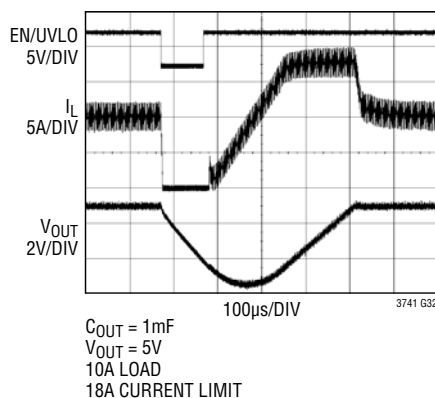
Voltage Regulation with 10A  
Regulated Inductor Current



Common Mode Lockout — LT3741



Shutdown and Recovery  
1.5nF Soft-Start Capacitor



## PIN FUNCTIONS (QFN/TSSOP)

**EN/UVLO (Pin 1/Pin 4):** Enable Pin. The EN/UVLO pin acts as an enable pin and turns on the internal current bias core and subregulators at 1.55V. The pin does not have any pull-up or pull-down, requiring a voltage bias for normal part operation. Full shutdown occurs at approximately 0.5V.

**V<sub>REF</sub> (Pin 2/Pin 5):** Buffered 2V reference capable of 0.5mA drive.

**CTRL2 (Pin 3/Pin 6):** Thermal control input used to reduce the regulated current level.

**GND (Pins 4, 11, 14, Exposed Pad Pin 21/Pins 2, 7, 16, Exposed Pad Pin 21):** Ground. The exposed pad must be soldered to the PCB.

**CTRL1 (Pin 5/Pin 8):** The CTRL1 pin sets the high level regulated output current and overcurrent. The maximum input voltage is internally clamped to 1.5V. The overcurrent set point is equal to the high level regulated current level set by the CTRL1 pin with an additional 23mV offset between the SENSE<sup>+</sup> and SENSE<sup>-</sup> pins.

**SS (Pin 6/Pin 9):** The Soft-Start Pin. Place an external capacitor to ground to limit the regulated current during start-up conditions. The soft-start pin has a 11μA charging current. This pin controls regulated output current determined by CTRL1.

**FB (Pin 7/Pin 10):** Feedback Pin for Voltage Regulation and Overvoltage Protection. The feedback voltage is 1.21V. Overvoltage is also sensed through the FB pin. When the feedback voltage exceeds 1.5V, the overvoltage lockout prevents switching for 13μs to allow the inductor current to discharge.

**SENSE<sup>+</sup> (Pin 8/Pin 11):** SENSE<sup>+</sup> is the inverting input of the average current mode loop error amplifier. This pin is connected to the external current sense resistor, R<sub>S</sub>. The voltage drop between SENSE<sup>+</sup> and SENSE<sup>-</sup> referenced to the voltage drop across an internal resistor produces the input voltages to the current regulation loop.

**SENSE<sup>-</sup> (Pin 9/Pin 12):** SENSE<sup>-</sup> is the non-inverting input of the average current mode loop error amplifier. The reference current, based on CTRL1 or CTRL2 flows out of the pin to the output side of the sense resistor, R<sub>S</sub>.

**VC (Pin 10/Pin 13):** VC provides the necessary compensation for the average current loop stability. Typical compensation values are 20k to 50k for the resistor and 2nF to 5nF for the capacitor.

**RT (Pin 12/Pin 14):** A resistor to ground sets the switching frequency between 200kHz and 1MHz. When using the SYNC function, set the frequency to be 20% lower than the SYNC pulse frequency. This pin is current limited to 60μA. Do not leave this pin open.

**SYNC (Pin 13/Pin 15):** Frequency Synchronization Pin. This pin allows the switching frequency to be synchronized to an external clock. The R<sub>T</sub> resistor should be chosen to operate the internal clock at 20% slower than the SYNC pulse frequency. This pin should be grounded when not in use. When laying out board, avoid noise coupling to or from SYNC trace.

**HG (Pin 15/Pin 17):** HG is the top-FET gate drive signal that controls the state of the high-side external power FET. The driver pull-up impedance is 2.3Ω and pull-down impedance is 1.3Ω.

**SW (Pin 16/Pin 18):** The SW pin is used internally as the lower-rail for the floating high-side driver. Externally, this node connects the two power-FETs and the inductor.

**CBOOT (Pin 17/Pin 19):** The CBOOT pin provides a floating 5V regulated supply for the high-side FET driver. An external Schottky diode is required from the V<sub>CC\_INT</sub> pin to the CBOOT pin to charge the CBOOT capacitor when the switch-pin is near ground.

**LG (Pin 18/Pin 20):** LG is the bottom-FET gate drive signal that controls the state of the low-side external power-FET. The driver pull-up impedance is 2.3Ω and pull-down impedance is 1.0Ω.

**V<sub>CC\_INT</sub> (Pin 19/Pin 1):** A regulated 5V output for charging the CBOOT capacitor. V<sub>CC\_INT</sub> also provides the power for the digital and switching subcircuits. Below 6V V<sub>IN</sub>, tie this pin to the rail. V<sub>CC\_INT</sub> is current limited to 50mA. Shutdown operation disables the output voltage drive.

**V<sub>IN</sub> (Pin 20/Pin 3):** Input Supply Pin. Must be locally bypassed with a 4.7μF low-ESR capacitor to ground.



# LT3741/LT3741-1

## BLOCK DIAGRAM (QFN Package)

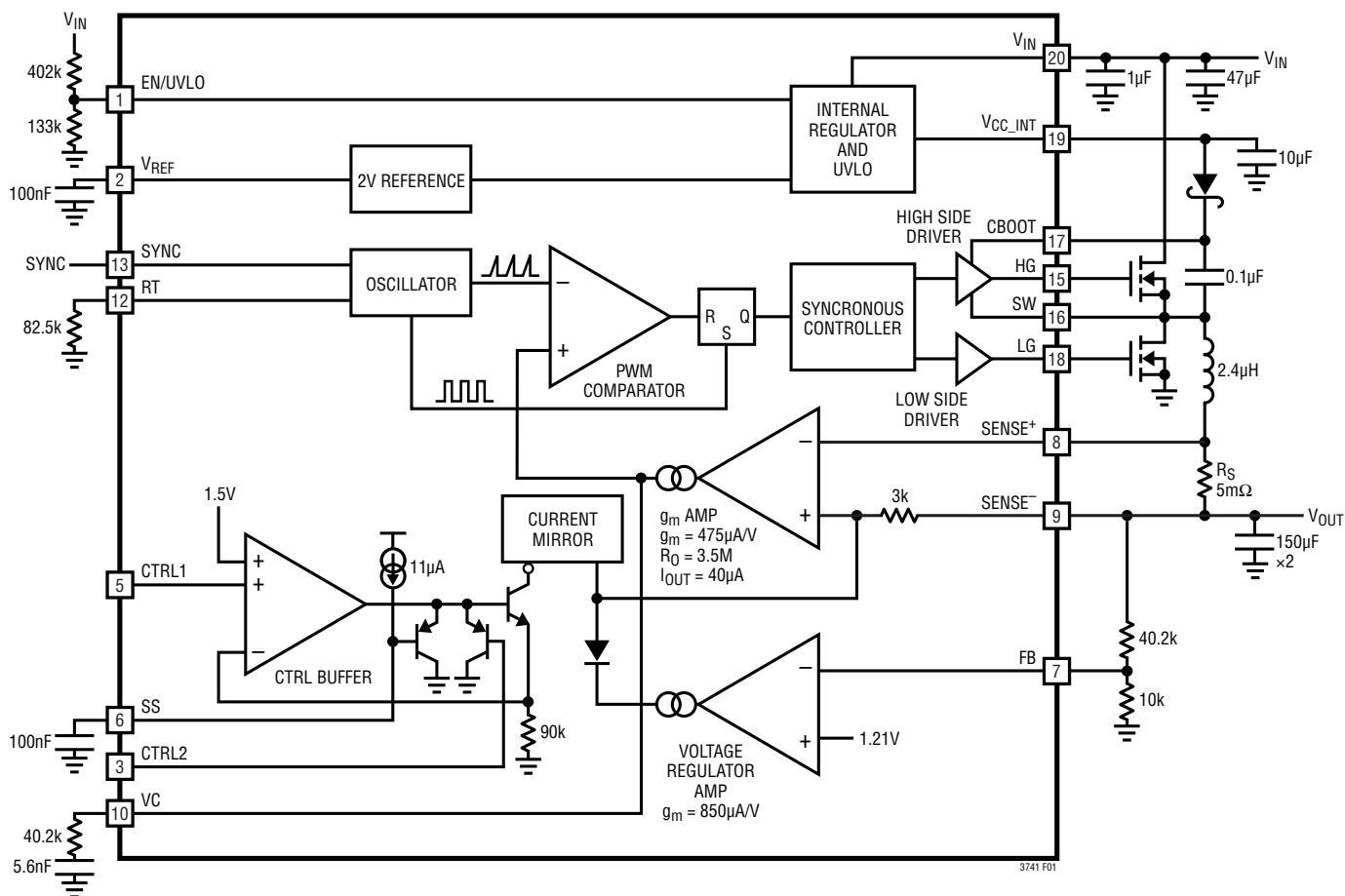


Figure 1. Block Diagram, LT3741

# BLOCK DIAGRAM (QFN Package)

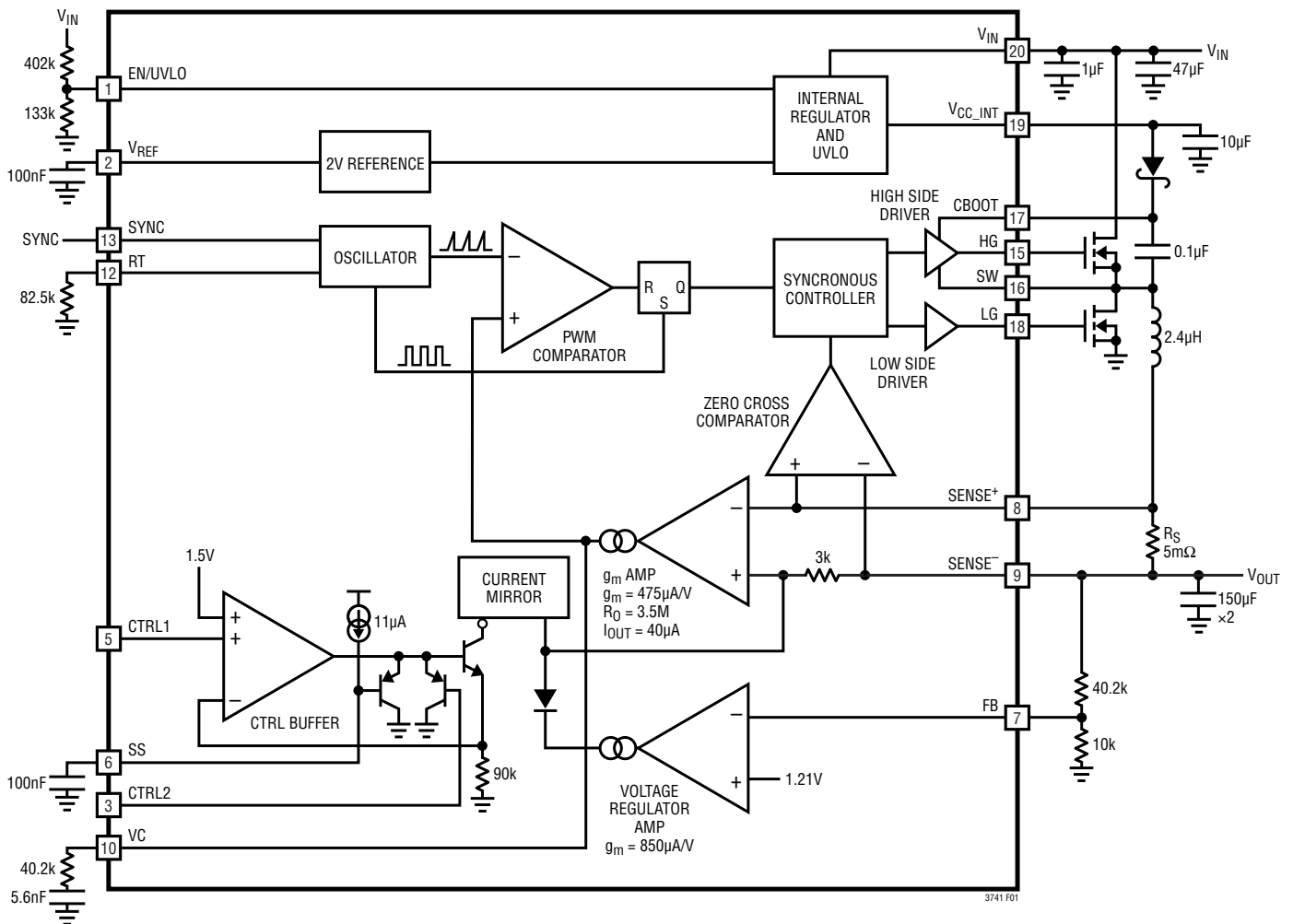


Figure 2. Block Diagram, LT3741-1

## OPERATION

The LT3741 utilizes fixed-frequency, average current mode control to accurately regulate the inductor current, independently from the output voltage. This is an ideal solution for applications requiring a regulated current source. The control loop will regulate the current in the inductor at an accuracy of  $\pm 6\%$ . Once the output has reached the regulation voltage determined by the resistor divider from the output to the FB pin and ground, the inductor current will be reduced by the voltage regulation loop. In voltage regulation, the output voltage has an accuracy of  $\pm 1.5\%$ . For additional operation information, refer to the Block Diagram in Figure 1.

The current control loop has two reference inputs, determined by the voltage at the analog control pins, CTRL1 and CTRL2. The lower of the two analog voltages on CTRL1 and CTRL2 determines the regulated output current. The analog voltage at the CTRL1 pin is buffered and produces a reference voltage across an internal resistor. The internal buffer has a 1.5V clamp on the output, limiting the analog control range of the CTRL1 and CTRL2 pins from 0V to 1.5V – corresponding to a 0mV to 51mV range on the sense resistor,  $R_S$ . The average current-mode control loop uses the internal reference voltage to regulate the inductor current, as a voltage drop across the external sense resistor,  $R_S$ .

A 2V reference voltage is provided on the  $V_{REF}$  pin to allow the use of a resistor voltage divider to the CTRL1 and CTRL2 pins. The  $V_{REF}$  pin can supply up to 500 $\mu$ A and is current limited to 1mA.

The error amplifier for the average current-mode control loop has a common mode lockout that regulates the inductor current so that the error amplifier is never operated out of the common mode range. The common mode range is from 0V to 2V below the  $V_{IN}$  supply rail.

The overcurrent set point is equal to the regulated current level set by the CTRL1 pin with an additional 23mV offset between the SENSE<sup>+</sup> and SENSE<sup>-</sup> pins. The overcurrent

is limited on a cycle-by-cycle basis; shutting switching down once the overcurrent level is reached. Overcurrent is not soft-started.

The regulated output voltage is set with a resistor divider from the output back to the FB pin. The reference at the FB pin is 1.21V. If the output voltage level is high enough to engage the voltage loop, the regulated inductor current will be reduced to support the load at the output. If the voltage at the FB pin reaches 1.5V (~25% higher than the regulation level), an internal overvoltage flag is set, shutting down switching for 13 $\mu$ s.

The EN/UVLO pin functions as a precision shutdown pin. When the voltage at the EN/UVLO pin is lower than 1.55V, the internal reset flag is asserted and switching is terminated. Full shutdown occurs at approximately 0.5V with a quiescent current of less than 1 $\mu$ A in full shutdown. The EN/UVLO pin has 130mV of built-in hysteresis. In addition, a 5.5 $\mu$ A current source is connected to this pin that allows any amount of hysteresis to be added with a series resistor or resistor divider from  $V_{IN}$ .

During startup, the SS pin is held low until the internal reset goes low. Once reset goes low, the capacitor at the soft-start pin is charged with an 11 $\mu$ A current source. The internal buffers for the CTRL1 and CTRL2 signals are limited by the voltage at the soft-start pin, slowly ramping the regulated inductor current to the current determined by the voltage at the CTRL1 or CTRL2 pins.

The thermal shutdown is set at 163°C with 8°C hysteresis. During thermal shutdown, all switching is terminated and the part is in reset (forcing the SS pin low).

The switching frequency is determined by a resistor at the RT pin. The RT pin is also limited to 60 $\mu$ A, while not recommended, this limits the switching frequency to 2MHz when the RT pin is shorted to ground. The LT3741 may also be synchronized to an external clock through the use of the SYNC pin.

## APPLICATIONS INFORMATION

### Programming Inductor Current

The analog voltage at the CTRL1 pin is buffered and produces a reference voltage,  $V_{CTRL}$ , across an internal resistor. The regulated average inductor current is determined by:

$$I_0 = \frac{V_{CTRL}}{30 \cdot R_S}$$

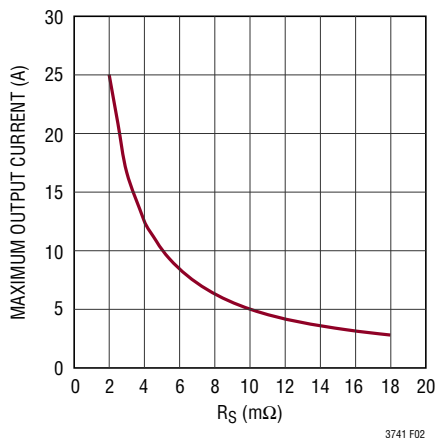
where  $R_S$  is the external sense resistor and  $I_0$  is the average inductor current, which is equal to the output current. Figure 2 shows the maximum output current vs  $R_S$ . The maximum power dissipation in the resistor will be:

$$P_{RS} = \frac{(0.05V)^2}{R_S}$$

Table 1 contains several resistors values, the corresponding maximum current and power dissipation in the sense resistor. Susumu, Panasonic and Vishay offer accurate sense resistors. Figure 3 shows the power dissipation in  $R_S$ .

**Table 1. Sense Resistor Values**

MAXIMUM OUTPUT CURRENT (A)	RESISTOR, $R_S$ (mΩ)	POWER DISSIPATION (W)
1	50	0.05
5	10	0.25
10	5	0.5
25	2	1.25



**Figure 2.  $R_S$  Value Selection for Regulated Output Current**

### Inductor Selection

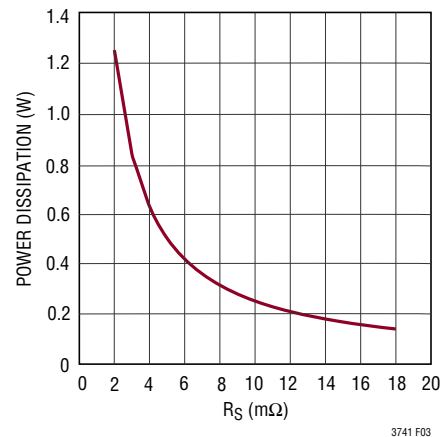
Size the inductor to have approximately 30% peak-to-peak ripple. The overcurrent set point is equal to the high level regulated current level set by the CTRL1 pin with an additional 23mV offset between the SENSE+ and SENSE- pins. The saturation current for the inductor should be at least 20% higher than the maximum regulated current. The following equation sizes the inductor for best performance:

$$L = \left( \frac{V_{IN} \cdot V_O - V_O^2}{0.3 \cdot f_S \cdot I_0 \cdot V_{IN}} \right)$$

where  $V_O$  is the output voltage,  $I_0$  is the maximum regulated current in the inductor and  $f_S$  is the switching frequency. Using this equation, the inductor will have approximately 15% ripple at maximum regulated current.

**Table 2. Recommended Inductor Manufacturers**

VENDOR	WEBSITE
Coilcraft	<a href="http://www.coilcraft.com">www.coilcraft.com</a>
Sumida	<a href="http://www.sumida.com">www.sumida.com</a>
Vishay	<a href="http://www.vishay.com">www.vishay.com</a>
Würth Electronics	<a href="http://www.we-online.com">www.we-online.com</a>
NEC-Tokin	<a href="http://www.nec-tokin.com">www.nec-tokin.com</a>



**Figure 3. Power Dissipation in  $R_S$**

### Switching MOSFET Selection

When selecting switching MOSFETs, the following parameters are critical in determining the best devices for a given application: total gate charge ( $Q_G$ ), on-resistance

## APPLICATIONS INFORMATION

( $R_{DS(ON)}$ ), gate to drain charge ( $Q_{GD}$ ), gate-to-source charge ( $Q_{GS}$ ), gate resistance ( $R_G$ ), breakdown voltages (maximum  $V_{GS}$  and  $V_{DS}$ ) and drain current (maximum  $I_D$ ). The following guidelines provide information to make the selection process easier.

Both of the switching MOSFETs need to have their maximum rated drain currents greater than the maximum inductor current. The following equation calculates the peak inductor current:

$$I_{MAX} = I_O + \left( \frac{V_{IN} \cdot V_O - V_O^2}{2 \cdot f_S \cdot L \cdot V_{IN}} \right)$$

where  $V_{IN}$  is the input voltage,  $L$  is the inductance value,  $V_O$  is the output voltage,  $I_O$  is the regulated output current and  $f_S$  is the switching frequency. During MOSFET selection, notice that the maximum drain current is temperature dependant. Most data sheets include a table or graph of the maximum rated drain current vs temperature.

The maximum  $V_{DS}$  should be selected to be higher than the maximum input supply voltage (including transient) for both MOSFETs. The signals driving the gates of the switching MOSFETs have a maximum voltage of 5V with respect to the source. During start-up and recovery conditions, the gate drive signals may be as low as 3V. To ensure that the LT3741 recovers properly, the maximum threshold should be less than 2V. For a robust design, select the maximum  $V_{GS}$  greater than 7V.

Power losses in the switching MOSFETs are related to the on-resistance,  $R_{DS(ON)}$ ; the transitional loss related to the gate resistance,  $R_G$ ; gate-to-drain capacitance,  $Q_{GD}$  and gate-to-source capacitance,  $Q_{GS}$ . Power loss to the on-resistance is an Ohmic loss,  $I^2 R_{DS(ON)}$ , and usually dominates for input voltages less than ~15V. Power losses to the gate capacitance dominate for voltages greater than ~12V. When operating at higher input voltages, efficiency can be optimized by selecting a high side MOSFET with higher  $R_{DS(ON)}$  and lower  $C_{GD}$ . The power loss in the high side MOSFET can be approximated by:

$$P_{LOSS} = (\text{ohmic loss}) + (\text{transition loss})$$

$$P_{LOSS} \approx \left( \frac{V_O}{V_{IN}} \cdot I_O^2 R_{DS(ON)} \cdot \rho_T \right) + \left( \left( \frac{V_{IN} \cdot I_{OUT}}{5V} \right) \cdot ((Q_{GD} + Q_{GS}) \cdot (2 \cdot R_G + R_{PU} + R_{PD})) \cdot f_S \right)$$

where  $\rho_T$  is a temperature-dependant term of the MOSFET's on-resistance. Using 70°C as the maximum ambient operating temperature,  $\rho_T$  is roughly equal to 1.3.  $R_{PD}$  and  $R_{PU}$  are the LT3741 high side gate driver output impedance, 1.3Ω and 2.3Ω respectively.

A good approach to MOSFET sizing is to select a high side MOSFET, then select the low side MOSFET. The trade-off between  $R_{DS(ON)}$ ,  $Q_G$ ,  $Q_{GD}$  and  $Q_{GS}$  for the high side MOSFET is shown in the following example.  $V_O$  is equal to 4V. Comparing two N-channel MOSFETs, with a rated  $V_{DS}$  of 40V and in the same package, but with 8× different  $R_{DS(ON)}$  and 4.5× different  $Q_G$  and  $Q_{GD}$ :

$$\text{M1: } R_{DS(ON)} = 2.3\text{m}\Omega, Q_G = 45.5\text{nC}, \\ Q_{GS} = 13.8\text{nC}, Q_{GD} = 14.4\text{nC}, R_G = 1\Omega$$

$$\text{M2: } R_{DS(ON)} = 18\text{m}\Omega, Q_G = 10\text{nC}, \\ Q_{GS} = 4.5\text{nC}, Q_{GD} = 3.1\text{nC}, R_G = 3.5\Omega$$

Power loss for both MOSFETs is shown in Figure 4. Observe that while the  $R_{DS(ON)}$  of M1 is eight times lower, the power loss at low input voltages is equal, but four times higher at high input voltages than the power loss for M2.

Power loss within the low side MOSFET is almost entirely from the  $R_{DS(ON)}$  of the FET. Select a low side FET with the lowest  $R_{DS(ON)}$  while keeping the total gate charge  $Q_G$  to 30nC or less.

Another power loss related to switching MOSFET selection is the power lost to driving the gates. The total gate charge,  $Q_G$ , must be charged and discharged each switching cycle. The power is lost to the internal LDO within the LT3741. The power lost to the charging of the gates is:

$$P_{LOSS\_LDO} \approx (V_{IN} - 5V) \cdot (Q_{GLG} + Q_{GHG}) \cdot f_S$$

where  $Q_{GLG}$  is the low side gate charge and  $Q_{GHG}$  is the high side gate charge.

Whenever possible, utilize a switching MOSFET that minimizes the total gate charge to limit the internal power dissipation of the LT3741.

## APPLICATIONS INFORMATION

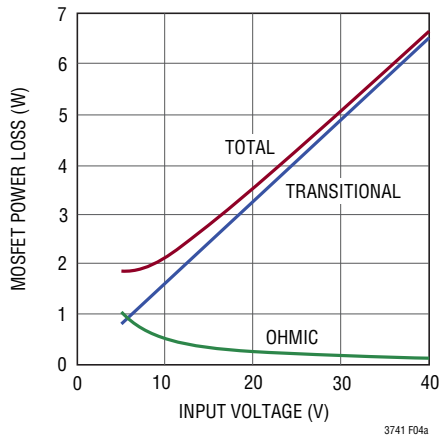


Figure 4a. Power Loss Example for M1

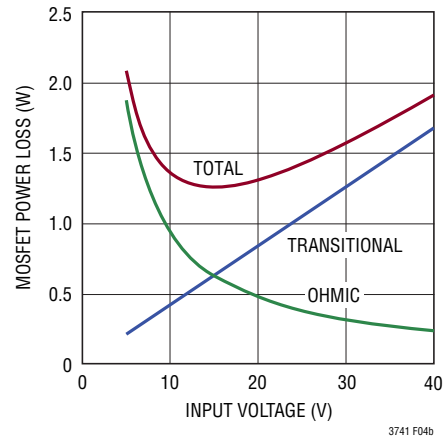


Figure 4b. Power Loss Example for M2

Figure 4

Table 3. Recommended Switching FETs

V <sub>IN</sub> (V)	V <sub>OUT</sub> (V)	I <sub>OUT</sub> (A)	TOP FET	BOTTOM FET	MANUFACTURER
8	4	5-10	RJK0365DPA	RJK0330DPB	Renesas www.renesas.com
24	4	5	RJK0368DPA	RJK0332DPB	
24	2-4	20	RJK0365DPA	RJK0346DPA	
12	2-4	10	FDMS8680	FDMS8672AS	Fairchild www.fairchildsemi.com
36	4	20	Si7884BDP	SiR470DP	Vishay www.vishay.com
24	4	40	PSMN4R0-30YL	RJK0346DPA	NXP/Philips www.nxp.com

## Input Capacitor Selection

The input capacitor should be sized at 4μF for every 1A of output current and placed very close to the high side MOSFET. A small 1μF ceramic capacitor should be placed near the V<sub>IN</sub> and ground pins of the LT3741 for optimal noise immunity. The input capacitor should have a ripple current rating equal to half of the maximum output current. It is recommended that several low ESR ceramic capacitors be used as the input capacitance. Use only type X5R or X7R capacitors as they maintain their capacitance over a wide range of operating voltages and temperatures.

## Output Capacitor Selection

The output capacitors need to have very low ESR (equivalent series resistance) to reduce output ripple. A minimum of

20μF/A of load current should be used in most designs. The capacitors also need to be surge rated to the maximum output current. To achieve the lowest possible ESR, several low ESR capacitors should be used in parallel. Many applications benefit from the use of high density POSCAP capacitors, which are easily destroyed when exposed to overvoltage conditions. To prevent this, select POSCAP capacitors that have a voltage rating that is at least 50% higher than the regulated voltage.

C<sub>BOOT</sub> Capacitor Selection

The C<sub>BOOT</sub> capacitor must be sized less than 220nF and more than 50nF to ensure proper operation of the LT3741. Use 220nF for high current switching MOSFETs with high gate charge.

V<sub>CC\_INT</sub> Capacitor Selection

The bypass capacitor for the V<sub>CC\_INT</sub> pin should be larger than 5μF for stability and has no ESR requirement. It is recommended that the ESR be lower than 50mΩ to reduce noise within the LT3741. For driving MOSFETs with gate charges larger than 10nC, use 0.5μF/nC of total gate charge.

## Soft-Start

Unlike conventional voltage regulators, the LT3741 utilizes the soft-start function to control the regulated inductor current. The charging current is 11μA and reduces the regulated current when the SS pin voltage is lower than CTRL1.

## APPLICATIONS INFORMATION

### Output Current Regulation

To adjust the regulated load current, an analog voltage is applied to the CTRL1 pin. Figure 5 shows the regulated voltage across the sense resistor for control voltages up to 2V. Figure 6 shows the CTRL1 voltage created by a voltage divider from  $V_{REF}$  to ground. When sizing the resistor divider, please be aware that the  $V_{REF}$  pin is current limited to 500 $\mu$ A. Above 1.5V, the control voltage has no effect on the regulated inductor current.

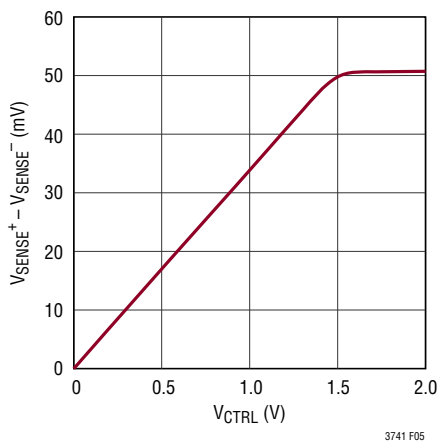


Figure 5. Sense Voltage vs CTRL Voltage

### Voltage Regulation and Overvoltage Protection

The LT3741 uses the FB pin to regulate the output voltage and to provide a high speed overvoltage lockout to avoid high voltage conditions. The regulated output voltage is programmed using a resistor divider from the output and ground (Figure 7). When the output voltage exceeds 125% of the regulated voltage level (1.5V at the FB pin), the internal overvoltage flag is set, terminating switching. The regulated output voltage must be greater than 1.5V and is set by the equation:

$$V_{OUT} = 1.21V \left( 1 + \frac{R2}{R1} \right)$$

### Programming Switching Frequency

The LT3741 has an operational switching frequency range between 200kHz and 1MHz. This frequency is programmed with an external resistor from the RT pin to ground. Do not

leave this pin open under any condition. The RT pin is also current limited to 60 $\mu$ A. See Table 4 and Figure 8 for resistor values and the corresponding switching frequencies.

Table 4. Switching Frequency

SWITCHING FREQUENCY (MHz)	$R_T$ (k $\Omega$ )
1	40.2
0.750	53.6
0.5	82.5
0.3	143
0.2	200

### Thermal Shutdown

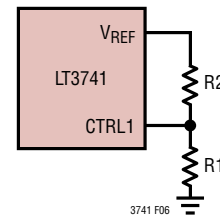


Figure 6. Analog Control of Inductor Current

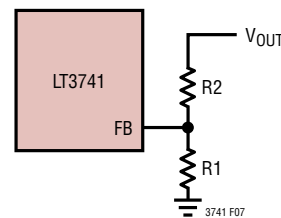


Figure 7. Output Voltage Regulation and Overvoltage Protection Feedback Connections

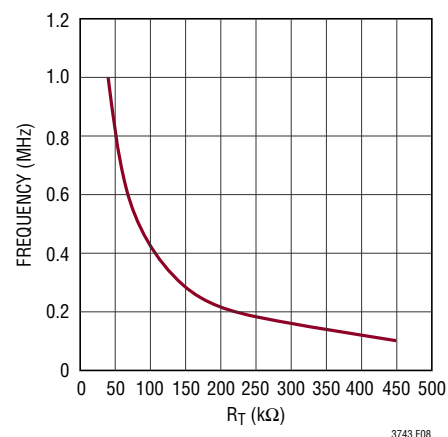


Figure 8. Frequency vs  $R_T$  Resistance



## APPLICATIONS INFORMATION

The internal thermal shutdown within the LT3741 engages at 163°C and terminates switching and resets soft-start. When the part has cooled to 155°C, the internal reset is cleared and soft-start is allowed to charge.

### Switching Frequency Synchronization

The nominal switching frequency of the LT3741 is determined by the resistor from the RT pin to ground and may be set from 200kHz to 1MHz. The internal oscillator may also be synchronized to an external clock through the SYNC pin. The external clock applied to the SYNC pin must have a logic low below 0.3V and a logic high higher than 1.25V. The input frequency must be 20% higher than the frequency determined by the resistor at the RT pin. Input signals outside of these specified parameters will cause erratic switching behavior and subharmonic oscillations. Synchronization is tested at 500kHz with a 200k  $R_T$  resistor. Operation under other conditions is guaranteed by design. When synchronizing to an external clock, please be aware that there will be a fixed delay from the input clock edge to the edge of switch. The SYNC pin must be grounded if the synchronization to an external clock is not required. When SYNC is grounded, the switching frequency is determined by the resistor at the RT pin.

### Shutdown and UVLO

The LT3741 has an internal UVLO that terminates switching, resets all synchronous logic, and discharges the soft-start capacitor for input voltages below 4.2V. The LT3741 also has a precision shutdown at 1.55V on the EN/UVLO pin. Partial shutdown occurs at 1.55V and full shutdown is guaranteed below 0.5V with  $<1\mu A$   $I_Q$  in the full shutdown state. Below 1.55V, an internal current source provides 5.5 $\mu A$  of pull-down current to allow for programmable UVLO hysteresis. The following equations determine the voltage divider resistors for programming the UVLO voltage and hysteresis as configured in Figure 9.

$$R2 = \frac{V_{HYST}}{5.5\mu A} - \frac{V_{UVLO}}{66\mu A}$$

$$R1 = \left( \frac{1.55V \cdot R2}{V_{UVLO} - 1.55V} \right)$$

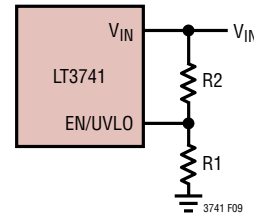


Figure 9. UVLO Configuration

The EN/UVLO pin has an absolute maximum voltage of 6V. To accommodate the largest range of applications, there is an internal Zener diode that clamps this pin. For applications where the supply range is greater than 4:1, size R2 greater than 375k.

### Load Current Derating Using the CTRL2 Pin

The LT3741 is designed specifically for driving high power loads. In high current applications, derating the maximum current based on operating temperature prevents damage to the load. In addition, many applications have thermal limitations that will require the regulated current to be reduced based on load and/or board temperature. To achieve this, the LT3741 uses the CTRL2 pin to reduce the effective regulated current in the load. While CTRL1 programs the regulated current in the load, CTRL2 can be configured to reduce this regulated current based on the analog voltage at the CTRL2 pin. The load/board temperature derating is programmed using a resistor divider with a temperature dependant resistance (Figure 10). When the board/load temperature rises, the CTRL2 voltage will decrease. To reduce the regulated current, the CTRL2 voltage must be lower than voltage at the CTRL1 pin.

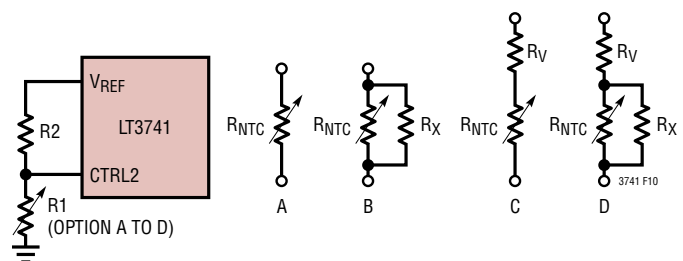


Figure 10. Load Current Derating vs Temperature Using NTC Resistor



## APPLICATIONS INFORMATION

### Average Current Mode Control Compensation

The use of average current mode control allows for precise regulation of the inductor and load currents. Figure 11 shows the average current mode control loop used in the LT3741, where the regulation current is programmed by a current source and a 3k resistor.

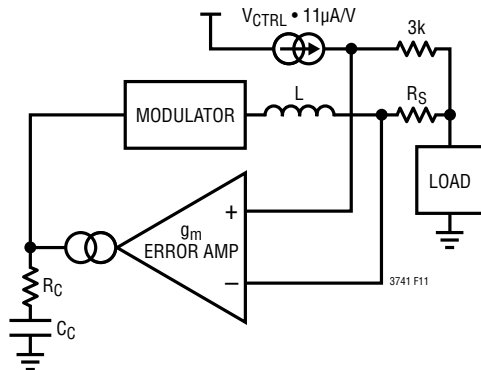


Figure 11. LT3741 Average Current Mode Control Scheme

To design the compensation network, the maximum compensation resistor needs to be calculated. In current mode controllers, the ratio of the sensed inductor current ramp to the slope compensation ramp determines the stability of the current regulation loop above 50% duty cycle. In the same way, average current mode controllers require the slope of the error voltage to not exceed the PWM ramp slope during the switch off-time.

Since the closed-loop gain at the switching frequency produces the error signal slope, the output impedance of

the error amplifier will be the compensation resistor,  $R_C$ . Use the following equation as a good starting point for compensation component sizing:

$$R_C = \frac{f_S \cdot L \cdot 1000V}{V_O \cdot R_S} [\Omega], C_C = \frac{0.002}{f_S} [F]$$

where  $f_S$  is the switching frequency,  $L$  is the inductance value,  $V_O$  is the output voltage and  $R_S$  is the sense resistor. For most applications, a 4.7nF compensation capacitor is adequate and provides excellent phase margin with optimized bandwidth. Please refer to Table 6 for recommended compensation values.

### Board Layout Considerations

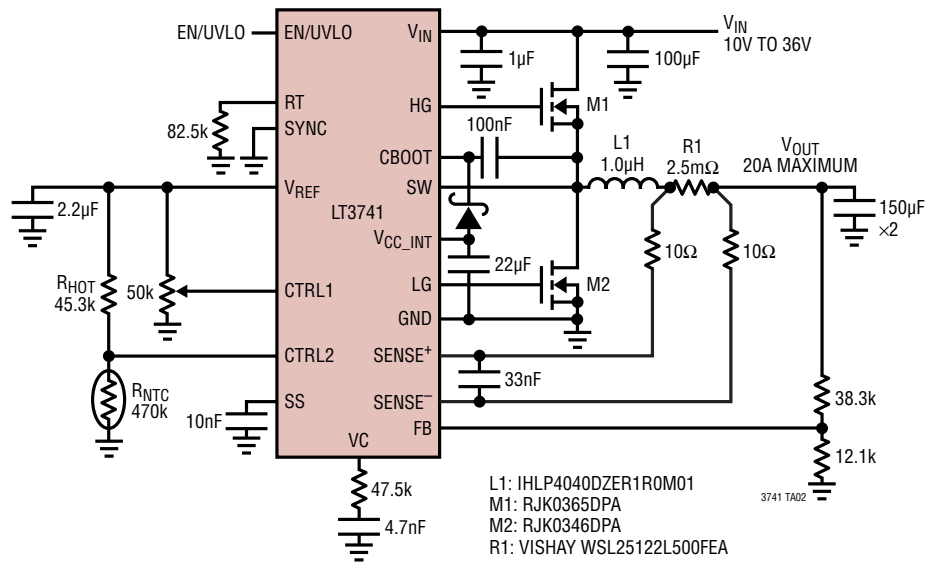
Average current mode control is relatively immune to the switching noise associated with other types of control schemes. Placing the sense resistor as close as possible to the SENSE+ and SENSE- pins avoids noise issues. Due to sense resistor ESL (equivalent series inductance), a 10Ω resistor in series with the SENSE+ and SENSE- pins with a 33nF capacitor placed between the SENSE pins is recommended. Utilizing a good ground plane underneath the switching components will minimize interplane noise coupling. To dissipate the heat from the switching components, use a large area for the switching mode while keeping in mind that this negatively affects the radiated noise.

Table 6. Recommended Compensation Values

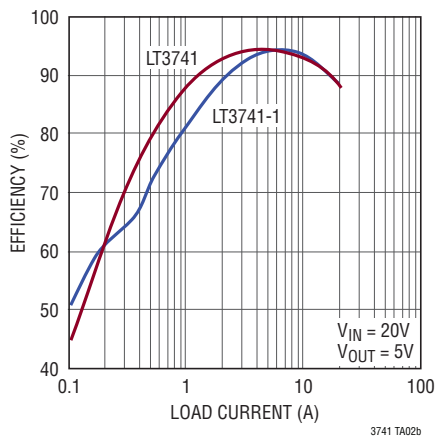
$V_{IN}$ (V)	$V_O$ (V)	$I_L$ (A)	$f_{SW}$ (MHz)	$L$ (µH)	$R_S$ (mΩ)	$R_C$ (kΩ)	$C_C$ (nF)
12	4	5	0.5	1.5	5	47.5	4.7
12	4	10	0.5	1.5	5	47.5	4.7
12	5	20	0.25	1.8	2.5	38.3	8.2
24	4	2	0.5	1.0	2.5	52.3	4.7
24	4	20	0.5	1.0	2.5	52.3	4.7

## TYPICAL APPLICATIONS

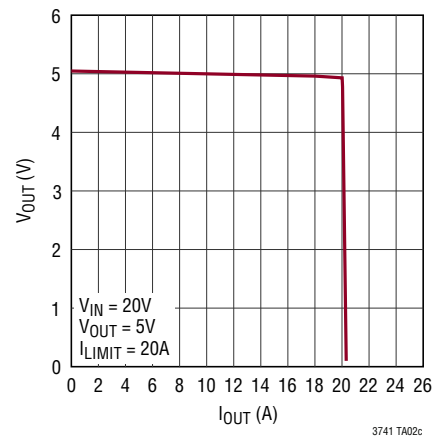
## 20A Super Capacitor Charger with 5V Regulated Output



### Efficiency and Power Loss vs Load Current

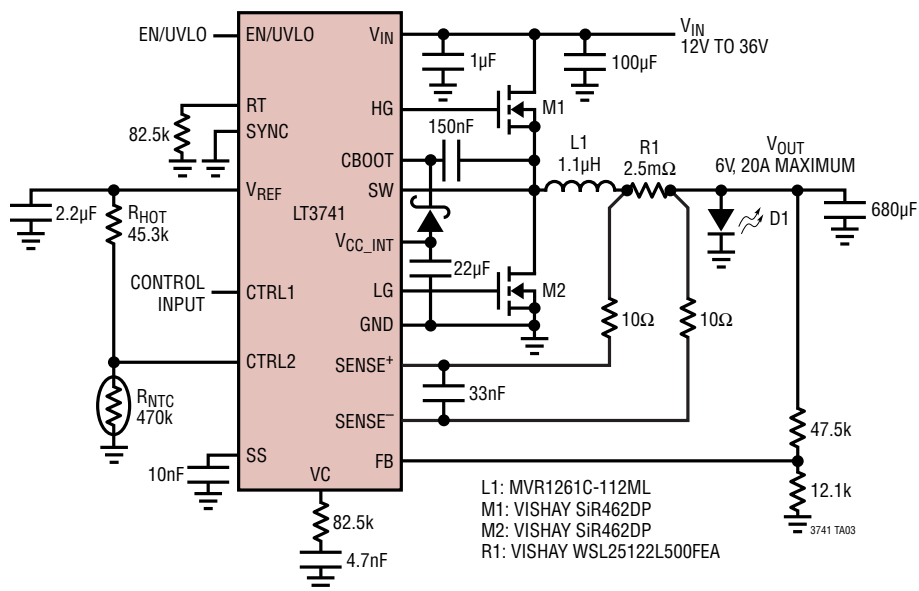


### V<sub>OUT</sub> vs I<sub>OUT</sub>

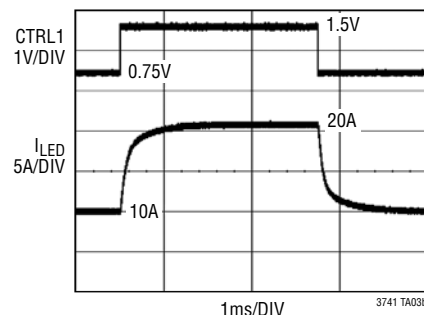


## TYPICAL APPLICATIONS

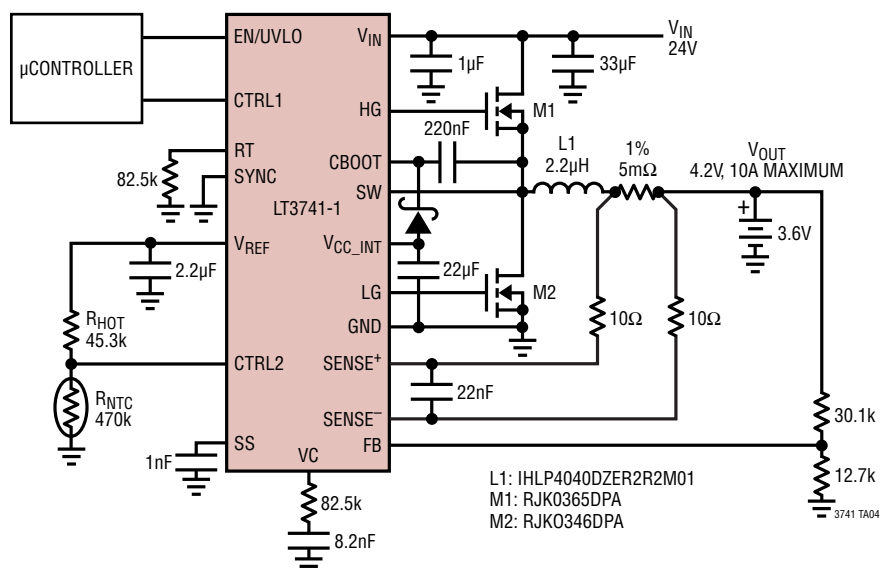
### 20A LED Driver



### LED Current Waveforms 10A to 20A Current Step



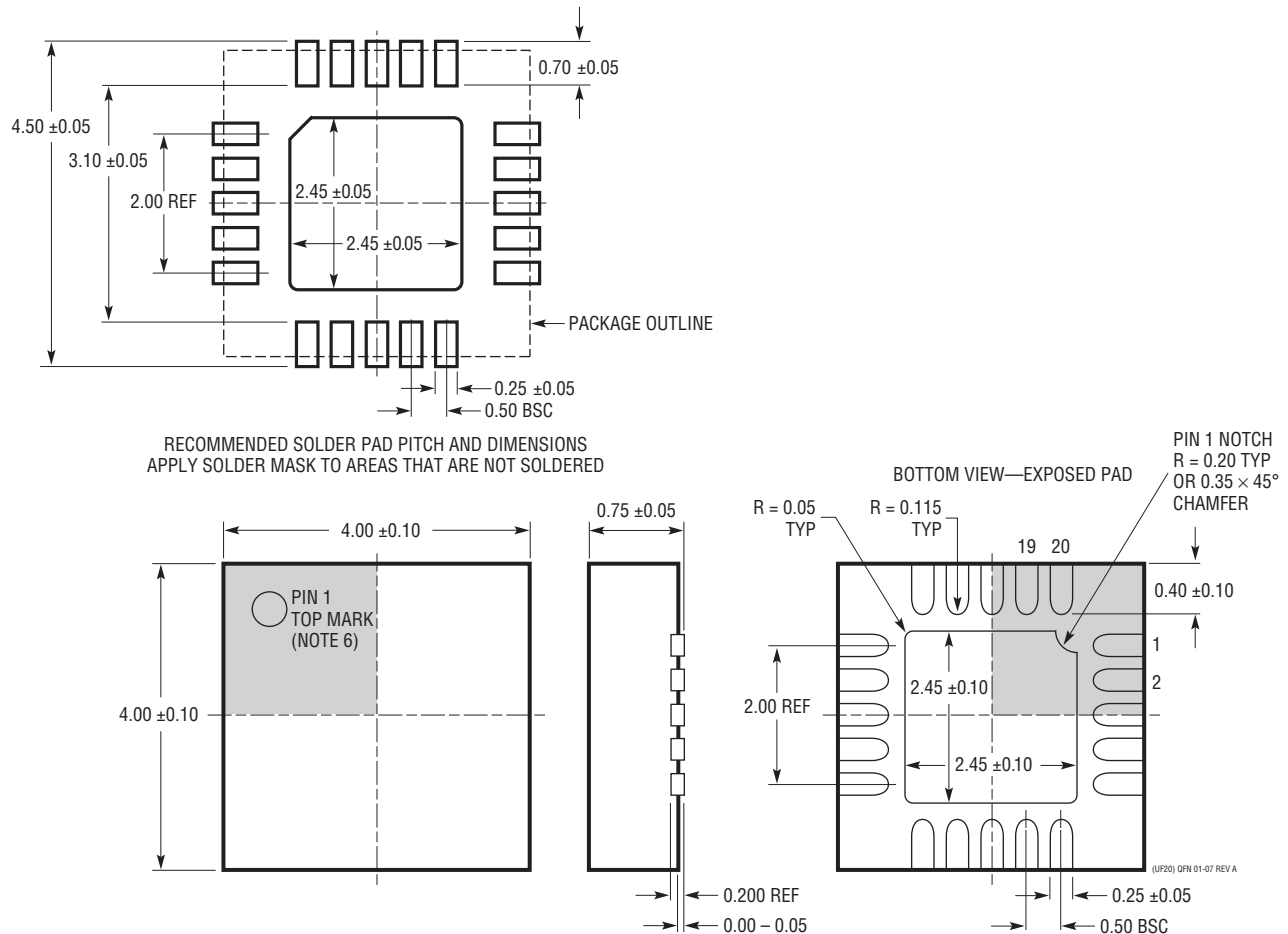
### 10A Single-Cell Lithium-Ion Battery Charger



# PACKAGE DESCRIPTION

Please refer to <http://www.linear.com/product/LT3741#packaging> for the most recent package drawings.

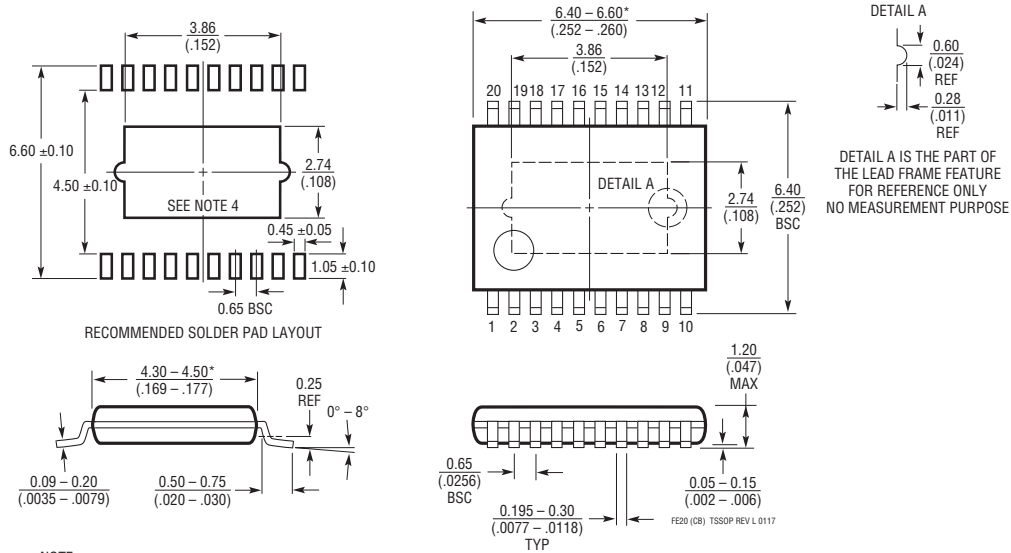
## UF Package 20-Lead Plastic QFN (4mm × 4mm) (Reference LTC DWG # 05-08-1710 Rev A)



## PACKAGE DESCRIPTION

Please refer to <http://www.linear.com/product/LT3741#packaging> for the most recent package drawings.

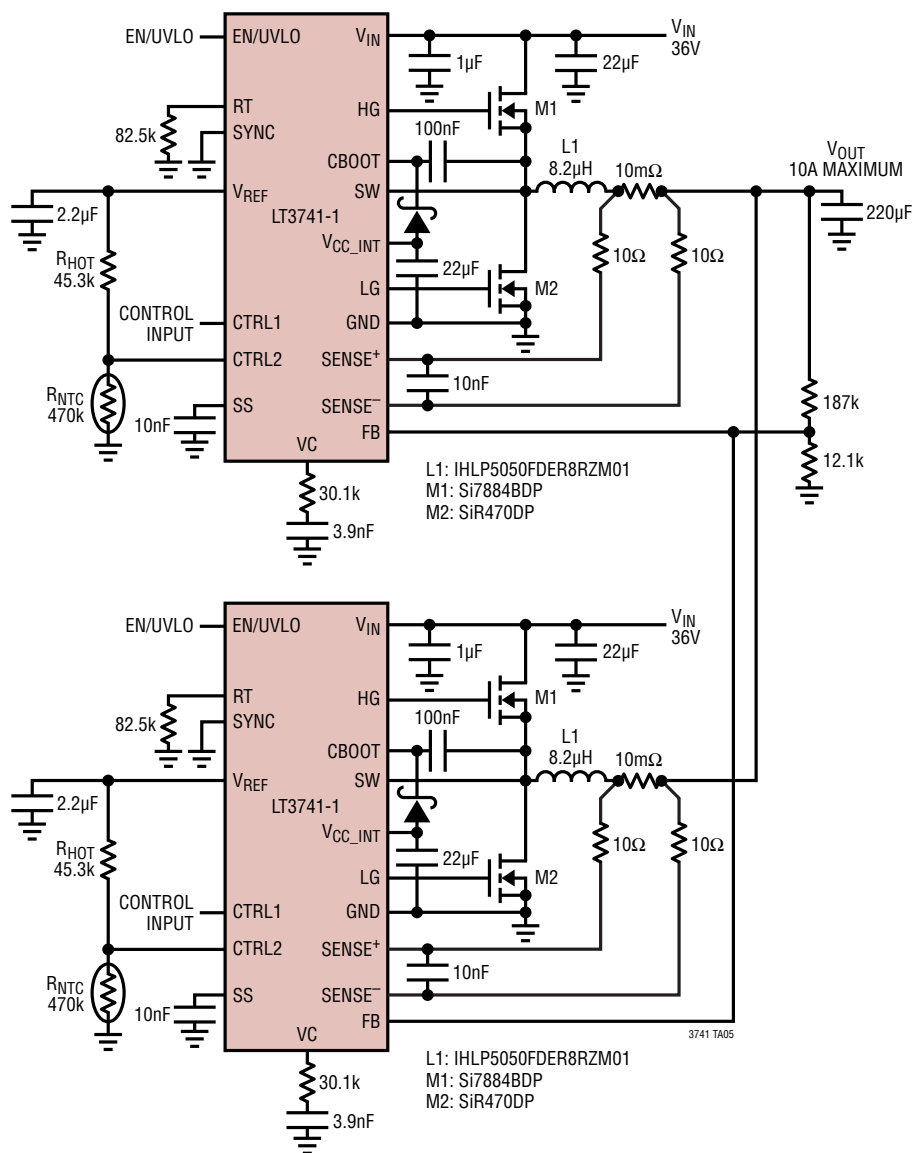
**FE Package**  
**20-Lead Plastic TSSOP (4.4mm)**  
 (Reference LTC DWG # 05-08-1663 Rev L)  
**Exposed Pad Variation CB**



## REVISION HISTORY

REV	DATE	DESCRIPTION	PAGE NUMBER
A	8/10	Revised to $\pm 1.5\%$ Voltage Regulation Accuracy in Features section	1
		Revised Absolute Maximum Ratings to delete CBOOT-SW Voltage	2
		Updated Electrical Characteristics section	3, 4
		Updated RT, HG and LG pin descriptions	10
		Updated Block Diagram	11
		Revised text, added a paragraph and revised equations in Applications Information section	13, 14
		Revised Table 4 and Switching Frequency Synchronization paragraph in the Applications Information section	16, 17
		Revised Typical Applications drawings and added vendor part numbers	19, 20, 24
		Updated Related Parts	24
B	9/10	Revised Voltage Regulator Amp value to $g_m = 800\mu A/V$ on Figure 1 Block Diagram	11
C	5/13	Added LT3741-1 Option	All
		Added LT3741-1 Option to Order Information	2
		Clarified Non-Overlap and CTRL Current Specifications	3
		Clarified Regulated Current vs $V_{FB}$ Graph	6
		Clarified Efficiency Graphs	8
		Clarified Common Mode Lockout Graph	9
		Added LT3741-1 Block Diagram	11
		Clarified Efficiency Graph	19
		Clarified Part Number on Schematic	20
D	9/13	Corrected package descriptions in Order Information section	2
E	1/14	Corrected package in Block Diagram	11
F	10/15	Revised UVLO Hysteresis Equation	17
G	11/17	Revised VC cap value Figures 1 and 2	10, 11
		Changed pin name to VC, 20A LED Driver circuit	20

## 20V Regulated Output with 5A Current Limit



## RELATED PARTS

PART NUMBER	DESCRIPTION	COMMENTS
LT3743	Synchronous Step-Down LED Driver	92% Efficiency, I <sub>OUT</sub> to 20A, V <sub>IN</sub> : 5.5V to 36V, I <sub>Q</sub> = 2mA, I <sub>SD</sub> < 1μA, 4mm × 5mm QFN-28, TSSOP-28E