

## Specifications

### Absolute Maximum Ratings at $T_c = 25^\circ\text{C}$

Parameter	Symbol	Conditions	Ratings	unit
Maximum supply voltage 1	$V_{CC}$ max	No signal	52	V
Maximum supply voltage 2	$V_{DD}$ max	No signal	-0.3 to +7.0	V
Input voltage	$V_{IN}$ max	Logic input pins	-0.3 to +7.0	V
Output current	$I_{OH}$ max	$V_{DD}=5\text{V}$ , $\text{CLOCK}\geq 200\text{Hz}$	4.0	A
Allowable power dissipation 1	$P_{DMF}$ max	With an arbitrarily large heat sink. Per MOSFET	10.2	W
Allowable power dissipation 2	$P_{DPK}$ max	No heat sink	3.1	W
Operating substrate temperature	$T_c$ max		105	$^\circ\text{C}$
Junction temperature	$T_j$ max		150	$^\circ\text{C}$
Storage temperature	$T_{stg}$		-40 to +125	$^\circ\text{C}$

Stresses exceeding Maximum Ratings may damage the device. Maximum Ratings are stress ratings only. Functional operation above the Recommended Operating Conditions is not implied. Extended exposure to stresses above the Recommended Operating Conditions may affect device reliability.

### Allowable Operating Ranges at $T_a = 25^\circ\text{C}$

Parameter	Symbol	Conditions	Ratings	unit
Operating supply voltage 1	$V_{CC}$	With signals applied	10 to 42	V
Operating supply voltage 2	$V_{DD}$	With signals applied	$5\pm 5\%$	V
Input high voltage	$V_{IH}$	Pins 10, 12, 13, 14, 15, 17	2.5 to $V_{DD}$	V
Input low voltage	$V_{IL}$	Pins 10, 12, 13, 14, 15, 17	0 to 0.6	V
Output current 1	$I_{OH1}$	$T_c=105^\circ\text{C}$ , $\text{CLOCK}\geq 200\text{Hz}$ , Continuous operation, duty=100%	3.0	A
Output current 2	$I_{OH2}$	$T_c=80^\circ\text{C}$ , $\text{CLOCK}\geq 200\text{Hz}$ , Continuous operation, duty=100%, See the motor current ( $I_{OH}$ ) derating curve	3.3	A
CLOCK frequency	$f_{CL}$	Minimum pulse width: at least $10\mu\text{s}$	0 to 50	kHz
Phase driver withstand voltage	$V_{DSS}$	$I_D=1\text{mA}$ ( $T_c=25^\circ\text{C}$ )	100min	V
Recommended operating substrate temperature	$T_c$	No condensation	0 to 105	$^\circ\text{C}$
Recommended $V_{ref}$ range	$V_{ref}$	$T_c=105^\circ\text{C}$	0.14 to 1.31	V

Refer to the graph for each conduction-period tolerance range for the output current and brake current.

### Electrical Characteristics at $T_c = 25^\circ\text{C}$ , $V_{CC} = 24\text{V}$ , $V_{DD} = 5.0\text{V}$

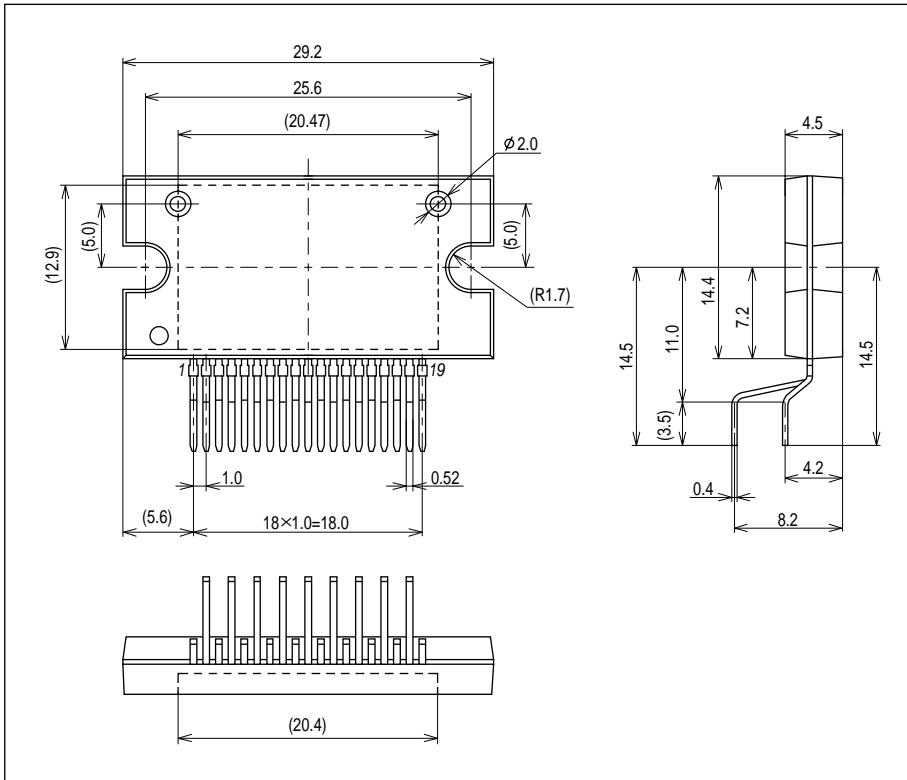
Parameter	Symbol	Conditions	min	typ	max	unit
$V_{DD}$ supply current	$I_{CCO}$	Pin 9 current $\text{CLOCK}=\text{GND}$		5.0	9	mA
Output average current	$I_{oave}$	$R/L=1\Omega/0.62\text{mH}$ in each phase	0.629	0.694	0.768	A
FET diode forward voltage	$V_{df}$	$I_f=1\text{A}$ ( $R_L=23\Omega$ )		1.0	1.6	V
Output saturation voltage	$V_{sat}$	$R_L=23\Omega$		0.26	0.38	V
Input leak current	$I_{IL}$	Pins 10, 12, 13, 14, 15, 17 $=\text{GND}$ and $5\text{V}$			$\pm 10$	$\mu\text{A}$
$V_{ref}$ input bias current	$I_{IB}$	Pin 19 $=1.0\text{V}$		204	216	$\mu\text{A}$
PWM frequency	$f_c$		35	45	56	kHz

\* $I_{oave}$  values are for when the lead frame of the product is soldered to the mounting substrate.

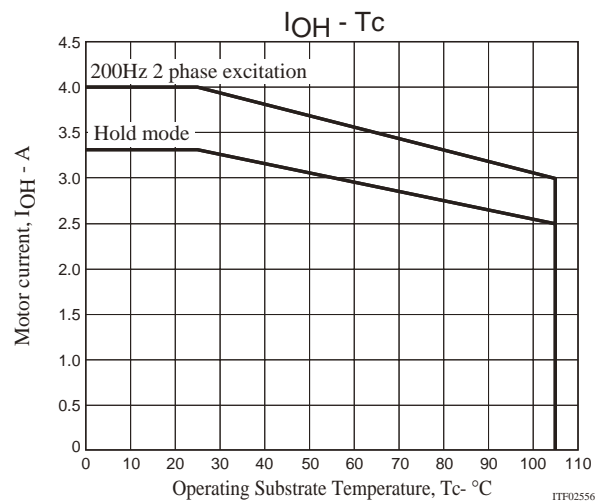
Notes: A fixed-voltage power supply must be used.

## Package Dimensions

unit:mm (typ)



Derating curve of motor current,  $I_{OH}$ , vs. STK672-610 Operating substrate temperature,  $T_c$



### Notes

- The current range given above represents conditions when output voltage is not in the avalanche state.
- If the output voltage is in the avalanche state, see the allowable avalanche energy for STK672-6\*\* series hybrid ICs given in a separate document.
- The operating substrate temperature,  $T_c$ , given above is measured while the motor is operating. Because  $T_c$  varies depending on the ambient temperature,  $T_a$ , the value of  $I_{OH}$ , and the continuous or intermittent operation of  $I_{OH}$ , always verify this value using an actual set.



## Precautions

[Damage to the internal MOSFET]

- The RESETB pin must be fixed low when applying 5V power. If the RESETB pin is allowed to go high at the same time as the 5V power, simultaneous ON of the output phase will result, causing damage to the internal MOSFET.

[GND wiring]

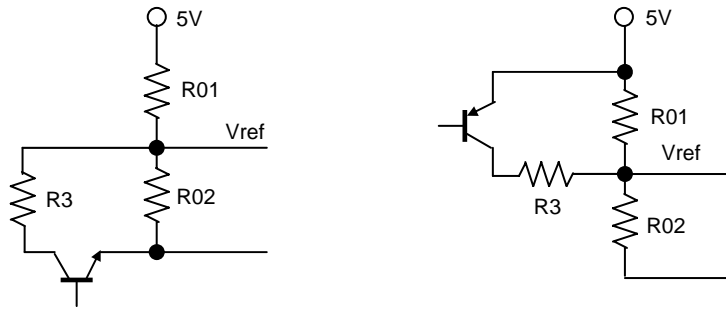
- To reduce noise on the 5V system, be sure to place the GND of C01 in the circuit given above as close as possible to Pin 2 and Pin 6 of the hybrid IC. Also, to achieve accurate current settings, be sure to connect Vref GND to Pin 18 (S.G) used to set the current and to the point where P.G1 and P.G2 share a connection.
- If the driver region VSS pin (Pin 16), S.G pin (Pin 18), P.G1 pin (Pin 2), and P.G2 pin (Pin 6) cannot be connected to a single ground, make sure to connect the VSS pin to the control system S.GND, and the S.G pin to the P.G1 pin and P.G2 pin.

[Input pins]

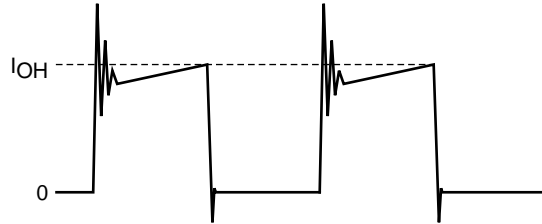
- If VDD is not being applied to the hybrid IC, do not apply voltage to input Pins 10, 12, 13, 14, 15, or 17. In addition, if VDD is being applied, use care that each input pin does not apply a negative voltage less than -0.3V to VSS, Pin 16, and do not apply a voltage greater than or equal to VDD voltage.
- Do not wire by connecting the circuit pattern on the P.C.B side to Pins 7, 8, or 11 on the N.C. shown in the internal block diagram.
- Insert resistor RO3 (47 to 100Ω) so that the discharge energy from capacitor CO4 is not directly applied to the CMOS IC in this hybrid device. If the diode D1 has Vf characteristics with Vf less than or equal to 0.6V (when If = 0.1A), this will be smaller than the CMOS IC input pin diode Vf. If this is the case RO3 may be replaced with a short without problem.
- Both TTL and CMOS levels are used for the pin 10, 12, 13, 15 and 17 inputs.
- Since the input pins do not have built-in pull-up resistors, when the open-collector type pins 10, 12, 13, 15, and 17 are used as inputs, a 1 to 15kΩ pull-up resistor (to VDD) must be used.  
At this time, use a device for the open collector driver that has output current specifications that pull the voltage down to less than 0.6V at Low level (less than 0.6V at Low level when IOL=5mA).
- If input pins are connected to GND (VSS) using a pull-down resistor, be sure to mount a resistor having a resistance of 120Ω or less. If designs call for a pull-down resistor having a resistance in the range 120Ω to 30kΩ, be absolutely sure to mount a 1,000pF capacitor between the input pins and the VSS Pin. Because sufficient VIL cannot be maintained due to the effect of input leak current, IIL=±10μA max, do not connect a pull-down resistor having a resistance of 30kΩ or higher.
- The sample application circuit includes a simple reset circuit using D1, R03, C02, and R04. If 5V power rises while voltage still remains in C02, the reset signal cannot be detected as LOW and the driver may be damaged because ON operations result at the same time that driver output is in A or AB phase or B or BB phase. The voltage of C02 must therefore be less than 0.6V when the 5V power rises.  
In addition, if a RESETB signal is to be input based on an external signal such as the CLOCK signal, RESETB must always be fixed to a Low level when the 5V power signal rises.
- To prevent malfunction due to chopping noise, we recommend that you mount a 1000pF capacitor between Pin 16 and each of the input Pins 10, 12, 13, 14, 15, and 17. Be sure to mount the capacitor as close as possible to the pins of hybrid IC.  
If input is fixed Low, directly connect to Pin 16.  
If input is fixed High, directly connect to the 5V power line.

[Current setting Vref]

- Considering the specifications of the Vref input bias current, IIB, a value of 1kΩ or less is recommended for R02.
- If the motor current is temporarily reduced, the circuit given below (STK672-600: IOH>0.2A, STK672-610: IOH>0.3A) is recommended.
- Although the driver is equipped with a fixed current control function, it is not equipped with an overcurrent protection function to ensure that the current does not exceed the maximum output current, IOH max. If Vref is mistakenly set to a voltage that exceeds IOH max, the driver will be damaged by overcurrent.



- Motor current peak value  $I_{OH}$  setting



- When R02 is open

$$I_{OH} = [V_{ref} \times 1k / (1k + 3.9k)] \div R_s = (V_{ref} \div 4.9) \div R_s$$

The values 1k and 3.9k represent internal driver resistance values, while  $R_s$  represents the internal driver current detection resistance.

$$V_{ref} = (4.9k \div (4.9k + R_{01})) \times 5V \text{ (or } 3.3V) = I_{OH} \times 4.9 \times R_s$$

The value 4.9k represents the series resistance value of the internal driver values of 1k and 3.9k.

- If R02 is connected

$$I_{OH} = [V_{ref} \times 1k / (1k + 3.9k)] \div R_s = (V_{ref} \div 4.9) \div R_s$$

The values 1k and 3.9k represent the internal driver resistance values, while  $R_s$  represents the internal driver current detection resistance.

$$V_{ref} = (R_{0x} \div (R_{01} + R_{0x})) \times 5V \text{ (or } 3.3V) = I_{OH} \times 4.9 \times R_s$$

$$= [(4.9k \times R_{02}) \div ((4.9k \times R_{02}) + R_{01} \times (4.9k + R_{02}))] \times 5V \text{ (or } 3.3V)$$

$$R_{0x} = (4.9k \times R_{02}) \div (4.9k + R_{02})$$

$R_s$  represents the current detection resistance inside the HIC, while the value 4.9k in the formula above represents the internal resistance value of the Vref pin.

$$R_s = 0.141\Omega \text{ when using the STK672-600}$$

$$R_s = 0.089\Omega \text{ when using the STK672-610}$$

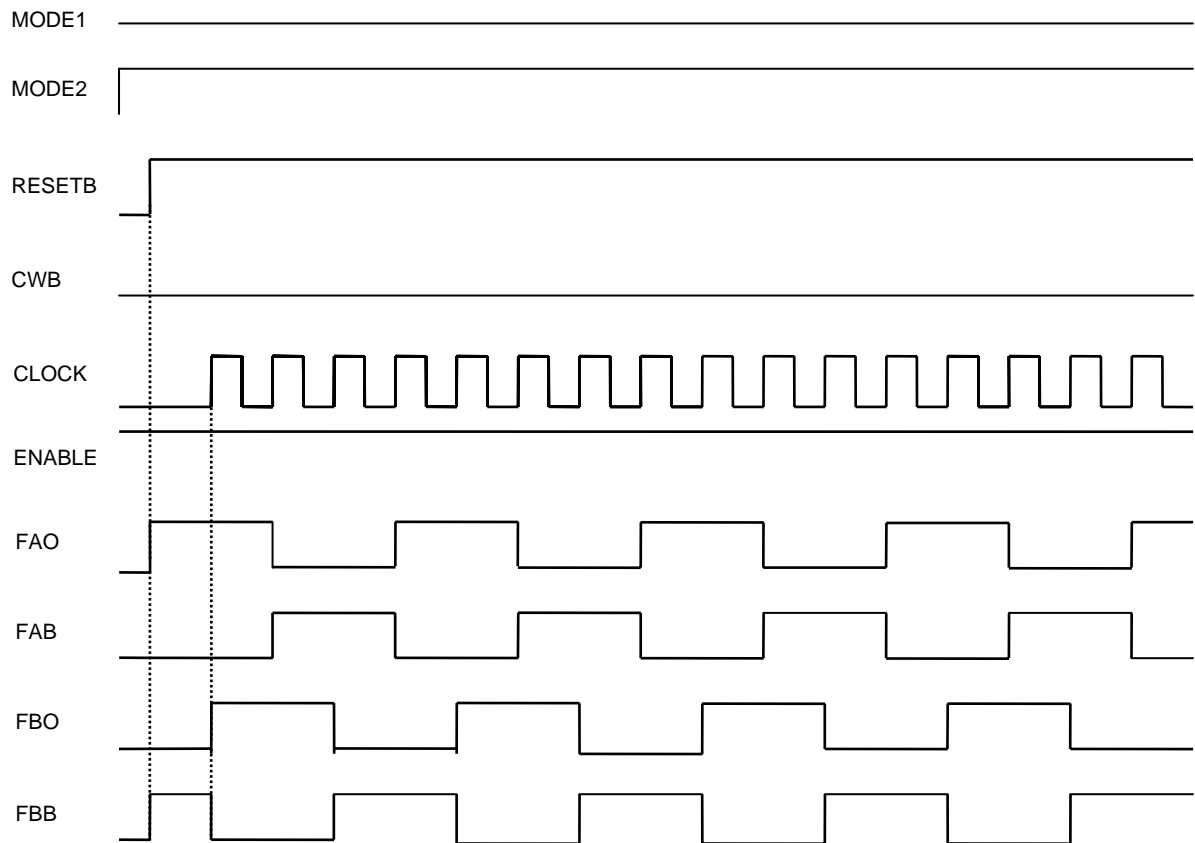
## Input Pin Functions

Pin Name	Pin No.	Function	Input Conditions When Operating
CLOCK	12	Reference clock for motor phase current switching	Operates on the rising edge of the signal (MODE2=H)
MODE1	10	Excitation mode selection	Low: 2-phase excitation High: 1-2 phase excitation
MODE2	17		High: Rising edge Low: Rising and falling edge
CWB	13	Motor direction switching	Low: CW (forward) High: CCW (reverse)
RESETB	14	System reset and A, AB, B, and BB outputs cutoff. Applications must apply a reset signal for at least 10μs when $V_{DD}$ is first applied.	A reset is applied by a low level
ENABLE	15	The A, AB, B, and BB outputs are turned off, and after operation is restored by returning the ENABLE pin to the high level, operation continues with the same excitation timing as before the low-level input.	The A, AB, B, and BB outputs are turned off by a low-level input.

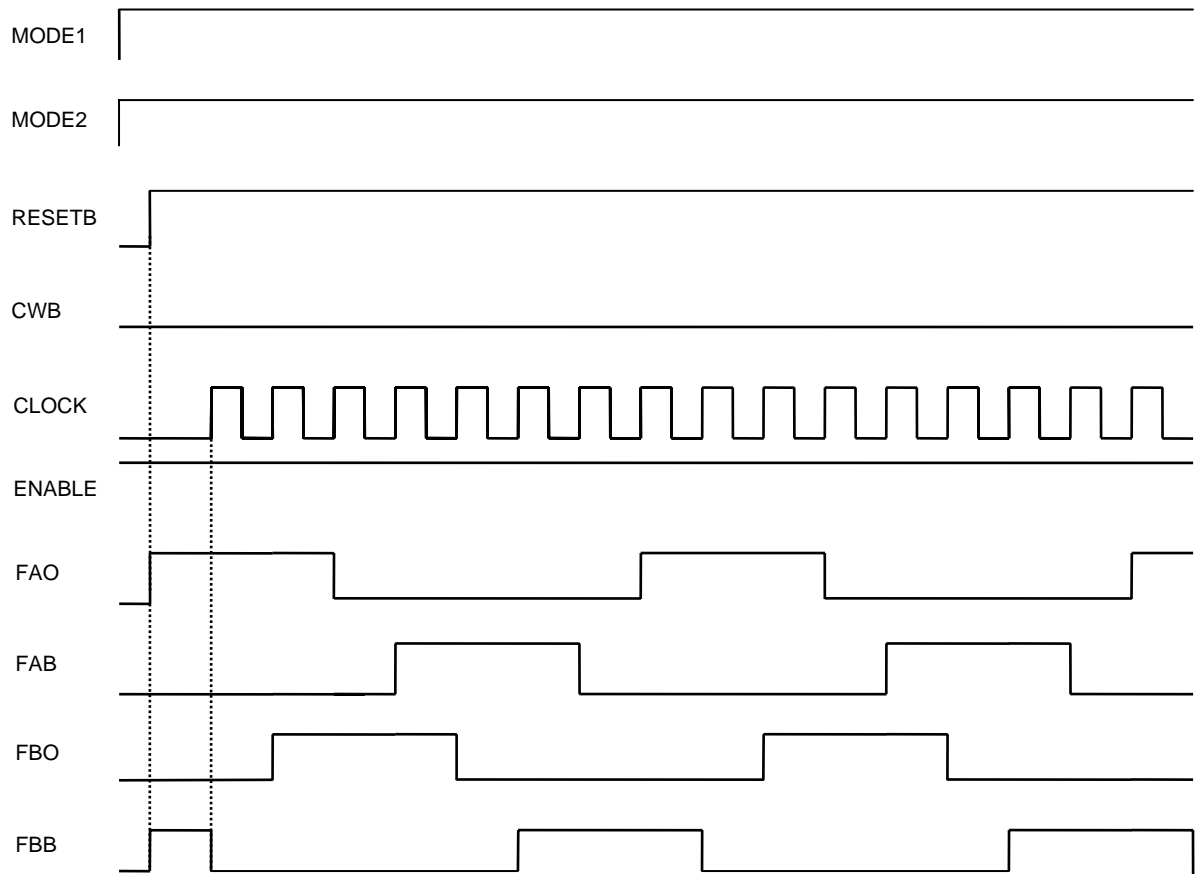
- (1) A simple reset function is formed from D1, CO4, RO3, and RO4 in this application circuit. With the CLOCK input held low, when the 5V supply voltage is brought up a reset is applied if the motor output phases A and BB are driven. If the 5V supply voltage rise time is slow (over 50ms), the motor output phases A and BB may not be driven. Increase the value of the capacitor CO2 and check circuit operation again.
- (2) See the timing chart for the concrete details on circuit operation.

## Timing Charts

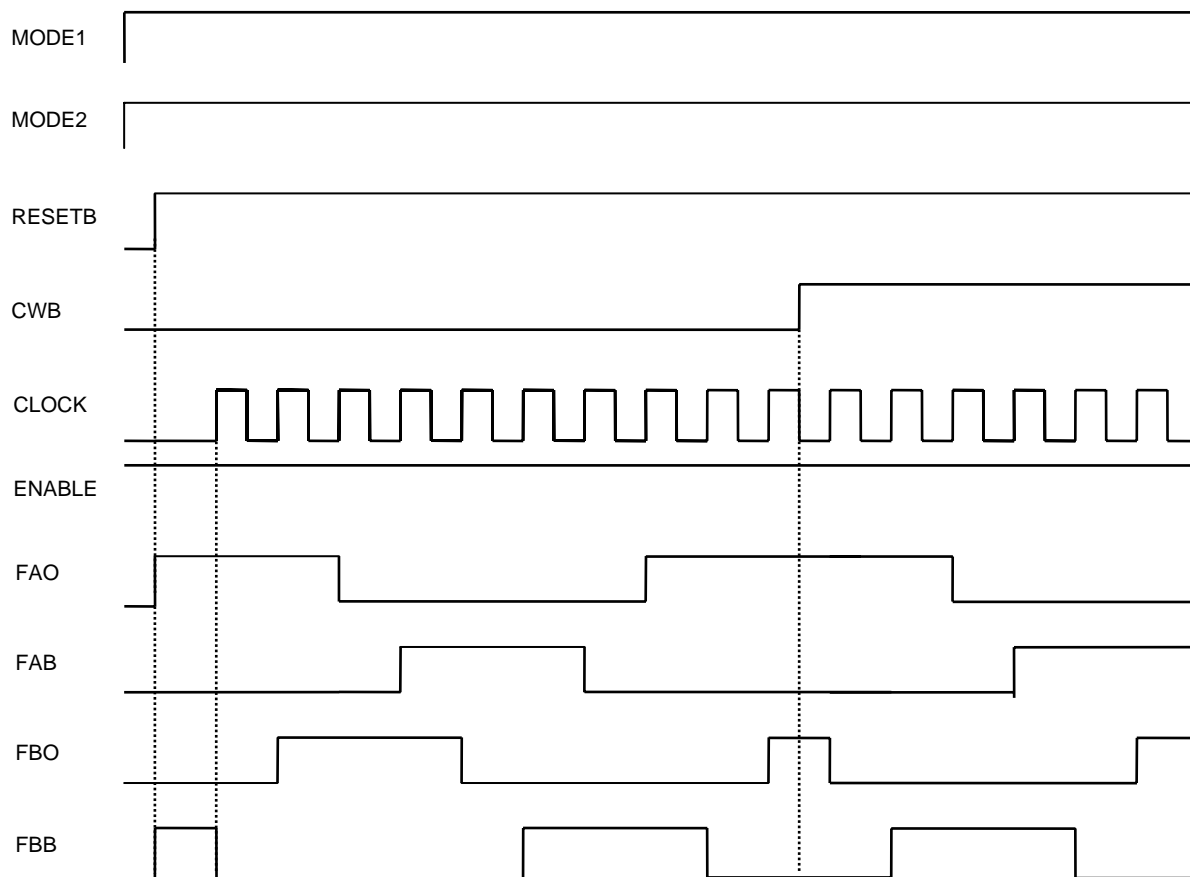
### 2-phase excitation



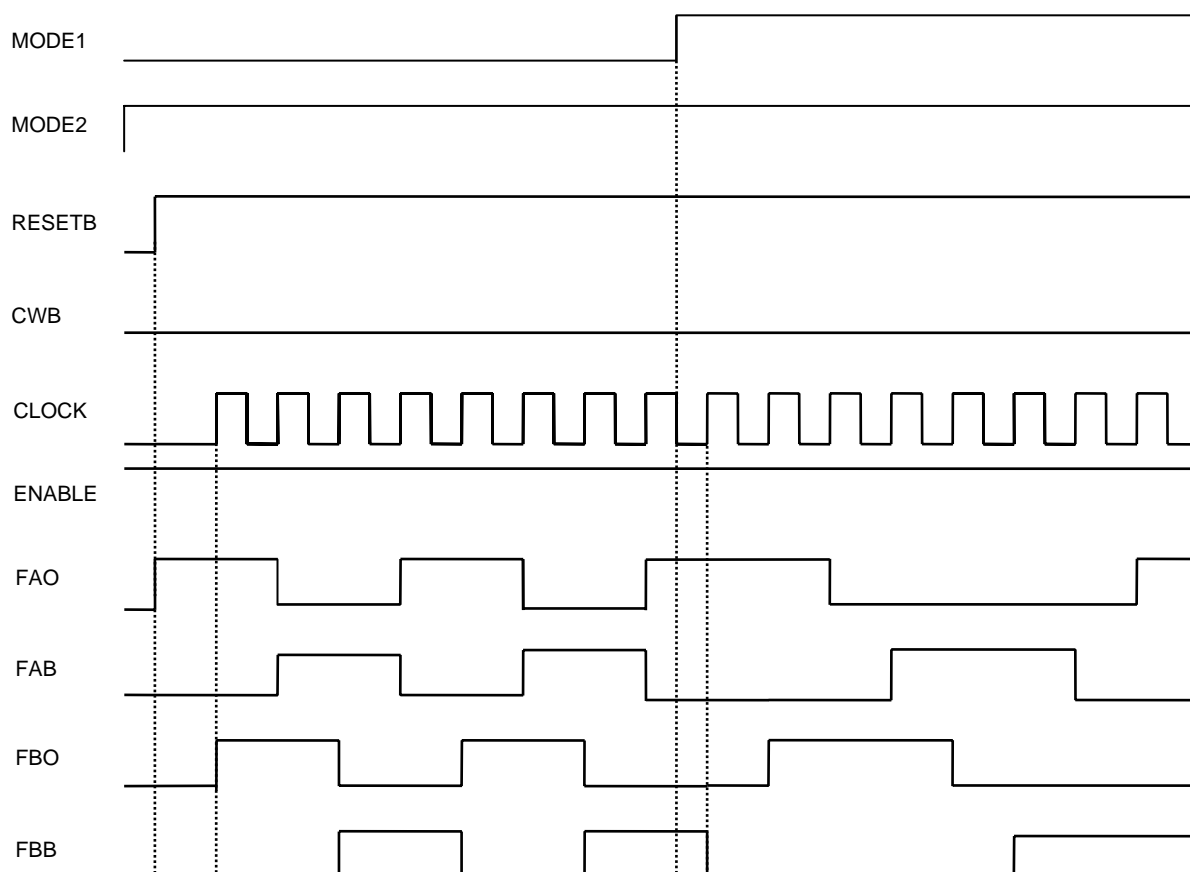
### 1-2 phase excitation



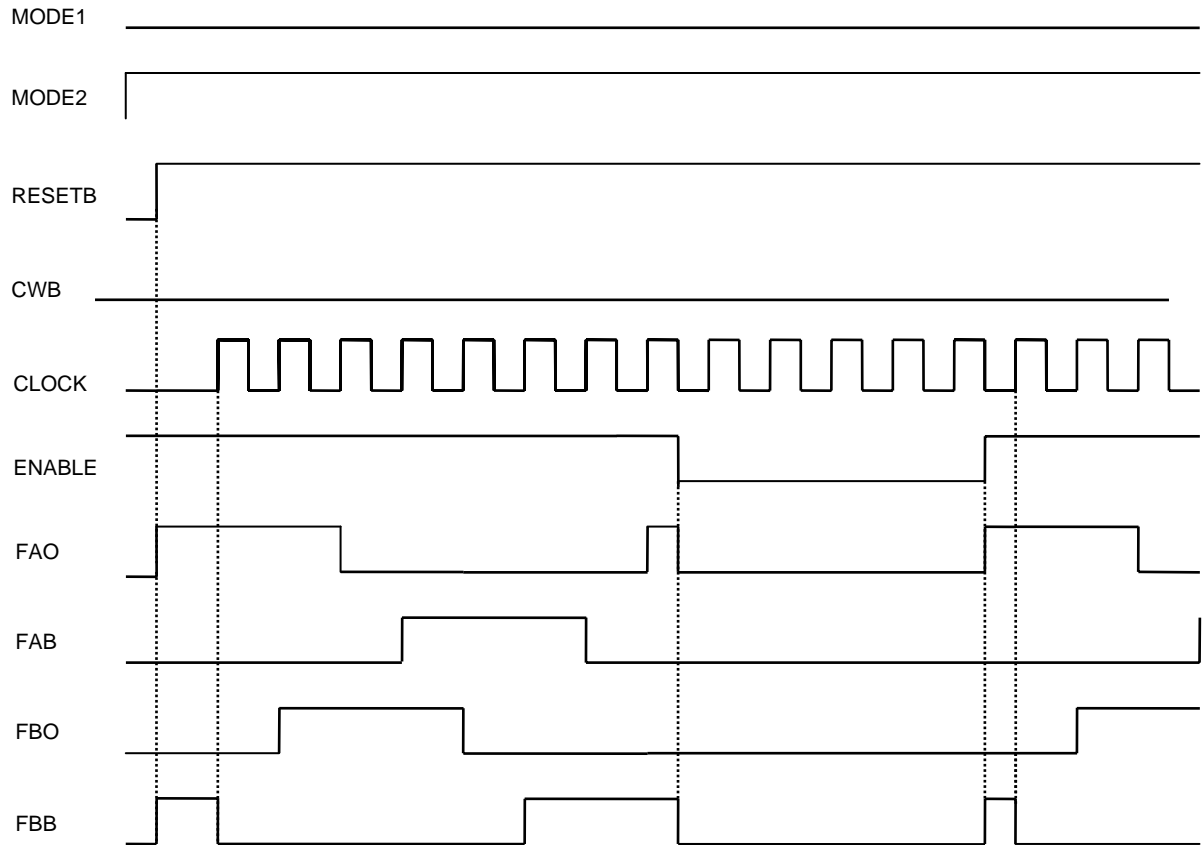
## 1-2 phase excitation (CWB)



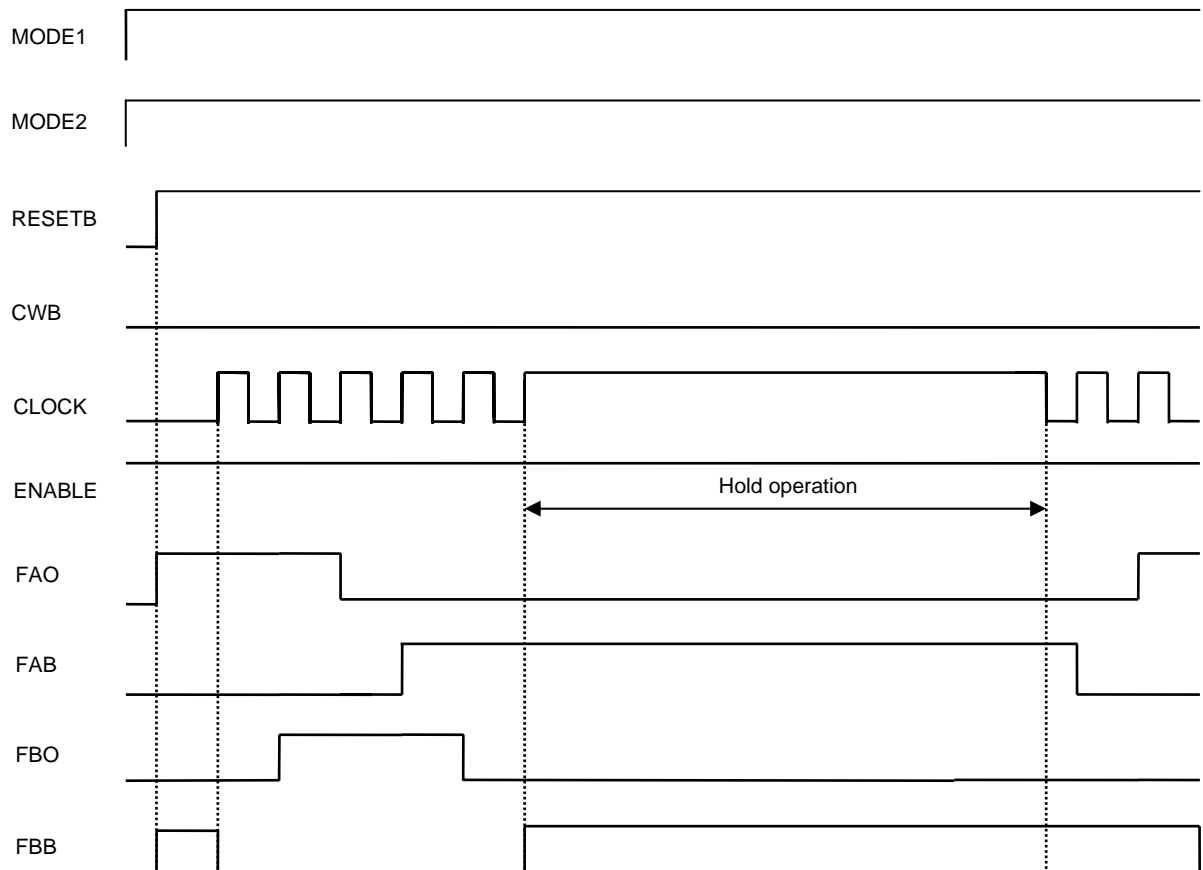
## 2-phase excitation→Switch to 1-2 phase excitation



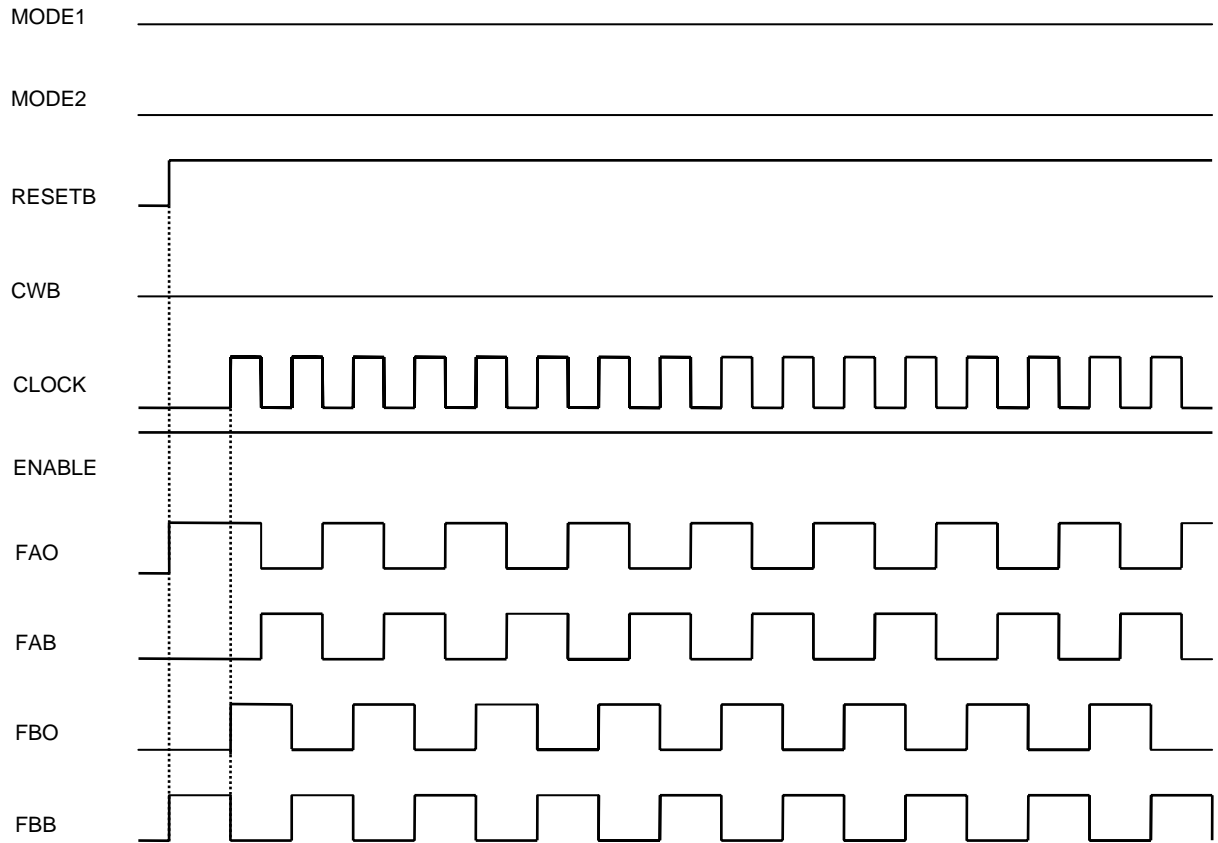
## 1-2 phase excitation (ENABLE)



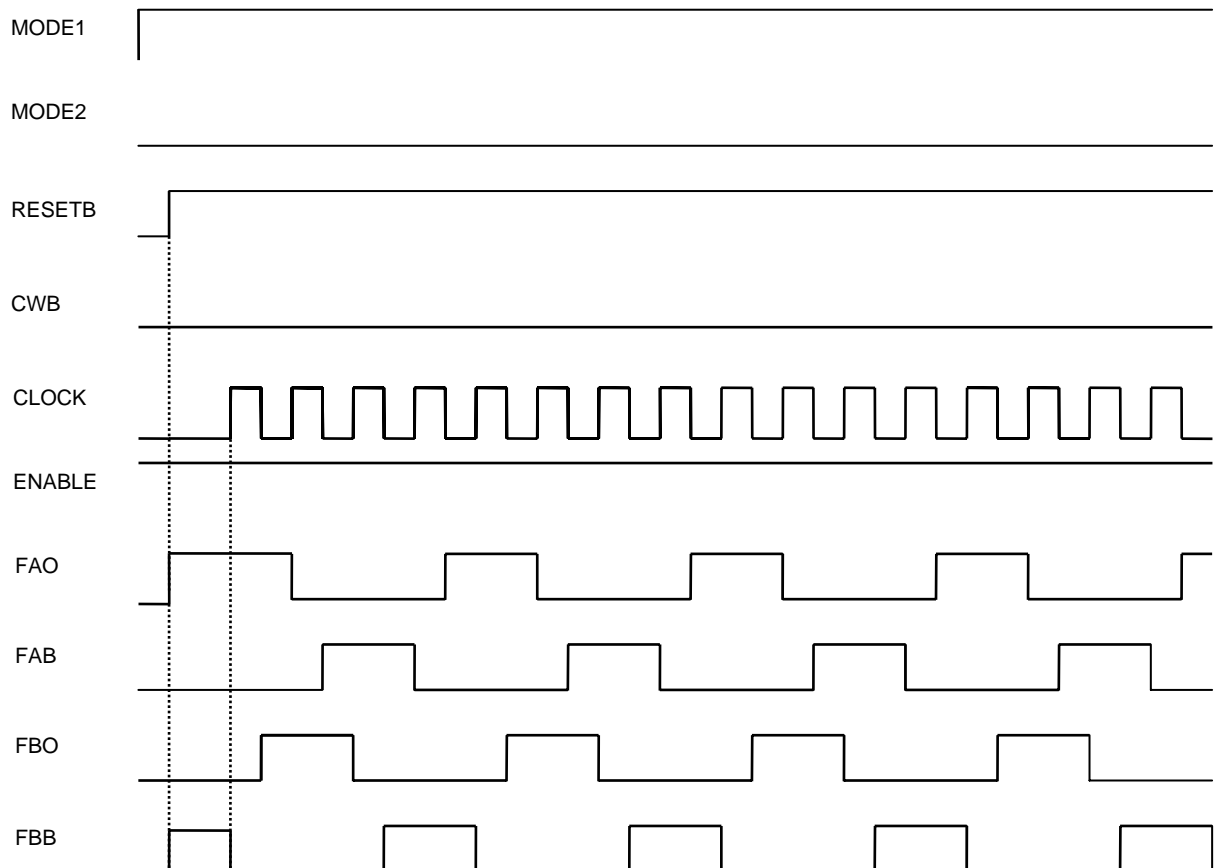
## 1-2 phase excitation (Hold operation results during fixed CLOCK)



## 2-phase excitation (MODE2)



## 1-2 phase excitation (MODE2)



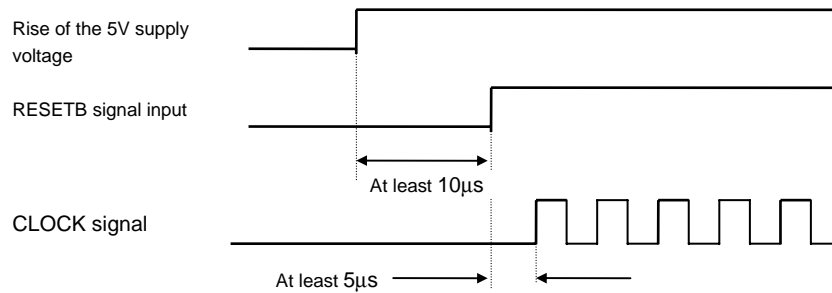
## Usage Notes

### 1. STK672-600 and STK672-610 input signal functions and timing

(All inputs have no internal pull-up resistor and are TTL level Schmitt trigger inputs.)

#### [RESETB and CLOCK (Input signal timing when power is first applied)]

As shown in the timing chart, a RESETB signal input is required by the driver to operate with the timing in which the F1 gate is turned on first. The RESETB signal timing must be set up to have a width of at least 10 $\mu$ s, as shown below. The capacitor CO2, and the resistors RO3 and RO4 in the application circuit form simple reset circuit that uses the RC time constant rising time. However, when designing the RESETB input based on V<sub>IH</sub> levels, the application must have the timing shown in figure.



RESETB and CLOCK Signals Input Timing

#### [CLOCK (Phase switching clock)]

- Input frequency: DC to 50kHz
- Minimum pulse width: 10 $\mu$ s
- MODE2=1(High) Signals are read on the rising edge.
- MODE2=0(Low) Signals are read on the rising and falling edges.

#### [CWB (Motor direction setting)]

The direction of rotation is switched by setting CWB to 1 (high) or 0 (low). See the timing charts for details on the operation of the outputs.

Note: The state of the CWB input must not be changed during the 6.25 $\mu$ s period before and after the rising edge of the CLOCK input.

#### [ENABLE (Forcible on/off control of the A, AB, B, and BB outputs, and hybrid IC internal operation)]

ENABLE=1: Normal operation

ENABLE=0: Outputs A, AB, B, and BB forced to the off state.

If, during the state where CLOCK signal input is provided, the ENABLE pin is set to 0 and then is later restored to the 1 state, the IC will resume operation with the excitation timing continued from before the point ENABLE was set to 0.

If sudden stop is applied to the CLOCK signal used for motor rotation, the motor axis may advance beyond the theoretical position due to inertia. To stop at the theoretical position, the SLOW DOWN setting for gradually slowing the CLOCK cycle is required.

Enable must be initially set high for input as shown in the timing chart.

#### [MODE1 and MODE2 (Excitation mode selection)]

MODE1=0: 2-phase excitation

MODE2=1: Rising edge of CLOCK

MODE1=1: 1-2 phase excitation

MODE2=0: Rising and falling edges of CLOCK

See the timing charts for details on output operation in these modes.

Note: The state of the MODE input must not be changed during the 5 $\mu$ s period before and after the rising edge of the CLOCK input.

## 2. Calculating STK672-610 HIC Internal Power Loss

The average internal power loss in each excitation mode of the STK672-610 can be calculated from the following formulas.

Each excitation mode

2-phase excitation mode

$$2PdAV_{ex} = (V_{sat} + V_{df}) \times 0.5 \times \text{CLOCK} \times I_{OH} \times t_2 + 0.5 \times \text{CLOCK} \times I_{OH} \times (V_{sat} \times t_1 + V_{df} \times t_3)$$

1-2 Phase excitation mode

$$1-2PdAV_{ex} = (V_{sat} + V_{df}) \times 0.25 \times \text{CLOCK} \times I_{OH} \times t_2 + 0.25 \times \text{CLOCK} \times I_{OH} \times (V_{sat} \times t_1 + V_{df} \times t_3)$$

Motor hold mode

$$\text{HoldPdAV}_{ex} = (V_{sat} + V_{df}) \times I_{OH}$$

$V_{sat}$ : Combined voltage represented by the  $R_{on}$  voltage drop+ shunt resistor

$V_{df}$ : Combined voltage represented by the MOSFET body diode+shunt resistor

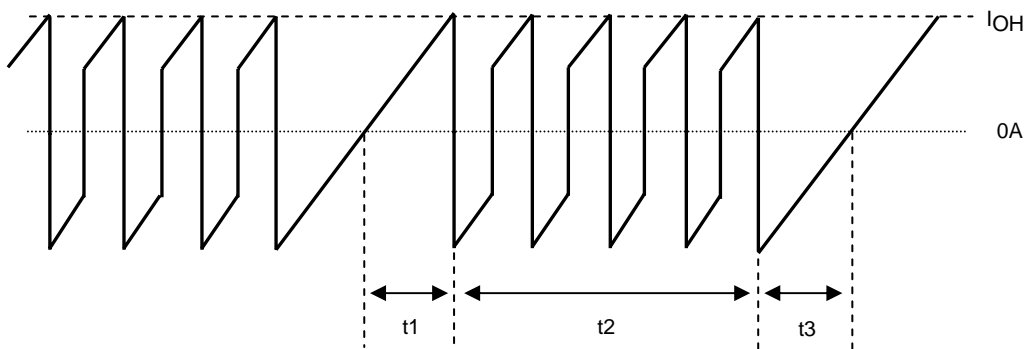
CLOCK: Input CLOCK (CLOCK pin signal frequency)

$t_1$ ,  $t_2$ , and  $t_3$  represent the waveforms shown in the figure below.

$t_1$ : Time required for the winding current to reach the set current ( $I_{OH}$ )

$t_2$ : Time in the constant current control (PWM) region

$t_3$ : Time from end of phase input signal until inverse current regeneration is complete



Motor COM Current Waveform Model

$$t_1 = (-L/(R+0.26)) \ln(1 - ((R+0.26)/V_{CC}) \times I_{OH})$$

$$t_3 = (-L/R) \ln((V_{CC}+0.42)/(I_{OH} \times R + V_{CC}+0.42))$$

$V_{CC}$ : Motor supply voltage (V)

$L$ : Motor inductance (H)

$R$ : Motor winding resistance ( $\Omega$ )

$I_{OH}$ : Motor set output current crest value (A)

Relationship of CLOCK,  $t_1$ ,  $t_2$ , and  $t_3$  in each excitation mode

2-phase excitation mode:  $t_2 = (2/\text{CLOCK}) - (t_1 + t_3)$

1-2 phase excitation mode:  $t_2 = (3/\text{CLOCK}) - t_1$

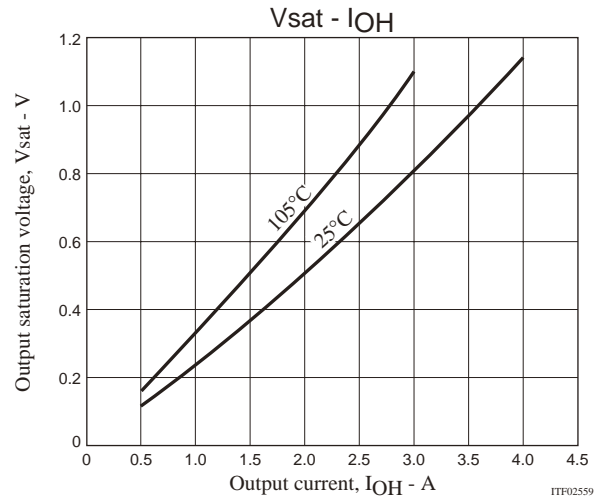
For  $V_{sat}$  and  $V_{df}$ , be sure to substitute values from the graphs of  $V_{sat}$  vs.  $I_{OH}$  and  $V_{df}$  vs.  $I_{OH}$  while the set current value is  $I_{OH}$ .

Then, determine whether a heat sink is required by comparing with the graph of  $\Delta T_c$  vs.  $P_d$  based on the average HIC power loss calculated.

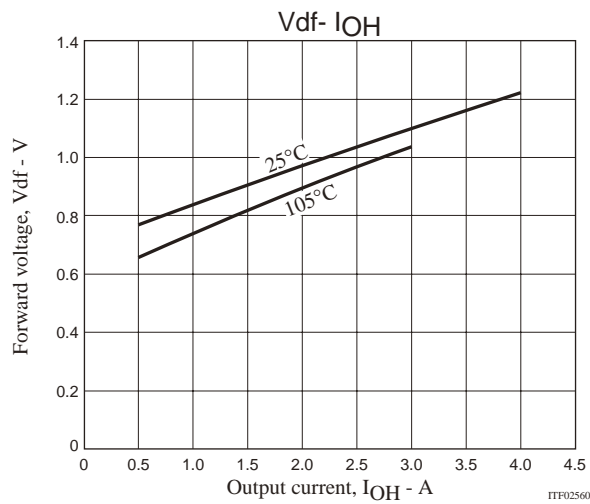
When designing a heat sink, refer to the section "Thermal design" found on the next page. The average HIC power loss,  $P_{dAV}$ , described above does not have the avalanche's loss. To include the avalanche's loss, be sure to add Equation (2), "STK676-6\*\* Allowable Avalanche Energy Value" to  $P_{dAV}$  above. When using this IC without a fin always check for temperature increases in the set, because the HIC substrate temperature,  $T_c$ , varies due to effects of convection around the HIC.

## STK672-610

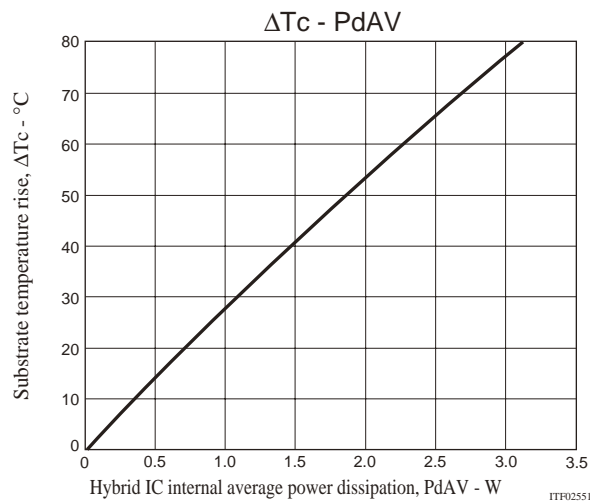
STK672-610 Output saturation voltage,  $V_{sat}$  - Output current,  $I_{OH}$



STK672-610 Forward voltage,  $V_{df}$  - Output current,  $I_{OH}$



Substrate temperature rise,  $\Delta T_c$  (no heat sink) - Internal average power dissipation,  $P_{dAV}$



### 3. STK672-610 Allowable Avalanche Energy Value

#### (1) Allowable Range in Avalanche Mode

When driving a 2-phase stepping motor with constant current chopping using an STK672-6\*\* Series hybrid IC, the waveforms shown in Figure 1 below result for the output current,  $I_D$ , and voltage,  $V_{DS}$ .

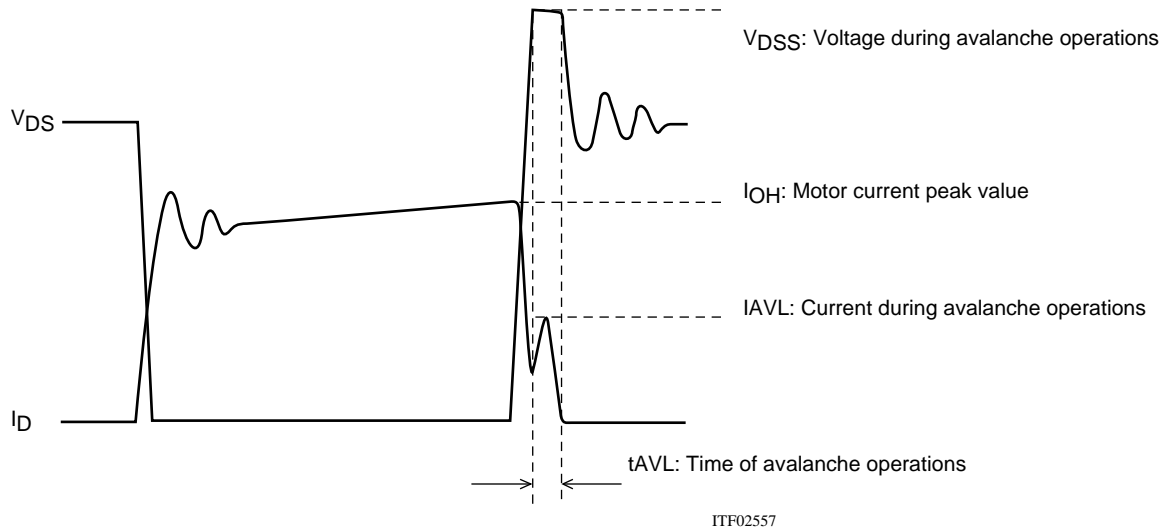


Figure 1 Output Current,  $I_D$ , and Voltage,  $V_{DS}$ , Waveforms 1 of the STK672-6\*\* Series when Driving a 2-Phase Stepping Motor with Constant Current Chopping

When operations of the MOSFET built into STK672-6\*\* Series ICs is turned off for constant current chopping, the  $I_D$  signal falls like the waveform shown in the figure above. At this time, the output voltage,  $V_{DS}$ , suddenly rises due to electromagnetic induction generated by the motor coil.

In the case of voltage that rises suddenly, voltage is restricted by the MOSFET  $V_{DS}$ . Voltage restriction by  $V_{DS}$  results in a MOSFET avalanche. During avalanche operations,  $I_D$  flows and the instantaneous energy at this time,  $E_{AVL1}$ , is represented by Equation (1).

$$E_{AVL1} = V_{DS} \times I_{AVL} \times 0.5 \times t_{AVL} \text{ ----- (1)}$$

$V_{DS}$ : V units,  $I_{AVL}$ : A units,  $t_{AVL}$ : sec units

The coefficient 0.5 in Equation (1) is a constant required to convert the  $I_{AVL}$  triangle wave to a square wave.

During STK672-6\*\* Series operations, the waveforms in the figure above repeat due to the constant current chopping operation. The allowable avalanche energy,  $E_{AVL}$ , is therefore represented by Equation (2) used to find the average power loss,  $P_{AVL}$ , during avalanche mode multiplied by the chopping frequency in Equation (1).

$$P_{AVL} = V_{DS} \times I_{AVL} \times 0.5 \times t_{AVL} \times f_c \text{ ----- (2)}$$

$f_c$ : Hz units ( $f_c$  is set to the PWM frequency of 50kHz.)

For  $V_{DS}$ ,  $I_{AVL}$ , and  $t_{AVL}$ , be sure to actually operate the STK672-6\*\* Series and substitute values when operations are observed using an oscilloscope.

Ex. If  $V_{DS}=110V$ ,  $I_{AVL}=1A$ ,  $t_{AVL}=0.2\mu s$  when using a STK672-610 driver, the result is:

$$P_{AVL} = 110 \times 1 \times 0.5 \times 0.2 \times 10^{-6} \times 50 \times 10^3 = 0.55W$$

$V_{DS}=110V$  is a value actually measured using an oscilloscope.

The allowable loss range for the allowable avalanche energy value,  $P_{AVL}$ , is shown in the graph in Figure 3. When examining the avalanche energy, be sure to actually drive a motor and observe the  $I_D$ ,  $V_{DS}$ , and  $t_{AVL}$  waveforms during operation, and then check that the result of calculating Equation (2) falls within the allowable range for avalanche operations.

(2)  $I_D$  and  $V_{DS}$  Operating Waveforms in Non-avalanche Mode

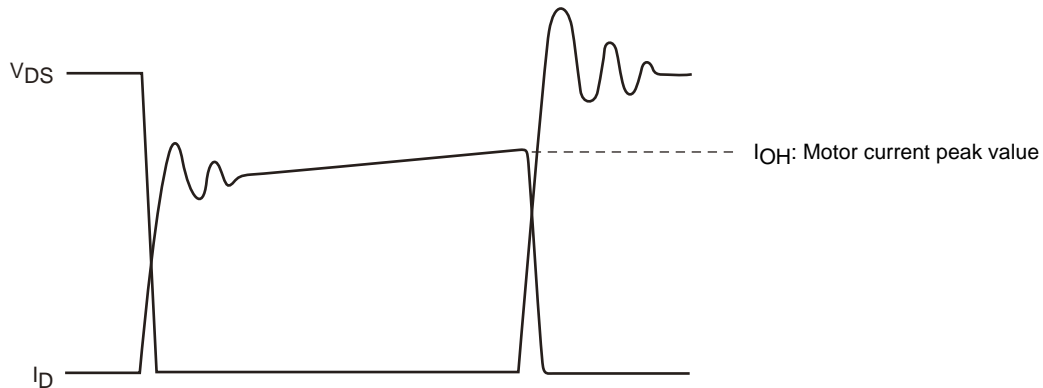
Although the waveforms during avalanche mode are given in Figure 1, sometimes an avalanche does not result during actual operations.

Factors causing avalanche are listed below.

- Poor coupling of the motor's phase coils (electromagnetic coupling of A phase and AB phase, B phase and BB phase).
- Increase in the lead inductance of the harness caused by the circuit pattern of the P.C. board and motor.
- Increases in  $V_{DS}$ ,  $t_{AVL}$ , and  $I_{AVL}$  in Figure 1 due to an increase in the supply voltage from 24V to 36V.

If the factors above are negligible, the waveforms shown in Figure 1 become waveforms without avalanche as shown in Figure 2.

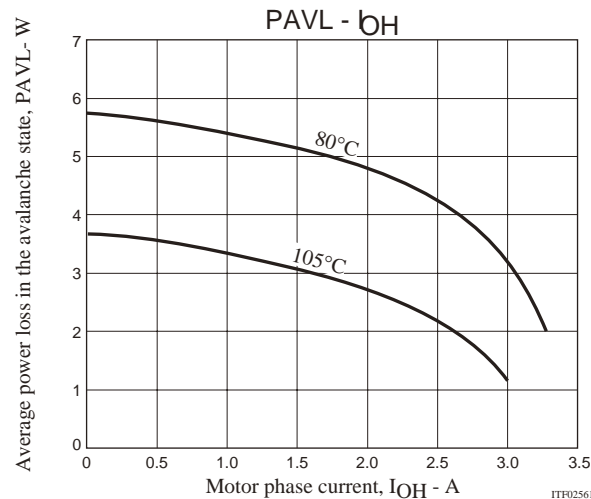
Under operations shown in Figure 2, avalanche does not occur and there is no need to consider the allowable loss range of  $PAVL$  shown in Figure 3.



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Figure 2 Output Current,  $I_D$ , and Voltage,  $V_{DS}$ , Waveforms 2 of the STK672-6\*\* Series when Driving a 2-Phase Stepping Motor with Constant Current Chopping

Figure 3 Allowable Loss Range,  $PAVL-I_{OH}$  During STK672-610 Avalanche Operations



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Note:

The operating conditions given above represent a loss when driving a 2-phase stepping motor with constant current chopping.

Because it is possible to apply 3.7W or more at  $I_{OH}=0A$ , be sure to avoid using the MOSFET body diode that is used to drive the motor as a zener diode.

#### 4. Thermal design

[Operating range in which a heat sink is not used]

Use of a heat sink to lower the operating substrate temperature of the HIC (Hybrid IC) is effective in increasing the quality of the HIC.

The size of heat sink for the HIC varies depending on the magnitude of the average power loss, PdAV, within the HIC. The value of PdAV increases as the output current increases. To calculate PdAV, refer to “Calculating Internal HIC Loss for the STK672-600 and STK672-610” in the specification document.

Calculate the internal HIC loss, PdAV, assuming repeat operation such as shown in Figure 1 below, since conduction during motor rotation and off time both exist during actual motor operations,

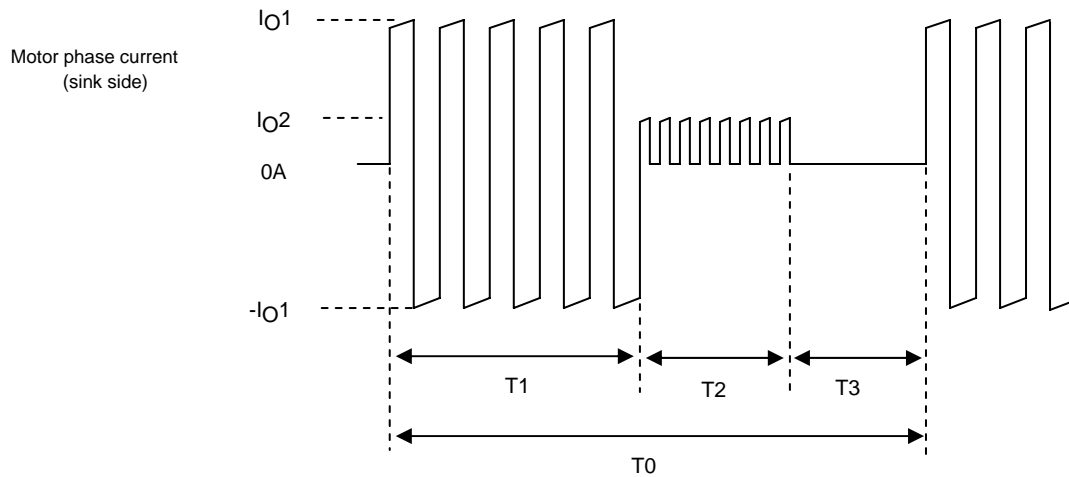


Figure 1 Motor Current Timing

T1: Motor rotation operation time

T2: Motor hold operation time

T3: Motor current off time

T2 may be reduced, depending on the application.

T0: Single repeated motor operating cycle

IO1 and IO2: Motor current peak values

Due to the structure of motor windings, the phase current is a positive and negative current with a pulse form.

Note that figure 1 presents the concepts here, and that the on/off duty of the actual signals will differ.

The hybrid IC internal average power dissipation PdAV can be calculated from the following formula.

$$PdAV = (T1 \times P1 + T2 \times P2 + T3 \times 0) \div T0 \quad \text{----- (I)}$$

(Here, P1 is the PdAV for IO1 and P2 is the PdAV for IO2)

If the value calculated using Equation (I) is 1.5W or less, and the ambient temperature, Ta, is 60°C or less, there is no need to attach a heat sink. Refer to Figure 2 for operating substrate temperature data when no heat sink is used.

[Operating range in which a heat sink is used]

Although a heat sink is attached to lower Tc if PdAV increases, the resulting size can be found using the value of θc-a in Equation (II) below and the graph depicted in Figure 3.

$$\theta_{c-a} = (Tc_{max} - Ta) \div PdAV \quad \text{----- (II)}$$

Tc max: Maximum operating substrate temperature = 105°C

Ta: HIC ambient temperature

Although a heat sink can be designed based on equations (I) and (II) above, be sure to mount the HIC in a set and confirm that the substrate temperature, Tc, is 105°C or less.

The average HIC power loss, PdAV, described above represents the power loss when there is no avalanche operation.

To add the loss during avalanche operations, be sure to add Equation (2), “Allowable STK672-6\*\* Avalanche Energy Value”, to PdAV.

Figure 2 Substrate temperature rise,  $\Delta T_c$ (no heat sink) - Internal average power dissipation, PdAV

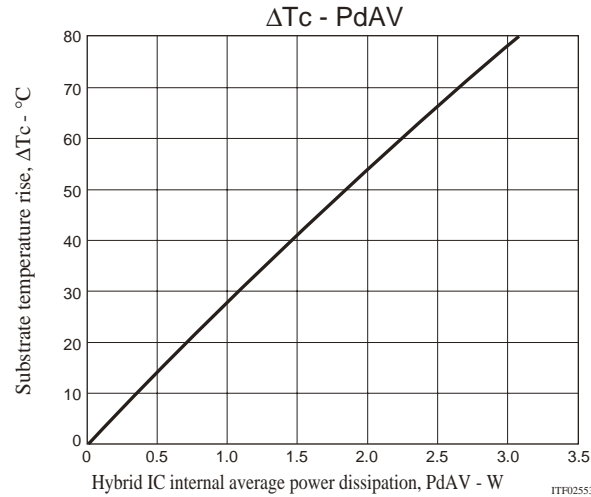
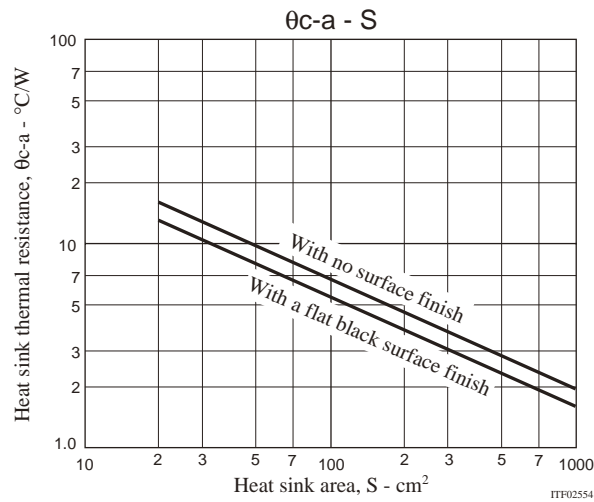


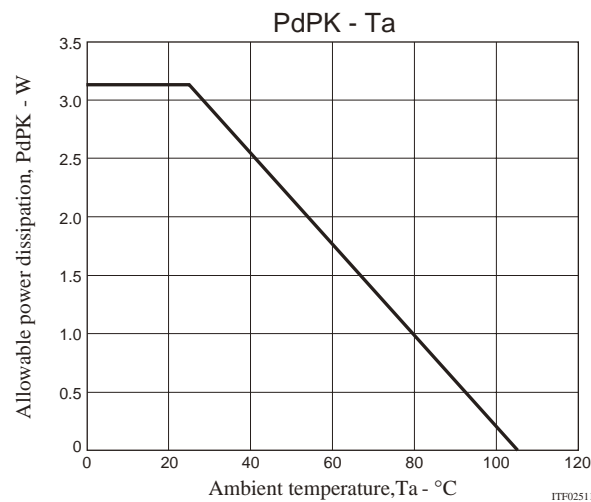
Figure 3 Heat sink area (Board thickness: 2mm) -  $\theta_{c-a}$



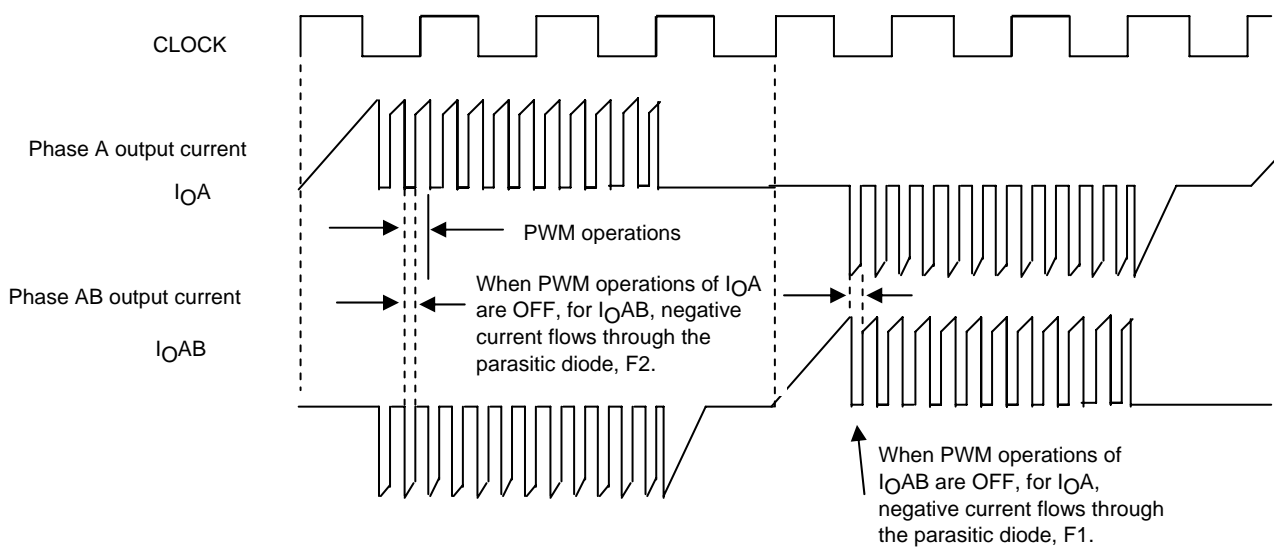
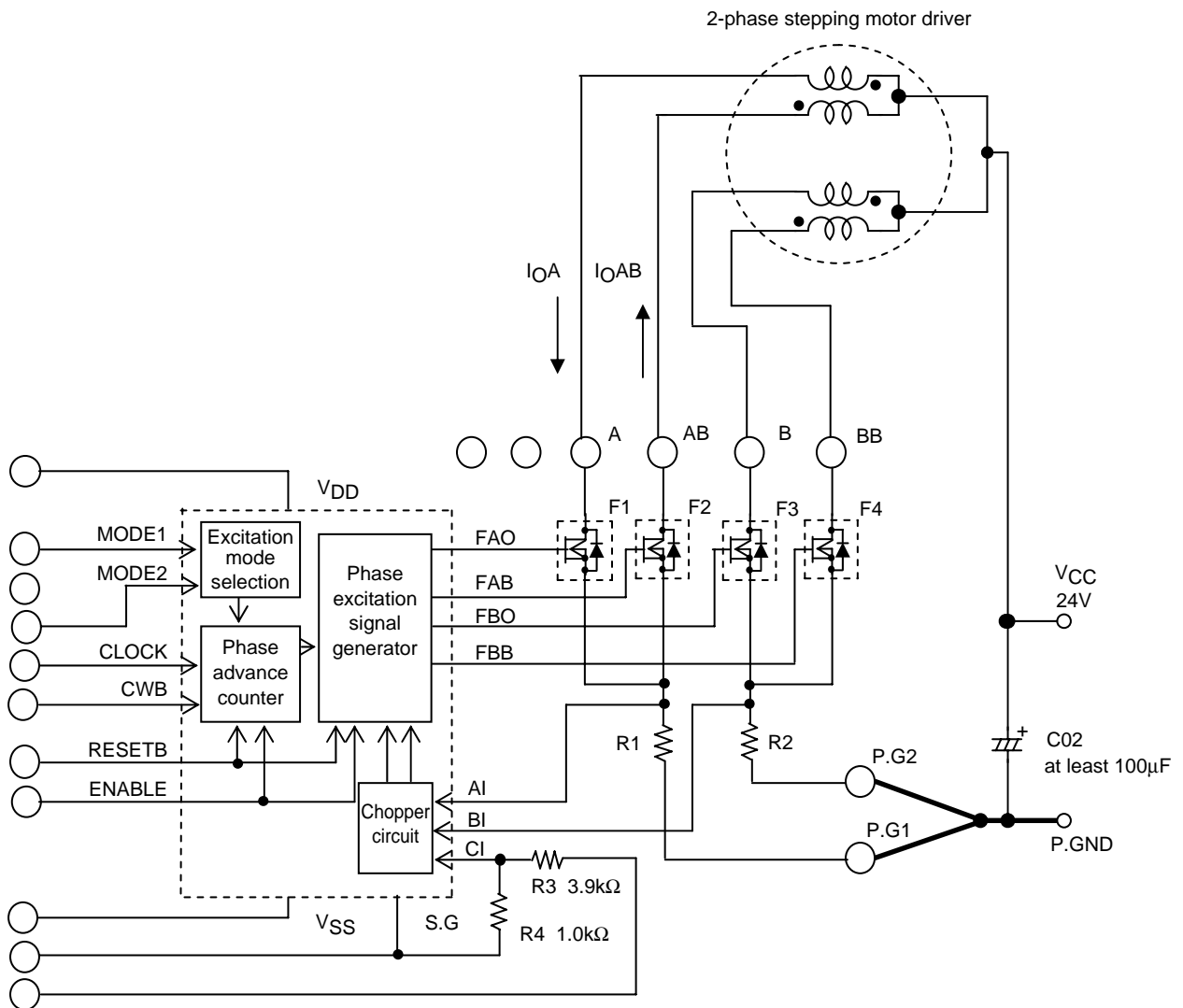
## 5. Mitigated Curve of Package Power Loss, PdPK, vs. Ambient Temperature, Ta

Package power loss, PdPK, refers to the average internal power loss, PdAV, allowable without a heat sink. The figure below represents the allowable power loss, PdPK, vs. fluctuations in the ambient temperature, Ta. Power loss of up to 3.1W is allowable at Ta=25°C, and of up to 1.75W at Ta=60°C.

Allowable power dissipation, PdPK(no heat sink) - Ambient temperature, Ta



6. Example of Stepping Motor Driver Output Current Path (1-2 phase excitation)



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